

## **Appendix B**

### **100-Year Pre-Project Modified Rational Method Analyses**

## **Drainage Basin 100**

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003,1985,1981 HYDROLOGY MANUAL

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Ver. 1.5A Release Date: 01/01/2003 License ID 1261

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* MEADOWOOD J-15965 \*  
\* 11/4/08 Pre-project (on-site) \*  
\* 100-yr Basin 100 \*  
\*\*\*\*\*

FILE NAME: MWB1H100.DAT

TIME/DATE OF STUDY: 09:17 11/04/2008

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00

6-HOUR DURATION PRECIPITATION (INCHES) = 3.600

SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP HIKE (FT) (FT) (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)				
=====	=====	=====	=====	=====	=====	=====
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN

OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

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FLOW PROCESS FROM NODE 100.00 TO NODE 101.00 IS CODE = 21

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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
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\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 813.00  
 DOWNSTREAM ELEVATION(FEET) = 780.00  
 ELEVATION DIFFERENCE(FEET) = 33.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

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 FLOW PROCESS FROM NODE 101.00 TO NODE 105.00 IS CODE = 51  
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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 780.00 DOWNSTREAM(FEET) = 500.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.4667  
 CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.358  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.48  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.83  
 AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 2.61  
 Tc(MIN.) = 9.30  
 SUBAREA AREA(ACRES) = 2.10 SUBAREA RUNOFF(CFS) = 4.01  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 2.30 PEAK FLOW RATE(CFS) = 4.39

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 4.54  
 LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 700.00 FEET.

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 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.30  
 RAINFALL INTENSITY(INCH/HR) = 6.36  
 TOTAL STREAM AREA(ACRES) = 2.30  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.39

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 103.00 TO NODE 104.00 IS CODE = 21  
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00



UPSTREAM ELEVATION (FEET) = 694.00  
 DOWNSTREAM ELEVATION (FEET) = 660.00  
 ELEVATION DIFFERENCE (FEET) = 34.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.865  
 SUBAREA RUNOFF (CFS) = 0.71  
 TOTAL AREA (ACRES) = 0.30 TOTAL RUNOFF (CFS) = 0.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 104.00 TO NODE 105.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 660.00 DOWNSTREAM (FEET) = 500.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 450.00 CHANNEL SLOPE = 0.3556  
 CHANNEL BASE (FEET) = 30.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.436  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 3.79  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 3.08  
 AVERAGE FLOW DEPTH (FEET) = 0.04 TRAVEL TIME (MIN.) = 2.44  
 Tc (MIN.) = 9.12  
 SUBAREA AREA (ACRES) = 3.20 SUBAREA RUNOFF (CFS) = 6.18  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA (ACRES) = 3.50 PEAK FLOW RATE (CFS) = 6.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.06 FLOW VELOCITY (FEET/SEC.) = 3.86  
 LONGEST FLOWPATH FROM NODE 103.00 TO NODE 105.00 = 550.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 105.00 TO NODE 105.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 9.12  
 RAINFALL INTENSITY (INCH/HR) = 6.44  
 TOTAL STREAM AREA (ACRES) = 3.50  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 6.76

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.39	9.30	6.358	2.30
2	6.76	9.12	6.436	3.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.06	9.12	6.436
2	11.06	9.30	6.358

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.06 Tc(MIN.) = 9.30

TOTAL AREA(ACRES) = 5.80

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 105.00 = 700.00 FEET.

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FLOW PROCESS FROM NODE 105.00 TO NODE 106.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 500.00 DOWNSTREAM(FEET) = 478.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 200.00 CHANNEL SLOPE = 0.1100

CHANNEL BASE(FEET) = 35.00 "Z" FACTOR = 10.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.965

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 15.90

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.46

AVERAGE FLOW DEPTH(FEET) = 0.13 TRAVEL TIME(MIN.) = 0.96

Tc(MIN.) = 10.26

SUBAREA AREA(ACRES) = 5.40 SUBAREA RUNOFF(CFS) = 9.66

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 11.20 PEAK FLOW RATE(CFS) = 20.04

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.15 FLOW VELOCITY(FEET/SEC.) = 3.72

LONGEST FLOWPATH FROM NODE 100.00 TO NODE 106.00 = 900.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 11.20 TC(MIN.) = 10.26

PEAK FLOW RATE(CFS) = 20.04

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 200**

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
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Ver. 1.5A Release Date: 01/01/2003 License ID 1261

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Pre-project (on-site) \*  
\* Drainage Basin 200 \*  
\*\*\*\*\*

FILE NAME: MW200100.DAT  
TIME/DATE OF STUDY: 12:20 07/10/2009

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
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2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)						
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

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FLOW PROCESS FROM NODE 200.00 TO NODE 201.00 IS CODE = 21  
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

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\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00  
 UPSTREAM ELEVATION (FEET) = 987.50  
 DOWNSTREAM ELEVATION (FEET) = 950.00  
 ELEVATION DIFFERENCE (FEET) = 37.50  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.865  
 SUBAREA RUNOFF (CFS) = 0.47  
 TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 201.00 TO NODE 204.00 IS CODE = 51  
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>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 950.00 DOWNSTREAM (FEET) = 530.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 1405.00 CHANNEL SLOPE = 0.2989  
 CHANNEL BASE (FEET) = 20.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.602

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 9.84  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 5.06  
 AVERAGE FLOW DEPTH (FEET) = 0.10 TRAVEL TIME (MIN.) = 4.63  
 Tc (MIN.) = 11.31  
 SUBAREA AREA (ACRES) = 10.90 SUBAREA RUNOFF (CFS) = 18.32  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA (ACRES) = 11.10 PEAK FLOW RATE (CFS) = 18.65

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.15 FLOW VELOCITY (FEET/SEC.) = 6.22  
 LONGEST FLOWPATH FROM NODE 200.00 TO NODE 204.00 = 1505.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 204.00 TO NODE 204.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 11.31  
 RAINFALL INTENSITY (INCH/HR) = 5.60  
 TOTAL STREAM AREA (ACRES) = 11.10  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 18.65

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 202.00 TO NODE 203.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 90.00

UPSTREAM ELEVATION(FEET) = 865.00  
 DOWNSTREAM ELEVATION(FEET) = 825.00  
 ELEVATION DIFFERENCE(FEET) = 40.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.341  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.137  
 SUBAREA RUNOFF(CFS) = 0.49  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 203.00 TO NODE 204.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 825.00 DOWNSTREAM(FEET) = 530.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1000.00 CHANNEL SLOPE = 0.2950  
 CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.632

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.58  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.42  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 4.88  
 Tc(MIN.) = 11.22  
 SUBAREA AREA(ACRES) = 6.90 SUBAREA RUNOFF(CFS) = 11.66  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 7.10 PEAK FLOW RATE(CFS) = 12.00

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 4.58  
 LONGEST FLOWPATH FROM NODE 202.00 TO NODE 204.00 = 1090.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 204.00 TO NODE 204.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.22  
 RAINFALL INTENSITY(INCH/HR) = 5.63  
 TOTAL STREAM AREA(ACRES) = 7.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.00

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	18.65	11.31	5.602	11.10
2	12.00	11.22	5.632	7.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	30.50	11.22	5.632
2	30.59	11.31	5.602

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 30.59 Tc (MIN.) = 11.31

TOTAL AREA (ACRES) = 18.20

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 204.00 = 1505.00 FEET..

\*\*\*\*\*  
FLOW PROCESS FROM NODE 204.00 TO NODE 209.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 530.00 DOWNSTREAM (FEET) = 477.00

CHANNEL LENGTH THRU SUBAREA (FEET) = 570.00 CHANNEL SLOPE = 0.0930

CHANNEL BASE (FEET) = 15.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00

100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.170

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2900

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 35.46

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 6.34

AVERAGE FLOW DEPTH (FEET) = 0.36 TRAVEL TIME (MIN.) = 1.50

Tc (MIN.) = 12.81

SUBAREA AREA (ACRES) = 6.50 SUBAREA RUNOFF (CFS) = 9.75

AREA-AVERAGE RUNOFF COEFFICIENT = 0.297

TOTAL AREA (ACRES) = 24.70 PEAK FLOW RATE (CFS) = 37.98

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.37 FLOW VELOCITY (FEET/SEC.) = 6.50

LONGEST FLOWPATH FROM NODE 200.00 TO NODE 209.00 = 2075.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 209.00 TO NODE 209.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION (MIN.) = 12.81

RAINFALL INTENSITY (INCH/HR) = 5.17

TOTAL STREAM AREA (ACRES) = 24.70

PEAK FLOW RATE (CFS) AT CONFLUENCE = 37.98

\*\*\*\*\*  
FLOW PROCESS FROM NODE 205.00 TO NODE 206.00 IS CODE = 21

>>>>RATIONAL METHOD. INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 791.00  
 DOWNSTREAM ELEVATION(FEET) = 750.00  
 ELEVATION DIFFERENCE(FEET) = 41.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.71  
 TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 206.00 TO NODE 207.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 750.00 DOWNSTREAM(FEET) = 650.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 210.00 CHANNEL SLOPE = 0.4762  
 CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.124  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.17  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.16  
 AVERAGE FLOW DEPTH(FEET) = 0.03 TRAVEL TIME(MIN.) = 1.11  
 Tc(MIN.) = 7.79  
 SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 4.92  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 2.60 PEAK FLOW RATE(CFS) = 5.56

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 3.80  
 LONGEST FLOWPATH FROM NODE 205.00 TO NODE 207.00 = 310.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 207.00 TO NODE 208.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 650.00 DOWNSTREAM(FEET) = 578.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 470.00 CHANNEL SLOPE = 0.1532  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.338  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 18.35  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.05  
 AVERAGE FLOW DEPTH(FEET) = 0.18 TRAVEL TIME(MIN.) = 1.55  
 Tc(MIN.) = 9.34  
 SUBAREA AREA(ACRES) = 13.40 SUBAREA RUNOFF(CFS) = 25.48  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 16.00 PEAK FLOW RATE(CFS) = 30.42



END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.24 FLOW VELOCITY(FEET/SEC.) = 6.21

LONGEST FLOWPATH FROM NODE 205.00 TO NODE 208.00 = 780.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 208.00 TO NODE 209.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 578.00 DOWNSTREAM(FEET) = 477.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1070.00 CHANNEL SLOPE = 0.0944

CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 3.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.271

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2800

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 36.47

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.77

AVERAGE FLOW DEPTH(FEET) = 0.30 TRAVEL TIME(MIN.) = 3.09

Tc(MIN.) = 12.43

SUBAREA AREA(ACRES) = 8.20 SUBAREA RUNOFF(CFS) = 12.10

AREA-AVERAGE RUNOFF COEFFICIENT = 0.293

TOTAL AREA(ACRES) = 24.20 PEAK FLOW RATE(CFS) = 37.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.31 FLOW VELOCITY(FEET/SEC.) = 5.77

LONGEST FLOWPATH FROM NODE 205.00 TO NODE 209.00 = 1850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 209.00 TO NODE 209.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 12.43

RAINFALL INTENSITY(INCH/HR) = 5.27

TOTAL STREAM AREA(ACRES) = 24.20

PEAK FLOW RATE(CFS) AT CONFLUENCE = 37.40

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	37.98	12.81	5.170	24.70
2	37.40	12.43	5.271	24.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	74.65	12.43	5.271

2            74.66        12.81            5.170

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =        74.66        Tc(MIN.) =        12.81  
TOTAL AREA(ACRES) =        48.90  
LONGEST FLOWPATH FROM NODE        200.00 TO NODE        209.00 =        2075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE        209.00 TO NODE        210.00 IS CODE =        51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) =        477.00        DOWNSTREAM( FEET) =        430.00

CHANNEL LENGTH THRU SUBAREA( FEET) =        800.00        CHANNEL SLOPE =        0.0587

CHANNEL BASE( FEET) =        20.00        "Z" FACTOR =        2.000

MANNING'S FACTOR = 0.035        MAXIMUM DEPTH( FEET) =        10.00

100 YEAR RAINFALL INTENSITY( INCH/HOUR) =        4.718

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2800

S.C.S. CURVE NUMBER (AMC II) =        0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =        83.39

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) =        6.83

AVERAGE FLOW DEPTH( FEET) =        0.58        TRAVEL TIME(MIN.) =        1.95

Tc(MIN.) =        14.76

SUBAREA AREA(ACRES) =        13.20            SUBAREA RUNOFF(CFS) =        17.44

AREA-AVERAGE RUNOFF COEFFICIENT =        0.292

TOTAL AREA(ACRES) =        62.10            PEAK FLOW RATE(CFS) =        85.58

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH( FEET) =        0.58        FLOW VELOCITY( FEET/SEC.) =        6.91

LONGEST FLOWPATH FROM NODE        200.00 TO NODE        210.00 =        2875.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)        =        62.10        TC(MIN.) =        14.76

PEAK FLOW RATE(CFS)        =        85.58

=====

=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 300**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 11/05/08 \*  
\* 100-yr Pre-project (on-site) \*  
\* Drainage Basin 300 \*  
\*\*\*\*\*

FILE NAME: MWB3H100.DAT  
TIME/DATE OF STUDY: 10:53 11/14/2008

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)						
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 300.00 TO NODE 301.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00  
 UPSTREAM ELEVATION (FEET) = 822.50  
 DOWNSTREAM ELEVATION (FEET) = 780.00  
 ELEVATION DIFFERENCE (FEET) = 42.50  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.865  
 SUBAREA RUNOFF (CFS) = 0.47  
 TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 301.00 TO NODE 302.00 IS CODE = 51

>>>> COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>> TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 780.00 DOWNSTREAM (FEET) = 545.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 1005.00 CHANNEL SLOPE = 0.2338  
 CHANNEL BASE (FEET) = 20.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.934  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 10.15  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 4.58  
 AVERAGE FLOW DEPTH (FEET) = 0.11 TRAVEL TIME (MIN.) = 3.66  
 Tc (MIN.) = 10.34  
 SUBAREA AREA (ACRES) = 10.60 SUBAREA RUNOFF (CFS) = 18.87  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA (ACRES) = 10.80 PEAK FLOW RATE (CFS) = 19.23

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.16 FLOW VELOCITY (FEET/SEC.) = 6.01  
 LONGEST FLOWPATH FROM NODE 300.00 TO NODE 302.00 = 1105.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 302.00 TO NODE 306.00 IS CODE = 51

>>>> COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>> TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 545.00 DOWNSTREAM (FEET) = 426.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 1330.00 CHANNEL SLOPE = 0.0895  
 CHANNEL BASE (FEET) = 30.00 "Z" FACTOR = 3.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.672  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 35.09  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 4.77  
 AVERAGE FLOW DEPTH (FEET) = 0.24 TRAVEL TIME (MIN.) = 4.65  
 Tc (MIN.) = 14.99  
 SUBAREA AREA (ACRES) = 24.00 SUBAREA RUNOFF (CFS) = 31.39  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.286  
 TOTAL AREA (ACRES) = 34.80 PEAK FLOW RATE (CFS) = 46.53

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.28 FLOW VELOCITY(FEET/SEC.) = 5.40

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 306.00 = 2435.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 306.00 TO NODE 306.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 14.99

RAINFALL INTENSITY(INCH/HR) = 4.67

TOTAL STREAM AREA(ACRES) = 34.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 46.53

\*\*\*\*\*

FLOW PROCESS FROM NODE 303.00 TO NODE 304.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 827.00

DOWNSTREAM ELEVATION(FEET) = 810.00

ELEVATION DIFFERENCE(FEET) = 17.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865

SUBAREA RUNOFF(CFS) = 0.47

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*

FLOW PROCESS FROM NODE 304.00 TO NODE 305.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 810.00 DOWNSTREAM(FEET) = 540.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 928.00 CHANNEL SLOPE = 0.2909

CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.379

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.82

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.03

AVERAGE FLOW DEPTH(FEET) = 0.14 TRAVEL TIME(MIN.) = 2.56

Tc(MIN.) = 9.25

SUBAREA AREA(ACRES) = 8.60 SUBAREA RUNOFF(CFS) = 16.46

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 8.80 PEAK FLOW RATE(CFS) = 16.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.21 FLOW VELOCITY (FEET/SEC.) = 7.74

LONGEST FLOWPATH FROM NODE 303.00 TO NODE 305.00 = 1028.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 305.00 TO NODE 306.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 540.00 DOWNSTREAM (FEET) = 426.00

CHANNEL LENGTH THRU SUBAREA (FEET) = 1300.00 CHANNEL SLOPE = 0.0877

CHANNEL BASE (FEET) = 20.00 "Z" FACTOR = 3.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00

100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.988

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2900

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 27.70

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 5.04

AVERAGE FLOW DEPTH (FEET) = 0.26 TRAVEL TIME (MIN.) = 4.30

Tc (MIN.) = 13.54

SUBAREA AREA (ACRES) = 14.90 SUBAREA RUNOFF (CFS) = 21.55

AREA-AVERAGE RUNOFF COEFFICIENT = 0.294

TOTAL AREA (ACRES) = 23.70 PEAK FLOW RATE (CFS) = 34.72

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.30 FLOW VELOCITY (FEET/SEC.) = 5.49

LONGEST FLOWPATH FROM NODE 303.00 TO NODE 306.00 = 2328.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 306.00 TO NODE 306.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION (MIN.) = 13.54

RAINFALL INTENSITY (INCH/HR) = 4.99

TOTAL STREAM AREA (ACRES) = 23.70

PEAK FLOW RATE (CFS) AT CONFLUENCE = 34.72

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	46.53	14.99	4.672	34.80
2	34.72	13.54	4.988	23.70

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	76.76	13.54	4.988
2	79.05	14.99	4.672

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 79.05 Tc(MIN.) = 14.99

TOTAL AREA(ACRES) = 58.50

LONGEST FLOWPATH FROM NODE 300.00 TO NODE 306.00 = 2435.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 58.50 TC(MIN.) = 14.99

PEAK FLOW RATE(CFS) = 79.05

=====

=====

END OF RATIONAL METHOD ANALYSIS



## **Drainage Basin 400**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2003 Advanced Engineering Software (aes)

Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY

5620 Friars Road

San Diego, California 92110

619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* MEADOWOOD J-15956 11/05/08 \*  
\* 100-yr Pre-project (on-site) \*  
\* Drainage Basin 400 \*  
\*\*\*\*\*

FILE NAME: 400.DAT

TIME/DATE OF STUDY: 11:05 11/07/2008

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00

6-HOUR DURATION PRECIPITATION (INCHES) = 3.600

SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN

OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 400.00 TO NODE 401.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
=====

\*USER SPECIFIED(SUBAREA) :

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 506.00  
 DOWNSTREAM ELEVATION(FEET) = 480.00  
 ELEVATION DIFFERENCE(FEET) = 26.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN  $T_c$  CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 401.00 TO NODE 402.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 480.00 DOWNSTREAM(FEET) = 430.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 305.00 CHANNEL SLOPE = 0.1639  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.717

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.10

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.74

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.85

$T_c$ (MIN.) = 8.54

SUBAREA AREA(ACRES) = 1.60 SUBAREA RUNOFF(CFS) = 3.22

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 1.80 PEAK FLOW RATE(CFS) = 3.63

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 3.43

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 402.00 = 405.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 402.00 TO NODE 403.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 430.00 DOWNSTREAM(FEET) = 384.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 925.00 CHANNEL SLOPE = 0.0497  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 5.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.377

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2800

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.70

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.38

AVERAGE FLOW DEPTH(FEET) = 0.46 TRAVEL TIME(MIN.) = 3.52

$T_c$ (MIN.) = 12.06

SUBAREA AREA(ACRES) = 9.30 SUBAREA RUNOFF(CFS) = 14.00

AREA-AVERAGE RUNOFF COEFFICIENT = 0.283

TOTAL AREA(ACRES) = 11.10 PEAK FLOW RATE(CFS) = 16.90

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH( FEET ) = 0.58      FLOW VELOCITY( FEET/SEC. ) = 4.98

LONGEST FLOWPATH FROM NODE 400.00 TO NODE 403.00 = 1330.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA( ACRES )      =      11.10      TC( MIN. ) =      12.06

PEAK FLOW RATE( CFS )      =      16.90

=====

=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 700A**

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RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
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Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Pre-project (on-site) \*  
\* Drainage Basin 700A \*  
\*\*\*\*\*

FILE NAME: MW700A00.DAT  
TIME/DATE OF STUDY: 20:19 07/16/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
NO.	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 700.00 TO NODE 701.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA) :  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 770.00  
 DOWNSTREAM ELEVATION(FEET) = 740.00  
 ELEVATION DIFFERENCE(FEET) = 30.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 1.42  
 TOTAL AREA(ACRES) = 0.60 TOTAL RUNOFF(CFS) = 1.42

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 701.00 TO NODE 702.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 740.00 DOWNSTREAM(FEET) = 350.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 2230.00 CHANNEL SLOPE = 0.1749  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 4.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 5.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.942  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 37.27  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.21  
 AVERAGE FLOW DEPTH(FEET) = 0.65 TRAVEL TIME(MIN.) = 3.64  
 Tc(MIN.) = 10.33  
 SUBAREA AREA(ACRES) = 38.40 SUBAREA RUNOFF(CFS) = 70.73  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.310  
 TOTAL AREA(ACRES) = 39.00 PEAK FLOW RATE(CFS) = 71.80

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.90 FLOW VELOCITY(FEET/SEC.) = 12.18  
 LONGEST FLOWPATH FROM NODE 700.00 TO NODE 702.00 = 2330.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 702.00 TO NODE 704.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 350.00 DOWNSTREAM(FEET) = 339.10  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 330.00 CHANNEL SLOPE = 0.0330  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 3.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.643  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 78.10  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.41  
 AVERAGE FLOW DEPTH(FEET) = 0.95 TRAVEL TIME(MIN.) = 0.86  
 Tc(MIN.) = 11.18  
 SUBAREA AREA(ACRES) = 7.20 SUBAREA RUNOFF(CFS) = 12.60  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.310  
 TOTAL AREA(ACRES) = 46.20 PEAK FLOW RATE(CFS) = 80.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.96 FLOW VELOCITY(FEET/SEC.) = 6.50

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 704.00 = 2660.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 704.00 TO NODE 710.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 339.10 DOWNSTREAM(FEET) = 327.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 190.00 CHANNEL SLOPE = 0.0637

CHANNEL BASE(FEET) = 4.00 "Z" FACTOR = 3.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.532

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3100

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 81.13

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.06

AVERAGE FLOW DEPTH(FEET) = 1.19 TRAVEL TIME(MIN.) = 0.35

Tc(MIN.) = 11.53

SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 0.69

AREA-AVERAGE RUNOFF COEFFICIENT = 0.310

TOTAL AREA(ACRES) = 46.60 PEAK FLOW RATE(CFS) = 80.79

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.18 FLOW VELOCITY(FEET/SEC.) = 9.08

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 710.00 = 2850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 710.00 TO NODE 710.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 11.53

RAINFALL INTENSITY(INCH/HR) = 5.53

TOTAL STREAM AREA(ACRES) = 46.60

PEAK FLOW RATE(CFS) AT CONFLUENCE = 80.79

\*\*\*\*\*

FLOW PROCESS FROM NODE 706.00 TO NODE 708.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 538.00

DOWNSTREAM ELEVATION(FEET) = 520.00

ELEVATION DIFFERENCE(FEET) = 18.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.601

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!



100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.929  
 SUBAREA RUNOFF (CFS) = 0.74  
 TOTAL AREA (ACRES) = 0.30 TOTAL RUNOFF (CFS) = 0.74

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 708.00 TO NODE 710.00 IS CODE = 51  
 -----

>>>> COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>> TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) =	520.00	DOWNSTREAM (FEET) =	327.00
CHANNEL LENGTH THRU SUBAREA (FEET) =	1400.00	CHANNEL SLOPE =	0.1379
CHANNEL BASE (FEET) =	10.00	"Z" FACTOR =	14.000
MANNING'S FACTOR =	0.035	MAXIMUM DEPTH (FEET) =	10.00
100 YEAR RAINFALL INTENSITY (INCH/HOUR) =	5.615		

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3100

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 14.25

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 5.00

AVERAGE FLOW DEPTH (FEET) = 0.22 TRAVEL TIME (MIN.) = 4.67

Tc (MIN.) = 11.27

SUBAREA AREA (ACRES) = 15.20 SUBAREA RUNOFF (CFS) = 26.46

AREA-AVERAGE RUNOFF COEFFICIENT = 0.310

TOTAL AREA (ACRES) = 15.50 PEAK FLOW RATE (CFS) = 26.98

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.31 FLOW VELOCITY (FEET/SEC.) = 6.07

LONGEST FLOWPATH FROM NODE 706.00 TO NODE 710.00 = 1500.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 710.00 TO NODE 710.00 IS CODE = 1  
 -----

>>>> DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>> AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 11.27  
 RAINFALL INTENSITY (INCH/HR) = 5.62  
 TOTAL STREAM AREA (ACRES) = 15.50  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 26.98

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	80.79	11.53	5.532	46.60
2	26.98	11.27	5.615	15.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	105.93	11.27	5.615
2	107.37	11.53	5.532

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 107.37 Tc(MIN.) = 11.53

TOTAL AREA(ACRES) = 62.10

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 710.00 = 2850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 710.00 TO NODE 712.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 327.00 DOWNSTREAM(FEET) = 290.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 730.00 CHANNEL SLOPE = 0.0507

CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 4.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.140

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3100

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 115.18

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.74

AVERAGE FLOW DEPTH(FEET) = 1.58 TRAVEL TIME(MIN.) = 1.39

Tc(MIN.) = 12.92

SUBAREA AREA(ACRES) = 9.80 SUBAREA RUNOFF(CFS) = 15.62

AREA-AVERAGE RUNOFF COEFFICIENT = 0.310

TOTAL AREA(ACRES) = 71.90 PEAK FLOW RATE(CFS) = 114.55

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.58 FLOW VELOCITY(FEET/SEC.) = 8.75

LONGEST FLOWPATH FROM NODE 700.00 TO NODE 712.00 = 3580.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 712.00 TO NODE 712.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.92

RAINFALL INTENSITY(INCH/HR) = 5.14

TOTAL STREAM AREA(ACRES) = 71.90

PEAK FLOW RATE(CFS) AT CONFLUENCE = 114.55

Flow Information From Node Number 506

\*\*\*\*\*

FLOW PROCESS FROM NODE 506.00 TO NODE 506.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 17.18 RAIN INTENSITY(INCH/HOUR) = 4.28

TOTAL AREA(ACRES) = 88.10 TOTAL RUNOFF(CFS) = 110.57

\*\*\*\*\*  
FLOW PROCESS FROM NODE 712.00 TO NODE 712.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	17.18
RAINFALL INTENSITY(INCH/HR) =	4.28
TOTAL STREAM AREA(ACRES) =	88.10
PEAK FLOW RATE(CFS) AT CONFLUENCE =	110.57

+-----+  
| Flow Information From Node Number 604 |  
+-----+

\*\*\*\*\*  
FLOW PROCESS FROM NODE 712.00 TO NODE 712.00 IS CODE = 7

-----  
>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:			
TC(MIN) =	15.71	RAIN INTENSITY(INCH/HOUR) =	4.53
TOTAL AREA(ACRES) =	32.00	TOTAL RUNOFF(CFS) =	38.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 712.00 TO NODE 712.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:	
TIME OF CONCENTRATION(MIN.) =	15.71
RAINFALL INTENSITY(INCH/HR) =	4.53
TOTAL STREAM AREA(ACRES) =	32.00
PEAK FLOW RATE(CFS) AT CONFLUENCE =	38.05

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	114.55	12.92	5.140	71.90
2	110.57	17.18	4.278	88.10
3	38.05	15.71	4.533	32.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	229.03	12.92	5.140
2	240.16	15.71	4.533

3            241.82        17.18            4.278

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =        241.82    Tc(MIN.) =        17.18

TOTAL AREA(ACRES) =        192.00

LONGEST FLOWPATH FROM NODE        700.00 TO NODE        712.00 =    3580.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES)        =        192.00    TC(MIN.) =        17.18

PEAK FLOW RATE(CFS)        =        241.82

=====

=====

END OF RATIONAL METHOD ANALYSIS

**Flow Information For Drainage  
Basin 700 A  
(Node 506)**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

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San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956, July 2009 \*  
\* 100-yr Pre-project (on-site) \*  
\* (Node 506) \*  
\*\*\*\*\*

FILE NAME: MW500100.DAT  
TIME/DATE OF STUDY: 12:30 07/10/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS  
\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*  
    HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING  
    WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR  
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)  
== =====  
1 30.0 20.0 0.018/0.018/0.020 0.67 2.00 0.0313 0.167 0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 500.00 TO NODE 501.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 800.00  
 DOWNSTREAM ELEVATION(FEET) = 750.00  
 ELEVATION DIFFERENCE(FEET) = 50.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 501.00 TO NODE 502.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 750.00 DOWNSTREAM(FEET) = 600.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 350.00 CHANNEL SLOPE = 0.4286  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 3.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.078

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.87

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.91

AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.19

Tc(MIN.) = 7.87

SUBAREA AREA(ACRES) = 3.20 SUBAREA RUNOFF(CFS) = 6.79

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 3.40 PEAK FLOW RATE(CFS) = 7.22

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.11 FLOW VELOCITY(FEET/SEC.) = 5.93

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 502.00 = 450.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 502.00 TO NODE 503.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 600.00 DOWNSTREAM(FEET) = 500.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 560.00 CHANNEL SLOPE = 0.1786  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 3.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.318

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.21

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.15

AVERAGE FLOW DEPTH(FEET) = 0.30 TRAVEL TIME(MIN.) = 1.52

Tc(MIN.) = 9.39

SUBAREA AREA(ACRES) = 4.20 SUBAREA RUNOFF(CFS) = 7.96

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 7.60 PEAK FLOW RATE(CFS) = 14.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.34 FLOW VELOCITY(FEET/SEC.) = 6.61

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 503.00 = 1010.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 503.00 TO NODE 504.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 500.00 DOWNSTREAM(FEET) = 366.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 1840.00 CHANNEL SLOPE = 0.0728

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 10.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 3.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.923

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 61.67

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.92

AVERAGE FLOW DEPTH(FEET) = 0.81 TRAVEL TIME(MIN.) = 4.43

Tc(MIN.) = 13.82

SUBAREA AREA(ACRES) = 63.40 SUBAREA RUNOFF(CFS) = 93.64

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 71.00 PEAK FLOW RATE(CFS) = 104.87

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.01 FLOW VELOCITY(FEET/SEC.) = 7.90

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 504.00 = 2850.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 504.00 TO NODE 505.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 366.00 DOWNSTREAM(FEET) = 334.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 420.00 CHANNEL SLOPE = 0.0762

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 10.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.734

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2800

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 108.18

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.07

AVERAGE FLOW DEPTH(FEET) = 1.02 TRAVEL TIME(MIN.) = 0.87

Tc(MIN.) = 14.69

SUBAREA AREA(ACRES) = 5.00 SUBAREA RUNOFF(CFS) = 6.63

AREA-AVERAGE RUNOFF COEFFICIENT = 0.299

TOTAL AREA(ACRES) = 76.00 PEAK FLOW RATE(CFS) = 107.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.01 FLOW VELOCITY(FEET/SEC.) = 8.10

LONGEST FLOWPATH FROM NODE 500.00 TO NODE 505.00 = 3270.00 FEET.



```

*****
FLOW PROCESS FROM NODE      505.00 TO NODE      506.00 IS CODE =  51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) =    334.00  DOWNSTREAM( FEET) =    303.00
CHANNEL LENGTH THRU SUBAREA( FEET) =    910.00  CHANNEL SLOPE =    0.0341
CHANNEL BASE( FEET) =      0.00  "Z" FACTOR =    10.000
MANNING'S FACTOR = 0.035  MAXIMUM DEPTH( FEET) =     3.00
  100 YEAR RAINFALL INTENSITY( INCH/HOUR) =    4.278
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2600
S.C.S. CURVE NUMBER (AMC II) =    0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    114.19
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) =     6.08
AVERAGE FLOW DEPTH( FEET) =     1.37  TRAVEL TIME( MIN.) =     2.49
Tc( MIN.) =    17.18
SUBAREA AREA( ACRES) =     12.10      SUBAREA RUNOFF( CFS) =    13.46
AREA-AVERAGE RUNOFF COEFFICIENT =    0.293
TOTAL AREA( ACRES) =     88.10      PEAK FLOW RATE( CFS) =    110.57

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH( FEET) =     1.36  FLOW VELOCITY( FEET/SEC.) =     6.02
LONGEST FLOWPATH FROM NODE      500.00 TO NODE      506.00 =  4180.00 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA( ACRES)      =     88.10  TC( MIN.) =     17.18
PEAK FLOW RATE( CFS)    =    110.57
=====
=====
END OF RATIONAL METHOD ANALYSIS

```

**Flow Information For Drainage  
Basin 700 A  
(Node 604)**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
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Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 11/05/08 \*  
\* 100-yr Pre-project (on-site) \*  
\* (Node 604) \*  
\*\*\*\*\*

FILE NAME: MW600100.DAT  
TIME/DATE OF STUDY: 08:08 03/18/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH LIP HIKE	MANNING FACTOR
NO.	(FT)	(FT)		(FT)	(FT) (FT) (FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313 0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)  
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)  
\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 600.00 TO NODE 601.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA) :  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00  
 UPSTREAM ELEVATION (FEET) = 502.00  
 DOWNSTREAM ELEVATION (FEET) = 490.00  
 ELEVATION DIFFERENCE (FEET) = 12.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.865  
 SUBAREA RUNOFF (CFS) = 0.47  
 TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 601.00 TO NODE 602.00 IS CODE = 51

>>>> COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>> TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 490.00 DOWNSTREAM (FEET) = 370.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 530.00 CHANNEL SLOPE = 0.2264  
 CHANNEL BASE (FEET) = 20.00 "Z" FACTOR = 20.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.726  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 1.52  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 2.08  
 AVERAGE FLOW DEPTH (FEET) = 0.04 TRAVEL TIME (MIN.) = 4.25  
 Tc (MIN.) = 10.93  
 SUBAREA AREA (ACRES) = 1.20 SUBAREA RUNOFF (CFS) = 2.06  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA (ACRES) = 1.40 PEAK FLOW RATE (CFS) = 2.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.04 FLOW VELOCITY (FEET/SEC.) = 2.69  
 LONGEST FLOWPATH FROM NODE 600.00 TO NODE 602.00 = 630.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 602.00 TO NODE 603.00 IS CODE = 51

>>>> COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>> TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 370.00 DOWNSTREAM (FEET) = 300.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 480.00 CHANNEL SLOPE = 0.1458  
 CHANNEL BASE (FEET) = 3.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 2.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.154  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 3.73  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 4.13  
 AVERAGE FLOW DEPTH (FEET) = 0.19 TRAVEL TIME (MIN.) = 1.94  
 Tc (MIN.) = 12.87  
 SUBAREA AREA (ACRES) = 1.90 SUBAREA RUNOFF (CFS) = 2.64  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.283  
 TOTAL AREA (ACRES) = 3.30 PEAK FLOW RATE (CFS) = 4.81

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.21 FLOW VELOCITY(FEET/SEC.) = 4.52

LONGEST FLOWPATH FROM NODE 600.00 TO NODE 603.00 = 1110.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 603.00 TO NODE 604.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 300.00 DOWNSTREAM(FEET) = 285.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 530.00 CHANNEL SLOPE = 0.0283

CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 20.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.533

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2600

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.83

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.12

AVERAGE FLOW DEPTH(FEET) = 0.52 TRAVEL TIME(MIN.) = 2.84

Tc(MIN.) = 15.71

SUBAREA AREA(ACRES) = 28.70 SUBAREA RUNOFF(CFS) = 33.82

AREA-AVERAGE RUNOFF COEFFICIENT = 0.262

TOTAL AREA(ACRES) = 32.00 PEAK FLOW RATE(CFS) = 38.05

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.65 FLOW VELOCITY(FEET/SEC.) = 3.63

LONGEST FLOWPATH FROM NODE 600.00 TO NODE 604.00 = 1640.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 32.00 TC(MIN.) = 15.71

PEAK FLOW RATE(CFS) = 38.05

=====

=====

END OF RATIONAL METHOD ANALYSIS

**Drainage Basin 700B**  
**(700A & 700B Combined)**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
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Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Pre-project (on-site) \*  
\* Drainage Basin 700A and 700B Combined \*  
\*\*\*\*\*

FILE NAME: MW700AB.DAT  
TIME/DATE OF STUDY: 14:25 08/13/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 750.00 TO NODE 751.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 800.00  
 DOWNSTREAM ELEVATION(FEET) = 740.00  
 ELEVATION DIFFERENCE(FEET) = 60.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 2.12  
 TOTAL AREA(ACRES) = 0.90 TOTAL RUNOFF(CFS) = 2.12

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 751.00 TO NODE 752.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 740.00 DOWNSTREAM(FEET) = 296.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1180.00 CHANNEL SLOPE = 0.3763  
 CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 3.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.599  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.46  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 9.41  
 AVERAGE FLOW DEPTH(FEET) = 0.25 TRAVEL TIME(MIN.) = 2.09  
 Tc(MIN.) = 8.77  
 SUBAREA AREA(ACRES) = 11.00 SUBAREA RUNOFF(CFS) = 22.50  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.309  
 TOTAL AREA(ACRES) = 11.90 PEAK FLOW RATE(CFS) = 24.28

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.35 FLOW VELOCITY(FEET/SEC.) = 11.54  
 LONGEST FLOWPATH FROM NODE 750.00 TO NODE 752.00 = 1280.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 752.00 TO NODE 753.00 IS CODE = 51

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 296.00 DOWNSTREAM(FEET) = 272.50  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 730.00 CHANNEL SLOPE = 0.0322  
 CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.614  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 52.14  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.87  
 AVERAGE FLOW DEPTH(FEET) = 0.90 TRAVEL TIME(MIN.) = 2.50  
 Tc(MIN.) = 11.27  
 SUBAREA AREA(ACRES) = 31.90 SUBAREA RUNOFF(CFS) = 55.52  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.310  
 TOTAL AREA(ACRES) = 43.80 PEAK FLOW RATE(CFS) = 76.18



END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 1.05 FLOW VELOCITY(FEET/SEC.) = 5.37

LONGEST FLOWPATH FROM NODE 750.00 TO NODE 753.00 = 2010.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 753.00 TO NODE 753.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 11.27

RAINFALL INTENSITY(INCH/HR) = 5.61

TOTAL STREAM AREA(ACRES) = 43.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 76.18

+-----+

| Flow Information from Node 712 |

| |

| |

+-----+

\*\*\*\*\*

FLOW PROCESS FROM NODE 712.00 TO NODE 712.00 IS CODE = 7

>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 17.18 RAIN INTENSITY(INCH/HOUR) = 4.28

TOTAL AREA(ACRES) = 192.00 TOTAL RUNOFF(CFS) = 241.82

\*\*\*\*\*

FLOW PROCESS FROM NODE 712.00 TO NODE 712.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 17.18

RAINFALL INTENSITY(INCH/HR) = 4.28

TOTAL STREAM AREA(ACRES) = 192.00

PEAK FLOW RATE(CFS) AT CONFLUENCE = 241.82

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	76.18	11.27	5.614	43.80
2	241.82	17.18	4.278	192.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
------------------	-----------------	--------------	--------------------------

1	234.86	11.27	5.614
2	299.87	17.18	4.278

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 299.87 Tc(MIN.) = 17.18

TOTAL AREA(ACRES) = 235.80

LONGEST FLOWPATH FROM NODE 750.00 TO NODE 712.00 = 2010.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 235.80 TC(MIN.) = 17.18

PEAK FLOW RATE(CFS) = 299.87

=====

=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 800**

\*\*\*\*\*

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Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
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Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 11/05/08 \*  
\* 100-yr Pre-project (on-site) \*  
\* Drainage Basin 800 \*  
\*\*\*\*\*

FILE NAME: MW800100.DAT  
TIME/DATE OF STUDY: 16:25 03/17/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)						
===	=====	=====	=====	=====	=====	=====	=====	=====
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 800.00 TO NODE 810.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 825.00  
 DOWNSTREAM ELEVATION(FEET) = 800.00  
 ELEVATION DIFFERENCE(FEET) = 25.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.200  
 SUBAREA RUNOFF(CFS) = 0.57  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 810.00 TO NODE 820.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 800.00 DOWNSTREAM(FEET) = 281.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 910.00 CHANNEL SLOPE = 0.5703  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.023  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 29.88  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.92  
 AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 1.70  
 Tc(MIN.) = 7.97  
 SUBAREA AREA(ACRES) = 25.10 SUBAREA RUNOFF(CFS) = 58.17  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.330  
 TOTAL AREA(ACRES) = 25.30 PEAK FLOW RATE(CFS) = 58.66

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.23 FLOW VELOCITY(FEET/SEC.) = 11.34  
 LONGEST FLOWPATH FROM NODE 800.00 TO NODE 820.00 = 1010.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 820.00 TO NODE 830.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 281.00 DOWNSTREAM(FEET) = 263.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 800.00 CHANNEL SLOPE = 0.0225  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.666  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2600  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 77.52  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.24  
 AVERAGE FLOW DEPTH(FEET) = 0.68 TRAVEL TIME(MIN.) = 3.15  
 Tc(MIN.) = 11.11  
 SUBAREA AREA(ACRES) = 25.40 SUBAREA RUNOFF(CFS) = 37.42  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.295  
 TOTAL AREA(ACRES) = 50.70 PEAK FLOW RATE(CFS) = 84.75

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH( FEET ) = 0.71 FLOW VELOCITY( FEET/SEC. ) = 4.37

LONGEST FLOWPATH FROM NODE 800.00 TO NODE 830.00 = 1810.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA( ACRES ) = 50.70 TC( MIN. ) = 11.11

PEAK FLOW RATE( CFS ) = 84.75

=====

=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 900**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2003 Advanced Engineering Software (aes)

Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY

5620 Friars Road

San Diego, California 92110

619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* MEADOWOOD J-15956 \*  
\* 05/12/2009 PRE-PROJECT \*  
\* 100-YR BASIN 900 \*  
\*\*\*\*\*

FILE NAME: B900.DAT

TIME/DATE OF STUDY: 15:20 05/13/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00

6-HOUR DURATION PRECIPITATION (INCHES) = 3.600

SPECIFIED MINIMUM PIPE SIZE(INCH) = 30.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN

OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 901.00 TO NODE 905.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0



INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 710.00  
 DOWNSTREAM ELEVATION(FEET) = 640.00  
 ELEVATION DIFFERENCE(FEET) = 70.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.200  
 SUBAREA RUNOFF(CFS) = 0.57  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 905.00 TO NODE 910.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 640.00 DOWNSTREAM(FEET) = 275.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 980.00 CHANNEL SLOPE = 0.3724  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.164  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3400  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.56  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.69  
 AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 3.49  
 Tc(MIN.) = 9.75  
 SUBAREA AREA(ACRES) = 6.60 SUBAREA RUNOFF(CFS) = 13.83  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.340  
 TOTAL AREA(ACRES) = 6.80 PEAK FLOW RATE(CFS) = 14.26

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 5.49  
 LONGEST FLOWPATH FROM NODE 901.00 TO NODE 910.00 = 1080.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 910.00 TO NODE 915.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 275.00 DOWNSTREAM(FEET) = 263.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1500.00 CHANNEL SLOPE = 0.0080  
 CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 1.500  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.50  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 4.503  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 27.48  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.09  
 AVERAGE FLOW DEPTH(FEET) = 1.55 TRAVEL TIME(MIN.) = 6.12  
 Tc(MIN.) = 15.87  
 SUBAREA AREA(ACRES) = 14.60 SUBAREA RUNOFF(CFS) = 26.30  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.381  
 TOTAL AREA(ACRES) = 21.40 PEAK FLOW RATE(CFS) = 36.71

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 1.78      FLOW VELOCITY (FEET/SEC.) = 4.41

LONGEST FLOWPATH FROM NODE 901.00 TO NODE 915.00 = 2580.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 21.40      TC (MIN.) = 15.87

PEAK FLOW RATE (CFS) = 36.71

=====

=====

END OF RATIONAL METHOD ANALYSIS

## **Appendix C**

### **100-Year Post-Project Modified Rational Method Analyses**

## **Drainage Basin 1000**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE

Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT

2003,1985,1981 HYDROLOGY MANUAL

(c) Copyright 1982-2003 Advanced Engineering Software (aes)

Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY

5620 Friars Road

San Diego, California 92110

619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*

\* MEADOWOOD J-15956 11/12/08 \*

\* 100-yr Post-project (on-site) \*

\* Drainage Basin 1000 \*

\*\*\*\*\*

FILE NAME: MW\_1K100.DAT

TIME/DATE OF STUDY: 11:25 01/09/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00

6-HOUR DURATION PRECIPITATION (INCHES) = 3.600

SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00

SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90

SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD

NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH	LIP	HIKE	MANNING FACTOR
NO.	(FT)	(FT)		(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.020/0.020/0.020	0.50	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = -0.10 FEET

as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)

2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN

OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 1000.00 TO NODE 1001.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 813.00  
 DOWNSTREAM ELEVATION(FEET) = 780.00  
 ELEVATION DIFFERENCE(FEET) = 33.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1001.00 TO NODE 1005.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 780.00 DOWNSTREAM(FEET) = 500.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 600.00 CHANNEL SLOPE = 0.4667  
 CHANNEL BASE(FEET) = 15.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.358

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.48  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.83  
 AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 2.61  
 Tc(MIN.) = 9.30

SUBAREA AREA(ACRES) = 2.10 SUBAREA RUNOFF(CFS) = 4.01  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 2.30 PEAK FLOW RATE(CFS) = 4.39

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 4.54  
 LONGEST FLOWPATH FROM NODE 1000.00 TO NODE 1005.00 = 700.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1005.00 TO NODE 1005.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.30  
 RAINFALL INTENSITY(INCH/HR) = 6.36  
 TOTAL STREAM AREA(ACRES) = 2.30  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.39

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1003.00 TO NODE 1004.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 694.00  
 DOWNSTREAM ELEVATION(FEET) = 660.00  
 ELEVATION DIFFERENCE(FEET) = 34.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.71  
 TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1004.00 TO NODE 1005.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 660.00 DOWNSTREAM(FEET) = 500.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 450.00 CHANNEL SLOPE = 0.3556  
 CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.436

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.79

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.08

AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 2.44

Tc(MIN.) = 9.12

SUBAREA AREA(ACRES) = 3.20 SUBAREA RUNOFF(CFS) = 6.18

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 3.50 PEAK FLOW RATE(CFS) = 6.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 3.86

LONGEST FLOWPATH FROM NODE 1003.00 TO NODE 1005.00 = 550.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1005.00 TO NODE 1005.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.12  
 RAINFALL INTENSITY(INCH/HR) = 6.44  
 TOTAL STREAM AREA(ACRES) = 3.50  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.76

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.39	9.30	6.358	2.30
2	6.76	9.12	6.436	3.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.06	9.12	6.436
2	11.06	9.30	6.358

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.06 Tc(MIN.) = 9.30  
 TOTAL AREA(ACRES) = 5.80  
 LONGEST FLOWPATH FROM NODE 1000.00 TO NODE 1005.00 = 700.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1005.00 TO NODE 1006.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 500.00 DOWNSTREAM(FEET) = 480.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 100.00 CHANNEL SLOPE = 0.2000  
 CHANNEL BASE(FEET) = 35.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.179  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.58  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.97  
 AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 0.42  
 Tc(MIN.) = 9.72  
 SUBAREA AREA(ACRES) = 3.80 SUBAREA RUNOFF(CFS) = 7.04  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 9.60 PEAK FLOW RATE(CFS) = 17.80

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.11 FLOW VELOCITY(FEET/SEC.) = 4.42  
 LONGEST FLOWPATH FROM NODE 1000.00 TO NODE 1006.00 = 800.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 1006.00 TO NODE 1011.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 480.00 DOWNSTREAM(FEET) = 458.00  
 FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 17.51  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 17.80  
 PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 9.95  
 LONGEST FLOWPATH FROM NODE 1000.00 TO NODE 1011.00 = 1050.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 9.60 TC(MIN.) = 9.95  
 PEAK FLOW RATE(CFS) = 17.80



=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 2000**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 11/12/08 \*  
\* 100-yr Post-project (on-site) \*  
\* Drainage Basin 2000 \*  
\*\*\*\*\*

FILE NAME: MW\_2K100.DAT  
TIME/DATE OF STUDY: 11:40 01/12/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)						
1	30.0	20.0	0.020/0.020/0.020	0.50	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = -0.10 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2000.00 TO NODE 2001.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA) :  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 987.50  
 DOWNSTREAM ELEVATION(FEET) = 950.00  
 ELEVATION DIFFERENCE(FEET) = 37.50  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2001.00 TO NODE 2004.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 950.00 DOWNSTREAM(FEET) = 530.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1405.00 CHANNEL SLOPE = 0.2989  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.602

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.84

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.06

AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 4.63

Tc(MIN.) = 11.31

SUBAREA AREA(ACRES) = 10.90 SUBAREA RUNOFF(CFS) = 18.32

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 11.10 PEAK FLOW RATE(CFS) = 18.65

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.15 FLOW VELOCITY(FEET/SEC.) = 6.22

LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2004.00 = 1505.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2004.00 TO NODE 2004.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 11.31

RAINFALL INTENSITY(INCH/HR) = 5.60

TOTAL STREAM AREA(ACRES) = 11.10

PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.65

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2002.00 TO NODE 2003.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 =====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00

UPSTREAM ELEVATION(FEET) = 865.00  
 DOWNSTREAM ELEVATION(FEET) = 825.00  
 ELEVATION DIFFERENCE(FEET) = 40.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.341  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.137  
 SUBAREA RUNOFF(CFS) = 0.49  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2003.00 TO NODE 2004.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 825.00 DOWNSTREAM(FEET) = 530.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1000.00 CHANNEL SLOPE = 0.2950  
 CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.632

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.58  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.42  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 4.88  
 Tc(MIN.) = 11.22  
 SUBAREA AREA(ACRES) = 6.90 SUBAREA RUNOFF(CFS) = 11.66  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 7.10 PEAK FLOW RATE(CFS) = 12.00

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.09 FLOW VELOCITY(FEET/SEC.) = 4.58  
 LONGEST FLOWPATH FROM NODE 2002.00 TO NODE 2004.00 = 1090.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2004.00 TO NODE 2004.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.22  
 RAINFALL INTENSITY(INCH/HR) = 5.63  
 TOTAL STREAM AREA(ACRES) = 7.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.00

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	18.65	11.31	5.602	11.10
2	12.00	11.22	5.632	7.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	30.50	11.22	5.632
2	30.59	11.31	5.602

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 30.59 Tc(MIN.) = 11.31  
 TOTAL AREA(ACRES) = 18.20  
 LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2004.00 = 1505.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2004.00 TO NODE 2009.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 530.00 DOWNSTREAM( FEET) = 512.00  
 CHANNEL LENGTH THRU SUBAREA( FEET) = 180.00 CHANNEL SLOPE = 0.1000  
 CHANNEL BASE( FEET) = 15.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH( FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY( INCH/HOUR) = 5.456  
 \*USER SPECIFIED( SUBAREA) :  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
 S.C.S. CURVE NUMBER ( AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS) = 33.99  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 6.37  
 AVERAGE FLOW DEPTH( FEET) = 0.34 TRAVEL TIME( MIN.) = 0.47  
 Tc( MIN.) = 11.78  
 SUBAREA AREA( ACRES) = 4.30 SUBAREA RUNOFF( CFS) = 6.80  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.298  
 TOTAL AREA( ACRES) = 22.50 PEAK FLOW RATE( CFS) = 36.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH( FEET) = 0.36 FLOW VELOCITY( FEET/SEC.) = 6.55  
 LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2009.00 = 1685.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2009.00 TO NODE 2010.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 512.00 DOWNSTREAM( FEET) = 510.00  
 FLOW LENGTH( FEET) = 100.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.7 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 11.79  
 ESTIMATED PIPE DIAMETER( INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW( CFS) = 36.60  
 PIPE TRAVEL TIME( MIN.) = 0.14 Tc( MIN.) = 11.93  
 LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2010.00 = 1785.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2010.00 TO NODE 2010.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.93  
 RAINFALL INTENSITY(INCH/HR) = 5.41  
 TOTAL STREAM AREA(ACRES) = 22.50  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.60

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2005.00 TO NODE 2006.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION( FEET) = 791.00  
 DOWNSTREAM ELEVATION( FEET) = 750.00  
 ELEVATION DIFFERENCE( FEET) = 41.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.71  
 TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2006.00 TO NODE 2007.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 750.00 DOWNSTREAM( FEET) = 650.00  
 CHANNEL LENGTH THRU SUBAREA( FEET) = 210.00 CHANNEL SLOPE = 0.4762  
 CHANNEL BASE( FEET) = 30.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH( FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.124  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.17  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 3.16  
 AVERAGE FLOW DEPTH( FEET) = 0.03 TRAVEL TIME(MIN.) = 1.11  
 Tc(MIN.) = 7.79  
 SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 4.92  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 2.60 PEAK FLOW RATE(CFS) = 5.56

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH( FEET) = 0.05 FLOW VELOCITY( FEET/SEC.) = 3.80  
 LONGEST FLOWPATH FROM NODE 2005.00 TO NODE 2007.00 = 310.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2007.00 TO NODE 2008.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 650.00 DOWNSTREAM(FEET) = 578.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 470.00 CHANNEL SLOPE = 0.1532  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.338  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 18.35  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.05  
 AVERAGE FLOW DEPTH(FEET) = 0.18 TRAVEL TIME(MIN.) = 1.55  
 Tc(MIN.) = 9.34  
 SUBAREA AREA(ACRES) = 13.40 SUBAREA RUNOFF(CFS) = 25.48  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 16.00 PEAK FLOW RATE(CFS) = 30.42  
  
 END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.24 FLOW VELOCITY(FEET/SEC.) = 6.21  
 LONGEST FLOWPATH FROM NODE 2005.00 TO NODE 2008.00 = 780.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2008.00 TO NODE 2011.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 578.00 DOWNSTREAM(FEET) = 512.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 680.00 CHANNEL SLOPE = 0.0971  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 3.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.600  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 35.28  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.73  
 AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 1.98  
 Tc(MIN.) = 11.32  
 SUBAREA AREA(ACRES) = 6.20 SUBAREA RUNOFF(CFS) = 9.72  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.294  
 TOTAL AREA(ACRES) = 22.20 PEAK FLOW RATE(CFS) = 36.60

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.30 FLOW VELOCITY(FEET/SEC.) = 5.79  
 LONGEST FLOWPATH FROM NODE 2005.00 TO NODE 2011.00 = 1460.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2011.00 TO NODE 2010.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 512.00 DOWNSTREAM(FEET) = 510.00  
 FLOW LENGTH(FEET) = 85.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.63  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1



PIPE-FLOW(CFS) = 36.60  
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 11.43  
 LONGEST FLOWPATH FROM NODE 2005.00 TO NODE 2010.00 = 1545.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2010.00 TO NODE 2010.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	11.43
RAINFALL INTENSITY(INCH/HR) =	5.56
TOTAL STREAM AREA(ACRES) =	22.20
PEAK FLOW RATE(CFS) AT CONFLUENCE =	36.60

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	36.60	11.93	5.414	22.50
2	36.60	11.43	5.564	22.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	72.21	11.43	5.564
2	72.21	11.93	5.414

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 72.21 Tc(MIN.) = 11.43  
 TOTAL AREA(ACRES) = 44.70  
 LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2010.00 = 1785.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2010.00 TO NODE 2012.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	510.00	DOWNSTREAM(FEET) =	474.00
FLOW LENGTH(FEET) =	420.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS	18.9 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	24.24		
ESTIMATED PIPE DIAMETER(INCH) =	27.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	72.21		
PIPE TRAVEL TIME(MIN.) =	0.29	Tc(MIN.) =	11.72
LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2012.00 =	2205.00 FEET.		

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2012.00 TO NODE 2012.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.72  
 RAINFALL INTENSITY(INCH/HR) = 5.48  
 TOTAL STREAM AREA(ACRES) = 44.70  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 72.21

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2013.00 TO NODE 2014.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 529.50  
 DOWNSTREAM ELEVATION(FEET) = 519.00  
 ELEVATION DIFFERENCE(FEET) = 10.50  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.671  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.71  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2014.00 TO NODE 2012.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 519.00 DOWNSTREAM ELEVATION(FEET) = 474.00  
 STREET LENGTH(FEET) = 430.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.52  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.30  
 HALFSTREET FLOOD WIDTH(FEET) = 7.28  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.61  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.01  
 STREET FLOW TRAVEL TIME(MIN.) = 1.08 Tc(MIN.) = 2.75  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
 S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
 SUBAREA AREA(ACRES) = 2.70 SUBAREA RUNOFF(CFS) = 15.62  
 TOTAL AREA(ACRES) = 2.90 PEAK FLOW RATE(CFS) = 17.33

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 9.84  
 FLOW VELOCITY(FEET/SEC.) = 7.48 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.66  
 LONGEST FLOWPATH FROM NODE 2013.00 TO NODE 2012.00 = 530.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2012.00 TO NODE 2012.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	2.75
RAINFALL INTENSITY(INCH/HR) =	9.49
TOTAL STREAM AREA(ACRES) =	2.90
PEAK FLOW RATE(CFS) AT CONFLUENCE =	17.33

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	72.21	11.72	5.475	44.70
2	17.33	2.75	9.485	2.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	59.01	2.75	9.485
2	82.21	11.72	5.475

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 82.21 Tc(MIN.) = 11.72  
 TOTAL AREA(ACRES) = 47.60  
 LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2012.00 = 2205.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2012.00 TO NODE 2015.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	474.00	DOWNSTREAM(FEET) =	471.50
FLOW LENGTH(FEET) =	40.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS	21.2 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	22.23		
ESTIMATED PIPE DIAMETER(INCH) =	30.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	82.21		
PIPE TRAVEL TIME(MIN.) =	0.03	Tc(MIN.) =	11.75
LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2015.00 =	2245.00 FEET.		

```

*****
FLOW PROCESS FROM NODE    2015.00 TO NODE    2015.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.75
RAINFALL INTENSITY(INCH/HR) =  5.47
TOTAL STREAM AREA(ACRES) =  47.60
PEAK FLOW RATE(CFS) AT CONFLUENCE =      82.21

*****
FLOW PROCESS FROM NODE    2016.00 TO NODE    2017.00 IS CODE =   21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =    85.00
UPSTREAM ELEVATION(FEET) =    485.90
DOWNSTREAM ELEVATION(FEET) =    482.50
ELEVATION DIFFERENCE(FEET) =    3.40
SUBAREA OVERLAND TIME OF FLOW(MIN.) =  5.123
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  9.338
SUBAREA RUNOFF(CFS) =    1.14
TOTAL AREA(ACRES) =    0.20  TOTAL RUNOFF(CFS) =    1.14

*****
FLOW PROCESS FROM NODE    2017.00 TO NODE    2018.00 IS CODE =   62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #  1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 482.50  DOWNSTREAM ELEVATION(FEET) = 473.00
STREET LENGTH(FEET) = 100.00  CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =      2.80
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.20
HALFSTREET FLOOD WIDTH(FEET) = 2.00
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.69
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.33
STREET FLOW TRAVEL TIME(MIN.) = 0.25  Tc(MIN.) = 5.37
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.056
*USER SPECIFIED(SUBAREA):

```

USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.610  
 SUBAREA AREA (ACRES) = 0.60 SUBAREA RUNOFF (CFS) = 3.31  
 TOTAL AREA (ACRES) = 0.80 PEAK FLOW RATE (CFS) = 4.42

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.25 HALFSTREET FLOOD WIDTH (FEET) = 4.41  
 FLOW VELOCITY (FEET/SEC.) = 5.76 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.42  
 LONGEST FLOWPATH FROM NODE 2016.00 TO NODE 2018.00 = 185.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2018.00 TO NODE 2015.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 473.00 DOWNSTREAM (FEET) = 471.50  
 FLOW LENGTH (FEET) = 55.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER (INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.4 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 7.90  
 ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 4.42  
 PIPE TRAVEL TIME (MIN.) = 0.12 Tc (MIN.) = 5.49  
 LONGEST FLOWPATH FROM NODE 2016.00 TO NODE 2015.00 = 240.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2015.00 TO NODE 2015.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 5.49  
 RAINFALL INTENSITY (INCH/HR) = 8.93  
 TOTAL STREAM AREA (ACRES) = 0.80  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 4.42

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	82.21	11.75	5.466	47.60
2	4.42	5.49	8.932	0.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	54.73	5.49	8.932
2	84.92	11.75	5.466

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 84.92 Tc (MIN.) = 11.75

```

TOTAL AREA(ACRES) =      48.40
LONGEST FLOWPATH FROM NODE    2000.00 TO NODE    2015.00 =  2245.00 FEET.

*****
FLOW PROCESS FROM NODE    2015.00 TO NODE    2019.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   471.50  DOWNSTREAM(FEET) =   457.00
FLOW LENGTH(FEET) =   235.00  MANNING'S N =   0.013
DEPTH OF FLOW IN  30.0 INCH PIPE IS  21.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   22.21
ESTIMATED PIPE DIAMETER(INCH) =   30.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =      84.92
PIPE TRAVEL TIME(MIN.) =    0.18  Tc(MIN.) =   11.93
LONGEST FLOWPATH FROM NODE    2000.00 TO NODE    2019.00 =  2480.00 FEET.

*****
FLOW PROCESS FROM NODE    2019.00 TO NODE    2019.00 IS CODE =   1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE: ...
TIME OF CONCENTRATION(MIN.) =   11.93
RAINFALL INTENSITY(INCH/HR) =    5.41
TOTAL STREAM AREA(ACRES) =    48.40
PEAK FLOW RATE(CFS) AT CONFLUENCE =      84.92

*****
FLOW PROCESS FROM NODE    2020.00 TO NODE    2021.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =   100.00
UPSTREAM ELEVATION(FEET) =   485.00
DOWNSTREAM ELEVATION(FEET) =   475.00
ELEVATION DIFFERENCE(FEET) =    10.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    1.671
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) =      2.56
TOTAL AREA(ACRES) =      0.30  TOTAL RUNOFF(CFS) =      2.56

*****
FLOW PROCESS FROM NODE    2021.00 TO NODE    2019.00 IS CODE =  62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #  1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =   475.00  DOWNSTREAM ELEVATION(FEET) =   457.00
STREET LENGTH(FEET) =   150.00  CURB HEIGHT(INCHES) =    6.0

```

STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.41

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.20

HALFSTREET FLOOD WIDTH(FEET) = 2.00

AVERAGE FLOW VELOCITY(FEET/SEC.) = 7.52

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.49

STREET FLOW TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 2.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900

SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 1.71

TOTAL AREA(ACRES) = 0.50 PEAK FLOW RATE(CFS) = 4.27

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 3.72

FLOW VELOCITY(FEET/SEC.) = 6.51 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.51

LONGEST FLOWPATH FROM NODE 2020.00 TO NODE 2019.00 = 250.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2019.00 TO NODE 2019.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 2.00

RAINFALL INTENSITY(INCH/HR) = 9.49

TOTAL STREAM AREA(ACRES) = 0.50

PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.27

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	84.92	11.93	5.414	48.40
2	4.27	2.00	9.485	0.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
------------------	-----------------	--------------	--------------------------

1	52.74	2.00	9.485
2	87.35	11.93	5.414

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 87.35 Tc(MIN.) = 11.93

TOTAL AREA(ACRES) = 48.90

LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2019.00 = 2480.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2019.00 TO NODE 2022.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 457.00 DOWNSTREAM(FEET) = 445.00

FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 33.0 INCH PIPE IS 22.2 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 20.54

ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 87.35

PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 12.13

LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2022.50 = 2730.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 2022.00 TO NODE 2022.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.13

RAINFALL INTENSITY(INCH/HR) = 5.36

TOTAL STREAM AREA(ACRES) = 48.90

PEAK FLOW RATE(CFS) AT CONFLUENCE = 87.35

\*\*\*\*\*

FLOW PROCESS FROM NODE 2023.00 TO NODE 2024.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 484.90

DOWNSTREAM ELEVATION(FEET) = 465.30

ELEVATION DIFFERENCE(FEET) = 19.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.094

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.74

TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.74

\*\*\*\*\*

FLOW PROCESS FROM NODE 2024.00 TO NODE 2022.50 IS CODE = 62

-----



```

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 465.30 DOWNSTREAM ELEVATION(FEET) = 445.00
STREET LENGTH(FEET) = 390.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.81
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.31
HALFSTREET FLOOD WIDTH(FEET) = 7.34
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.67
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.42
STREET FLOW TRAVEL TIME(MIN.) = 1.39 Tc(MIN.) = 5.49
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.934
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.627
SUBAREA AREA(ACRES) = 1.80 SUBAREA RUNOFF(CFS) = 10.13
TOTAL AREA(ACRES) = 2.10 PEAK FLOW RATE(CFS) = 11.77

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.35 HALFSTREET FLOOD WIDTH(FEET) = 9.66
FLOW VELOCITY(FEET/SEC.) = 5.24 DEPTH*VELOCITY(FT*FT/SEC.) = 1.84
LONGEST FLOWPATH FROM NODE 2023.00 TO NODE 2022.50 = 490.00 FEET.

*****
FLOW PROCESS FROM NODE 2022.50 TO NODE 2022.50 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.49
RAINFALL INTENSITY(INCH/HR) = 8.93
TOTAL STREAM AREA(ACRES) = 2.10
PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.77

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	87.35	12.13	5.355	48.90
2	11.77	5.49	8.934	2.10

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

```

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	64.13	5.49	8.934
2	94.41	12.13	5.355

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 94.41 Tc(MIN.) = 12.13

TOTAL AREA(ACRES) = 51.00

LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2022.50 = 2730.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2022.50 TO NODE 2029.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 445.00 DOWNSTREAM(FEET) = 433.00

FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 25.20

ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 94.41

PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 12.23

LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2029.00 = 2880.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2029.00 TO NODE 2029.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 12.23

RAINFALL INTENSITY(INCH/HR) = 5.33

TOTAL STREAM AREA(ACRES) = 51.00

PEAK FLOW RATE(CFS) AT CONFLUENCE = 94.41

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2030.00 TO NODE 2031.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00

UPSTREAM ELEVATION(FEET) = 720.00

DOWNSTREAM ELEVATION(FEET) = 670.00

ELEVATION DIFFERENCE(FEET) = 50.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.727

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 0.57

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.57

```

*****
FLOW PROCESS FROM NODE    2031.00 TO NODE    2032.00 IS CODE =  51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) =    670.00  DOWNSTREAM( FEET) =    490.00
CHANNEL LENGTH THRU SUBAREA( FEET) =    630.00  CHANNEL SLOPE =    0.2857
CHANNEL BASE( FEET) =    15.00  "Z" FACTOR =    2.000
MANNING'S FACTOR = 0.035  MAXIMUM DEPTH( FEET) =    10.00
100 YEAR RAINFALL INTENSITY( INCH/HOUR) =    7.195
*USER SPECIFIED( SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) =    0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS) =      3.44
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) =    3.56
AVERAGE FLOW DEPTH( FEET) =    0.06  TRAVEL TIME( MIN.) =    2.95
Tc( MIN.) =    7.67
SUBAREA AREA( ACRES) =    2.60  SUBAREA RUNOFF( CFS) =    5.61
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
TOTAL AREA( ACRES) =    2.80  PEAK FLOW RATE( CFS) =    6.04

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH( FEET) = 0.09  FLOW VELOCITY( FEET/SEC.) =    4.49
LONGEST FLOWPATH FROM NODE    2030.00 TO NODE    2032.00 =    680.00 FEET.

*****
FLOW PROCESS FROM NODE    2032.00 TO NODE    2033.00 IS CODE =  51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) =    490.00  DOWNSTREAM( FEET) =    440.00
CHANNEL LENGTH THRU SUBAREA( FEET) =    680.00  CHANNEL SLOPE =    0.0735
CHANNEL BASE( FEET) =    15.00  "Z" FACTOR =    2.000
MANNING'S FACTOR = 0.035  MAXIMUM DEPTH( FEET) =    10.00
100 YEAR RAINFALL INTENSITY( INCH/HOUR) =    5.796
*USER SPECIFIED( SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) =    0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS) =    11.04
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) =    3.71
AVERAGE FLOW DEPTH( FEET) =    0.19  TRAVEL TIME( MIN.) =    3.06
Tc( MIN.) =    10.73
SUBAREA AREA( ACRES) =    5.70  SUBAREA RUNOFF( CFS) =    9.91
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
TOTAL AREA( ACRES) =    8.50  PEAK FLOW RATE( CFS) =    14.78

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH( FEET) = 0.23  FLOW VELOCITY( FEET/SEC.) =    4.23
LONGEST FLOWPATH FROM NODE    2030.00 TO NODE    2033.00 =   1360.00 FEET.

*****
FLOW PROCESS FROM NODE    2033.00 TO NODE    2029.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

```

```

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 440.00 DOWNSTREAM(FEET) = 433.00
FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.88
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 14.78
PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 10.89
LONGEST FLOWPATH FROM NODE 2030.00 TO NODE 2029.00 = 1490.00 FEET.

*****
FLOW PROCESS FROM NODE 2029.00 TO NODE 2029.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.89
RAINFALL INTENSITY(INCH/HR) = 5.74
TOTAL STREAM AREA(ACRES) = 8.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.78

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	94.41	12.23	5.327	51.00
2	14.78	10.89	5.742	8.50

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	102.37	10.89	5.742
2	108.12	12.23	5.327

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 108.12 Tc(MIN.) = 12.23
TOTAL AREA(ACRES) = 59.50
LONGEST FLOWPATH FROM NODE 2000.00 TO NODE 2029.00 = 2880.00 FEET.
=====
END OF STUDY SUMMARY:
TOTAL AREA(ACRES) = 59.50 TC(MIN.) = 12.23
PEAK FLOW RATE(CFS) = 108.12
=====
END OF RATIONAL METHOD ANALYSIS

```

## **Drainage Basin 3000**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
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San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Post-project (on-site) \*  
\* Drainage Basin 3000 \*  
\*\*\*\*\*

FILE NAME: MW\_3K100.DAT  
TIME/DATE OF STUDY: 10:43 07/13/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)						
===	=====	=====	=====	=====	=====	=====	=====	=====
1	30.0	20.0	0.020/0.020/0.020	0.50	1.50	0.0100	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = -0.10 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3000.00 TO NODE 3001.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA) :  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 822.50  
 DOWNSTREAM ELEVATION(FEET) = 780.00  
 ELEVATION DIFFERENCE(FEET) = 42.50  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3001.00 TO NODE 3002.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 780.00 DOWNSTREAM(FEET) = 545.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1005.00 CHANNEL SLOPE = 0.2338  
 CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.934

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.15

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.58

AVERAGE FLOW DEPTH(FEET) = 0.11 TRAVEL TIME(MIN.) = 3.66

Tc(MIN.) = 10.34

SUBAREA AREA(ACRES) = 10.60 SUBAREA RUNOFF(CFS) = 18.87

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 10.80 PEAK FLOW RATE(CFS) = 19.23

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 6.01

LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3002.00 = 1105.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3002.00 TO NODE 3006.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 545.00 DOWNSTREAM(FEET) = 507.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 160.00 CHANNEL SLOPE = 0.2375  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.814

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2800

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 21.34

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.98

AVERAGE FLOW DEPTH(FEET) = 0.25 TRAVEL TIME(MIN.) = 0.33

Tc(MIN.) = 10.68

SUBAREA AREA(ACRES) = 2.60 SUBAREA RUNOFF(CFS) = 4.23

AREA-AVERAGE RUNOFF COEFFICIENT = 0.296

TOTAL AREA(ACRES) = 13.40 PEAK FLOW RATE(CFS) = 23.07

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.26 FLOW VELOCITY (FEET/SEC.) = 8.29

LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3006.00 = 1265.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3006.00 TO NODE 3007.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 507.00 DOWNSTREAM (FEET) = 484.00

FLOW LENGTH (FEET) = 300.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.6 INCHES

PIPE-FLOW VELOCITY (FEET/SEC.) = 17.48

ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW (CFS) = 23.07

PIPE TRAVEL TIME (MIN.) = 0.29 Tc (MIN.) = 10.97

LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3007.00 = 1565.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3007.00 TO NODE 3007.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION (MIN.) = 10.97

RAINFALL INTENSITY (INCH/HR) = 5.72

TOTAL STREAM AREA (ACRES) = 13.40

PEAK FLOW RATE (CFS) AT CONFLUENCE = 23.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 3008.00 TO NODE 3009.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00

UPSTREAM ELEVATION (FEET) = 898.70

DOWNSTREAM ELEVATION (FEET) = 830.00

ELEVATION DIFFERENCE (FEET) = 68.70

SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.684

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.865

SUBAREA RUNOFF (CFS) = 0.47

TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 0.47

\*\*\*\*\*

FLOW PROCESS FROM NODE 3009.00 TO NODE 3010.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 830.00 DOWNSTREAM (FEET) = 575.00



CHANNEL LENGTH THRU SUBAREA (FEET) = 670.00    CHANNEL SLOPE = 0.3806  
 CHANNEL BASE (FEET) = 10.00    "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035    MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.723  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 7.28  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 6.07  
 AVERAGE FLOW DEPTH (FEET) = 0.12    TRAVEL TIME (MIN.) = 1.84  
 Tc (MIN.) = 8.52  
 SUBAREA AREA (ACRES) = 6.70    SUBAREA RUNOFF (CFS) = 13.51  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA (ACRES) = 6.90    PEAK FLOW RATE (CFS) = 13.92

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.17    FLOW VELOCITY (FEET/SEC.) = 7.88  
 LONGEST FLOWPATH FROM NODE 3008.00 TO NODE 3010.00 = 770.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3010.00 TO NODE 3011.00 IS CODE = 51

>>>> COMPUTE TRAPEZOIDAL CHANNEL FLOW <<<<<  
 >>>> TRAVELTIME THRU SUBAREA (EXISTING ELEMENT) <<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 575.00    DOWNSTREAM (FEET) = 487.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 350.00    CHANNEL SLOPE = 0.2514  
 CHANNEL BASE (FEET) = 20.00    "Z" FACTOR = 3.000  
 MANNING'S FACTOR = 0.035    MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.268  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 18.25  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 5.96  
 AVERAGE FLOW DEPTH (FEET) = 0.15    TRAVEL TIME (MIN.) = 0.98  
 Tc (MIN.) = 9.50  
 SUBAREA AREA (ACRES) = 4.60    SUBAREA RUNOFF (CFS) = 8.65  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA (ACRES) = 11.50    PEAK FLOW RATE (CFS) = 21.62

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.16    FLOW VELOCITY (FEET/SEC.) = 6.40  
 LONGEST FLOWPATH FROM NODE 3008.00 TO NODE 3011.00 = 1120.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3011.00 TO NODE 3007.00 IS CODE = 31

>>>> COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA <<<<<  
 >>>> USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 487.00    DOWNSTREAM (FEET) = 484.00  
 FLOW LENGTH (FEET) = 190.00    MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.3 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 9.54  
 ESTIMATED PIPE DIAMETER (INCH) = 24.00    NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 21.62

PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 9.84  
 LONGEST FLOWPATH FROM NODE 3008.00 TO NODE 3007.00 = 1310.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3007.00 TO NODE 3007.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	9.84
RAINFALL INTENSITY(INCH/HR) =	6.13
TOTAL STREAM AREA(ACRES) =	11.50
PEAK FLOW RATE(CFS) AT CONFLUENCE =	21.62

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	23.07	10.97	5.716	13.40
2	21.62	9.84	6.131	11.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	42.32	9.84	6.131
2	43.23	10.97	5.716

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 43.23 Tc(MIN.) = 10.97  
 TOTAL AREA(ACRES) = 24.90  
 LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3007.00 = 1565.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3007.00 TO NODE 3012.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	484.00	DOWNSTREAM(FEET) =	477.00
FLOW LENGTH(FEET) =	120.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS	16.7 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	18.47		
ESTIMATED PIPE DIAMETER(INCH) =	24.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	43.23		
PIPE TRAVEL TIME(MIN.) =	0.11	Tc(MIN.) =	11.07
LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3012.00 =	1685.00 FEET.		

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3012.00 TO NODE 3012.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.07  
 RAINFALL INTENSITY(INCH/HR) = 5.68  
 TOTAL STREAM AREA(ACRES) = 24.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.23

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3013.00 TO NODE 3014.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(Feet) = 100.00  
 UPSTREAM ELEVATION(Feet) = 520.00  
 DOWNSTREAM ELEVATION(Feet) = 513.00  
 ELEVATION DIFFERENCE(Feet) = 7.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.611  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.16  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.16

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3014.00 TO NODE 3012.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(Feet) = 513.00 DOWNSTREAM ELEVATION(Feet) = 477.00  
 STREET LENGTH(Feet) = 320.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(Feet) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(Feet) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.98  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(Feet) = 0.24  
 HALFSTREET FLOOD WIDTH(Feet) = 6.98  
 AVERAGE FLOW VELOCITY(Feet/Sec.) = 6.09  
 PRODUCT OF DEPTH&VELOCITY(Ft\*Ft/Sec.) = 1.49  
 STREET FLOW TRAVEL TIME(MIN.) = 0.88 Tc(MIN.) = 5.49  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.934  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.619  
 SUBAREA AREA(ACRES) = 2.10 SUBAREA RUNOFF(CFS) = 11.63  
 TOTAL AREA(ACRES) = 2.30 PEAK FLOW RATE(CFS) = 12.72

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.29    HALFSTREET FLOOD WIDTH(FEET) = 9.04  
FLOW VELOCITY(FEET/SEC.) = 7.04    DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.01  
LONGEST FLOWPATH FROM NODE 3013.00 TO NODE 3012.00 = 420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3012.00 TO NODE 3012.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.49  
RAINFALL INTENSITY(INCH/HR) = 8.93  
TOTAL STREAM AREA(ACRES) = 2.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.72

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	43.23	11.07	5.680	24.90
2	12.72	5.49	8.934	2.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	40.21	5.49	8.934
2	51.32	11.07	5.680

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 51.32    Tc(MIN.) = 11.07  
TOTAL AREA(ACRES) = 27.20  
LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3012.00 = 1685.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3012.00 TO NODE 3015.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 477.00    DOWNSTREAM(FEET) = 474.00  
FLOW LENGTH(FEET) = 50.00    MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 19.2 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.07  
ESTIMATED PIPE DIAMETER(INCH) = 24.00    NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 51.32  
PIPE TRAVEL TIME(MIN.) = 0.04    Tc(MIN.) = 11.12  
LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3015.00 = 1735.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3015.00 TO NODE 3015.00 IS CODE = 1

-----

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.12
RAINFALL INTENSITY(INCH/HR) = 5.67
TOTAL STREAM AREA(ACRES) = 27.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 51.32

*****
FLOW PROCESS FROM NODE 3016.00 TO NODE 3017.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00
UPSTREAM ELEVATION(FEET) = 495.00
DOWNSTREAM ELEVATION(FEET) = 490.00
ELEVATION DIFFERENCE(FEET) = 5.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.505
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.74
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.74

*****
FLOW PROCESS FROM NODE 3017.00 TO NODE 3018.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 490.00 DOWNSTREAM ELEVATION(FEET) = 475.00
STREET LENGTH(FEET) = 380.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.39
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.28
HALFSTREET FLOOD WIDTH(FEET) = 8.97
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.15
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.18
STREET FLOW TRAVEL TIME(MIN.) = 1.53 Tc(MIN.) = 6.03
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.403
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) = 0

```

AREA-AVERAGE RUNOFF COEFFICIENT = 0.610  
 SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 11.28  
 TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 12.81

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 11.29  
 FLOW VELOCITY(FEET/SEC.) = 4.71 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.56  
 LONGEST FLOWPATH FROM NODE 3016.00 TO NODE 3018.00 = 465.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3018.00 TO NODE 3015.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 475.00 DOWNSTREAM(FEET) = 474.00  
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.04  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 12.81  
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 6.13  
 LONGEST FLOWPATH FROM NODE 3016.00 TO NODE 3015.00 = 515.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3015.00 TO NODE 3015.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.13  
 RAINFALL INTENSITY(INCH/HR) = 8.32  
 TOTAL STREAM AREA(ACRES) = 2.50  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.81

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	51.32	11.12	5.665	27.20
2	12.81	6.13	8.321	2.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	47.75	6.13	8.321
2	60.04	11.12	5.665

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 60.04 Tc(MIN.) = 11.12  
 TOTAL AREA(ACRES) = 29.70  
 LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3015.00 = 1735.00 FEET.

```

*****
FLOW PROCESS FROM NODE    3015.00 TO NODE    3019.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   474.00  DOWNSTREAM(FEET) =   473.00
FLOW LENGTH(FEET) =   40.00  MANNING'S N =  0.013
DEPTH OF FLOW IN  30.0 INCH PIPE IS  24.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =  14.28
ESTIMATED PIPE DIAMETER(INCH) =  30.00  NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =   60.04
PIPE TRAVEL TIME(MIN.) =   0.05  Tc(MIN.) =  11.16
LONGEST FLOWPATH FROM NODE    3000.00 TO NODE    3019.00 =  1775.00 FEET.

*****
FLOW PROCESS FROM NODE    3019.00 TO NODE    3019.00 IS CODE =   1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =  11.16
RAINFALL INTENSITY(INCH/HR) =   5.65
TOTAL STREAM AREA(ACRES) =   29.70
PEAK FLOW RATE(CFS) AT CONFLUENCE =   60.04

*****
FLOW PROCESS FROM NODE    3020.00 TO NODE    3021.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) =   0
INITIAL SUBAREA FLOW-LENGTH(FEET) =  100.00
UPSTREAM ELEVATION(FEET) =   645.00
DOWNSTREAM ELEVATION(FEET) =   590.00
ELEVATION DIFFERENCE(FEET) =   55.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =   6.684
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  7.865
SUBAREA RUNOFF(CFS) =   0.47
TOTAL AREA(ACRES) =   0.20  TOTAL RUNOFF(CFS) =   0.47

*****
FLOW PROCESS FROM NODE    3021.00 TO NODE    3022.00 IS CODE =  51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   590.00  DOWNSTREAM(FEET) =   482.00
CHANNEL LENGTH THRU SUBAREA(FEET) =  580.00  CHANNEL SLOPE =  0.1862
CHANNEL BASE(FEET) =  10.00  "Z" FACTOR =  2.000
MANNING'S FACTOR = 0.035  MAXIMUM DEPTH(FEET) =  10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  6.024
*USER SPECIFIED(SUBAREA):

```

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.66  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.83  
 AVERAGE FLOW DEPTH(FEET) = 0.06 TRAVEL TIME(MIN.) = 3.42  
 Tc(MIN.) = 10.11  
 SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 2.35  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 1.50 PEAK FLOW RATE(CFS) = 2.71

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.08 FLOW VELOCITY(FEET/SEC.) = 3.37  
 LONGEST FLOWPATH FROM NODE 3020.00 TO NODE 3022.00 = 680.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3022.00 TO NODE 3019.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 482.00 DOWNSTREAM(FEET) = 473.00  
 FLOW LENGTH(FEET) = 240.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.70  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.71  
 PIPE TRAVEL TIME(MIN.) = 0.52 Tc(MIN.) = 10.63  
 LONGEST FLOWPATH FROM NODE 3020.00 TO NODE 3019.00 = 920.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3019.00 TO NODE 3019.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.63  
 RAINFALL INTENSITY(INCH/HR) = 5.83  
 TOTAL STREAM AREA(ACRES) = 1.50  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.71

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	60.04	11.16	5.650	29.70
2	2.71	10.63	5.833	1.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	60.87	10.63	5.833
2	62.67	11.16	5.650



COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 62.67 Tc(MIN.) = 11.16

TOTAL AREA(ACRES) = 31.20

LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3019.00 = 1775.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3019.00 TO NODE 3023.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 473.00 DOWNSTREAM(FEET) = 457.00

FLOW LENGTH(FEET) = 300.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.5 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 19.37

ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 62.67

PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 11.42

LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3023.00 = 2075.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3023.00 TO NODE 3023.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 11.42

RAINFALL INTENSITY(INCH/HR) = 5.57

TOTAL STREAM AREA(ACRES) = 31.20

PEAK FLOW RATE(CFS) AT CONFLUENCE = 62.67

\*\*\*\*\*

FLOW PROCESS FROM NODE 3024.00 TO NODE 3025.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA) :

USER-SPECIFIED RUNOFF COEFFICIENT = .6100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00

UPSTREAM ELEVATION(FEET) = 478.50

DOWNSTREAM ELEVATION(FEET) = 475.50

ELEVATION DIFFERENCE(FEET) = 3.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.543

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 2.31

TOTAL AREA(ACRES) = 0.40 TOTAL RUNOFF(CFS) = 2.31

\*\*\*\*\*

FLOW PROCESS FROM NODE 3025.00 TO NODE 3026.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 475.50 DOWNSTREAM ELEVATION(FEET) = 458.00  
STREET LENGTH(FEET) = 370.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.38  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.30  
HALFSTREET FLOOD WIDTH(FEET) = 9.57  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.68  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.39  
STREET FLOW TRAVEL TIME(MIN.) = 1.32 Tc(MIN.) = 5.86  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.562  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.610  
SUBAREA AREA(ACRES) = 2.70 SUBAREA RUNOFF(CFS) = 14.10  
TOTAL AREA(ACRES) = 3.10 PEAK FLOW RATE(CFS) = 16.19

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 11.99  
FLOW VELOCITY(FEET/SEC.) = 5.31 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.83  
LONGEST FLOWPATH FROM NODE 3024.00 TO NODE 3026.00 = 440.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3026.00 TO NODE 3023.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET)	=	458.00	DOWNSTREAM(FEET)	=	457.00
FLOW LENGTH(FEET)	=	75.00	MANNING'S N	=	0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.1 INCHES					
PIPE-FLOW VELOCITY(FEET/SEC.)	=	8.20			
ESTIMATED PIPE DIAMETER(INCH)	=	21.00	NUMBER OF PIPES	=	1
PIPE-FLOW(CFS)	=	16.19			
PIPE TRAVEL TIME(MIN.)	=	0.15	Tc(MIN.)	=	6.01
LONGEST FLOWPATH FROM NODE 3024.00 TO NODE 3023.00 = 515.00 FEET.					

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3023.00 TO NODE 3023.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS	=	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:		
TIME OF CONCENTRATION(MIN.)	=	6.01

RAINFALL INTENSITY (INCH/HR) = 8.42  
 TOTAL STREAM AREA (ACRES) = 3.10  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 16.19

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	62.67	11.42	5.567	31.20
2	16.19	6.01	8.421	3.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	57.62	6.01	8.421
2	73.37	11.42	5.567

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 73.37 Tc (MIN.) = 11.42  
 TOTAL AREA (ACRES) = 34.30  
 LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3023.00 = 2075.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3023.00 TO NODE 3023.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 457.00 DOWNSTREAM (FEET) = 433.00  
 FLOW LENGTH (FEET) = 270.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.9 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 24.67  
 ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 73.37  
 PIPE TRAVEL TIME (MIN.) = 0.18 Tc (MIN.) = 11.60  
 LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3023.10 = 2345.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3023.10 TO NODE 3043.70 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 433.00 DOWNSTREAM (FEET) = 431.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 170.00 CHANNEL SLOPE = 0.0118  
 CHANNEL BASE (FEET) = 50.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.045 MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.165  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 74.00  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 2.31  
 AVERAGE FLOW DEPTH (FEET) = 0.58 TRAVEL TIME (MIN.) = 1.23  
 Tc (MIN.) = 12.83

SUBAREA AREA(ACRES) = 0.70 SUBAREA RUNOFF(CFS) = 1.27  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.370  
TOTAL AREA(ACRES) = 35.00 PEAK FLOW RATE(CFS) = 73.37

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.57 FLOW VELOCITY(FEET/SEC.) = 2.31  
LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3043.70 = 2515.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3043.70 TO NODE 3043.70 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 3003.00 TO NODE 3004.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 827.00

DOWNSTREAM ELEVATION(FEET) = 810.00

ELEVATION DIFFERENCE(FEET) = 17.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION:

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865

SUBAREA RUNOFF(CFS) = 0.47

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*

FLOW PROCESS FROM NODE 3004.00 TO NODE 3005.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 810.00 DOWNSTREAM(FEET) = 540.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 928.00 CHANNEL SLOPE = 0.2909

CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 2.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.379

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.82

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.03

AVERAGE FLOW DEPTH(FEET) = 0.14 TRAVEL TIME(MIN.) = 2.56

Tc(MIN.) = 9.25

SUBAREA AREA(ACRES) = 8.60 SUBAREA RUNOFF(CFS) = 16.46

AREA-AVERAGE RUNOFF COEFFICIENT = 0.300

TOTAL AREA(ACRES) = 8.80 PEAK FLOW RATE(CFS) = 16.84

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.21 FLOW VELOCITY(FEET/SEC.) = 7.74

LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3005.00 = 1028.00 FEET.

```

*****
FLOW PROCESS FROM NODE 3005.00 TO NODE 3028.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 540.00 DOWNSTREAM(FEET) = 480.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 500.00 CHANNEL SLOPE = 0.1200
CHANNEL BASE(FEET) = 20.00 "Z" FACTOR = 2.000
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.781
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 25.25
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.46
AVERAGE FLOW DEPTH(FEET) = 0.23 TRAVEL TIME(MIN.) = 1.53
Tc(MIN.) = 10.77
SUBAREA AREA(ACRES) = 9.70 SUBAREA RUNOFF(CFS) = 16.82
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
TOTAL AREA(ACRES) = 18.50 PEAK FLOW RATE(CFS) = 32.09

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.26 FLOW VELOCITY(FEET/SEC.) = 5.92
LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3028.00 = 1528.00 FEET..

*****
FLOW PROCESS FROM NODE 3028.00 TO NODE 3033.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 480.00 DOWNSTREAM(FEET) = 474.00
FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.91
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 32.09
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 10.90
LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3033.00 = 1648.00 FEET.

*****
FLOW PROCESS FROM NODE 3033.00 TO NODE 3033.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.90
RAINFALL INTENSITY(INCH/HR) = 5.74
TOTAL STREAM AREA(ACRES) = 18.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 32.09

*****
FLOW PROCESS FROM NODE 3032.00 TO NODE 3035.00 IS CODE = 21
-----

```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 495.00  
DOWNSTREAM ELEVATION(FEET) = 491.00  
ELEVATION DIFFERENCE(FEET) = 4.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.853  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.74  
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.74

\*\*\*\*\*

FLOW PROCESS FROM NODE 3035.00 TO NODE 3033.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 491.00 DOWNSTREAM ELEVATION(FEET) = 457.00  
STREET LENGTH(FEET) = 350.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.97  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 7.18  
AVERAGE FLOW VELOCITY(FT/SEC.) = 5.79  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.44  
STREET FLOW TRAVEL TIME(MIN.) = 1.01 Tc(MIN.) = 5.86  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.562

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.610  
SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 10.45  
TOTAL AREA(ACRES) = 2.30 PEAK FLOW RATE(CFS) = 12.01

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 9.10  
FLOW VELOCITY(FT/SEC.) = 6.56 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.88  
LONGEST FLOWPATH FROM NODE 3032.00 TO NODE 3033.00 = 435.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3033.00 TO NODE 3033.00 IS CODE = 1

-----

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>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.86
RAINFALL INTENSITY(INCH/HR) = 8.56
TOTAL STREAM AREA(ACRES) = 2.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.01

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/ HOUR)  (ACRE)
    1      32.09      10.90      5.738      18.50
    2      12.01      5.86      8.562      2.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/ HOUR)
    1      29.26      5.86      8.562
    2      40.14      10.90      5.738

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 40.14 Tc(MIN.) = 10.90
TOTAL AREA(ACRES) = 20.80
LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3033.00 = 1648.00 FEET.

*****
FLOW PROCESS FROM NODE 3033.00 TO NODE 3036.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 457.00 DOWNSTREAM( FEET) = 441.00
FLOW LENGTH( FEET) = 250.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.4 INCHES
PIPE-FLOW VELOCITY( FEET/ SEC.) = 18.91
ESTIMATED PIPE DIAMETER( INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 40.14
PIPE TRAVEL TIME( MIN.) = 0.22 Tc( MIN.) = 11.12
LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3036.00 = 1898.00 FEET.

*****
FLOW PROCESS FROM NODE 3036.00 TO NODE 3036.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 11.12
RAINFALL INTENSITY(INCH/HR) = 5.66
TOTAL STREAM AREA(ACRES) = 20.80
PEAK FLOW RATE(CFS) AT CONFLUENCE = 40.14

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*****
FLOW PROCESS FROM NODE 3037.00 TO NODE 3038.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .6200
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 474.00
DOWNSTREAM ELEVATION(FEET) = 460.50
ELEVATION DIFFERENCE(FEET) = 13.50
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.011
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.18
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.18

*****
FLOW PROCESS FROM NODE 3038.00 TO NODE 3036.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 460.50 DOWNSTREAM ELEVATION(FEET) = 441.00
STREET LENGTH(FEET) = 150.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.53
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.20
HALFSTREET FLOOD WIDTH(FEET) = 4.79
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.59
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.12
STREET FLOW TRAVEL TIME(MIN.) = 0.45 Tc(MIN.) = 4.46
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .6200
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.620
SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 4.70
TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 5.88

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 6.18
FLOW VELOCITY(FEET/SEC.) = 6.28 DEPTH*VELOCITY(FT*FT/SEC.) = 1.44

```



LONGEST FLOWPATH FROM NODE 3037.00 TO NODE 3036.00 = 250.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3036.00 TO NODE 3036.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	4.46
RAINFALL INTENSITY(INCH/HR) =	9.49
TOTAL STREAM AREA(ACRES) =	1.00
PEAK FLOW RATE(CFS) AT CONFLUENCE =	5.88

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	40.14	11.12	5.664	20.80
2	5.88	4.46	9.485	1.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	29.85	4.46	9.485
2	43.65	11.12	5.664

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 43.65 Tc(MIN.) = 11.12  
TOTAL AREA(ACRES) = 21.80

LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3036.00 = 1898.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3036.00 TO NODE 3027.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	441.00	DOWNSTREAM(FEET) =	439.00
FLOW LENGTH(FEET) =	200.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 33.0 INCH PIPE IS	23.8 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	9.51		
ESTIMATED PIPE DIAMETER(INCH) =	33.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	43.65		
PIPE TRAVEL TIME(MIN.) =	0.35	Tc(MIN.) =	11.47
LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3027.00 =	2098.00 FEET.		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 3027.00 TO NODE 3042.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	439.00	DOWNSTREAM(FEET) =	438.00
----------------------------------	--------	--------------------	--------

FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 23.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.51  
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 43.65  
 PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 11.64  
 LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3042.00 = 2198.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3042.00 TO NODE 3042.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 11.64  
 RAINFALL INTENSITY(INCH/HR) = 5.50  
 TOTAL STREAM AREA(ACRES) = 21.80  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 43.65

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3040.00 TO NODE 3041.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 476.50  
 DOWNSTREAM ELEVATION(FEET) = 446.50  
 ELEVATION DIFFERENCE(FEET) = 30.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.094  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.74  
 TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.74

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3041.00 TO NODE 3042.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<

=====  
 UPSTREAM ELEVATION(FEET) = 446.50 DOWNSTREAM ELEVATION(FEET) = 433.00  
 STREET LENGTH(FEET) = 325.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

```

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =          6.13
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.27
HALFSTREET FLOOD WIDTH(FEET) = 8.17
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.06
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.09
STREET FLOW TRAVEL TIME(MIN.) = 1.33   Tc(MIN.) = 5.43
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.997
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.610
SUBAREA AREA(ACRES) = 1.60   SUBAREA RUNOFF(CFS) = 8.78
TOTAL AREA(ACRES) = 1.90   PEAK FLOW RATE(CFS) = 10.43

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.31   HALFSTREET FLOOD WIDTH(FEET) = 10.27
FLOW VELOCITY(FEET/SEC.) = 4.57   DEPTH*VELOCITY(FT*FT/SEC.) = 1.42
LONGEST FLOWPATH FROM NODE 3040.00 TO NODE 3042.00 = 425.00 FEET.

*****
FLOW PROCESS FROM NODE 3042.00 TO NODE 3042.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.43
RAINFALL INTENSITY(INCH/HR) = 9.00
TOTAL STREAM AREA(ACRES) = 1.90
PEAK FLOW RATE(CFS) AT CONFLUENCE = 10.43

** CONFLUENCE DATA **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	43.65	11.64	5.498	21.80
2	10.43	5.43	8.997	1.90

```

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

```

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	37.10	5.43	8.997
2	50.02	11.64	5.498

```

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 50.02   Tc(MIN.) = 11.64
TOTAL AREA(ACRES) = 23.70
LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3042.00 = 2198.00 FEET.

*****
FLOW PROCESS FROM NODE 3042.00 TO NODE 2025.00 IS CODE = 31
-----

```

```

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 438.00 DOWNSTREAM( FEET) = 436.00
FLOW LENGTH( FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 33.0 INCH PIPE IS 27.0 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 9.63
ESTIMATED PIPE DIAMETER( INCH) = 33.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 50.02
PIPE TRAVEL TIME( MIN.) = 0.35 Tc( MIN.) = 11.99
LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 2025.00 = 2398.00 FEET.

*****
FLOW PROCESS FROM NODE 3042.50 TO NODE 3042.50 IS CODE = 10
-----
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<
=====

*****
FLOW PROCESS FROM NODE 1008.00 TO NODE 1009.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED( SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER ( AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH( FEET) = 100.00
UPSTREAM ELEVATION( FEET) = 488.00
DOWNSTREAM ELEVATION( FEET) = 483.50
ELEVATION DIFFERENCE( FEET) = 4.50
SUBAREA OVERLAND TIME OF FLOW( MIN.) = 2.167
WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN
THE MAXIMUM OVERLAND FLOW LENGTH = 98.75
(Reference: Table 3-1B of Hydrology Manual)
THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY( INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF( CFS) = 1.71
TOTAL AREA( ACRES) = 0.20 TOTAL RUNOFF( CFS) = 1.71

*****
FLOW PROCESS FROM NODE 1009.00 TO NODE 1010.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>( STREET TABLE SECTION # 1 USED) <<<<<
=====
UPSTREAM ELEVATION( FEET) = 483.50 DOWNSTREAM ELEVATION( FEET) = 465.00
STREET LENGTH( FEET) = 500.00 CURB HEIGHT( INCHES) = 6.0
STREET HALFWIDTH( FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK( FEET) = 20.00
INSIDE STREET CROSSFALL( DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL( DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL( DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section( curb-to-curb) = 0.0150

```

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.83  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 8.84  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.94  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.11  
STREET FLOW TRAVEL TIME(MIN.) = 2.12 Tc(MIN.) = 4.28  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 10.24  
TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 11.95

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.33 HALFSTREET FLOOD WIDTH(FEET) = 11.13  
FLOW VELOCITY(FEET/SEC.) = 4.51 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.48  
LONGEST FLOWPATH FROM NODE 1008.00 TO NODE 1010.00 = 600.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 1010.00 TO NODE 2028.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	465.00	DOWNSTREAM(FEET) =	442.00
FLOW LENGTH(FEET) =	360.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000			
DEPTH OF FLOW IN 18.0 INCH PIPE IS 8.7 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) =	14.07		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	11.95		
PIPE TRAVEL TIME(MIN.) =	0.43	Tc(MIN.) =	4.71
LONGEST FLOWPATH FROM NODE	1008.00	TO NODE	2028.00 = 960.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2028.00 TO NODE 2028.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS =		2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM. 1 ARE:		
TIME OF CONCENTRATION(MIN.) =	4.71	
RAINFALL INTENSITY(INCH/HR) =	9.49	
TOTAL STREAM AREA(ACRES) =	1.40	
PEAK FLOW RATE(CFS) AT CONFLUENCE =	11.95	

\*\*\*\*\*  
FLOW PROCESS FROM NODE 2026.00 TO NODE 2027.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00  
 UPSTREAM ELEVATION (FEET) = 471.00  
 DOWNSTREAM ELEVATION (FEET) = 464.00  
 ELEVATION DIFFERENCE (FEET) = 7.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 1.882  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF (CFS) = 1.71  
 TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 1.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2027.00 TO NODE 2028.00 IS CODE = 62

>>>> COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>> (STREET TABLE SECTION # 1 USED)<<<<<

=====  
 UPSTREAM ELEVATION (FEET) = 464.00 DOWNSTREAM ELEVATION (FEET) = 442.00  
 STREET LENGTH (FEET) = 260.00 CURB HEIGHT (INCHES) = 6.0  
 STREET HALFWIDTH (FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 20.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0150  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 4.27  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.22  
 HALFSTREET FLOOD WIDTH (FEET) = 5.92  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 4.89  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 1.09  
 STREET FLOW TRAVEL TIME (MIN.) = 0.89 Tc (MIN.) = 2.77  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA (ACRES) = 0.60 SUBAREA RUNOFF (CFS) = 5.12  
 TOTAL AREA (ACRES) = 0.80 PEAK FLOW RATE (CFS) = 6.83

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.25 HALFSTREET FLOOD WIDTH (FEET) = 7.38  
 FLOW VELOCITY (FEET/SEC.) = 5.42 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.37  
 LONGEST FLOWPATH FROM NODE 2026.00 TO NODE 2028.00 = 360.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2028.00 TO NODE 2028.00 IS CODE = 1

>>>> DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>> AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```

=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 2.77
RAINFALL INTENSITY(INCH/HR) = 9.49
TOTAL STREAM AREA(ACRES) = 0.80
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.83

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
    1         11.95      4.71      9.485         1.40
    2          6.83      2.77      9.485         0.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)
    1         13.85      2.77      9.485
    2         18.78      4.71      9.485

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 18.78   Tc(MIN.) = 4.71
TOTAL AREA(ACRES) = 2.20
LONGEST FLOWPATH FROM NODE 1008.00 TO NODE 2028.00 = 960.00 FEET.

*****
FLOW PROCESS FROM NODE 2028.00 TO NODE 2025.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 442.00 DOWNSTREAM(FEET) = 436.00
FLOW LENGTH(FEET) = 125.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 13.91
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 18.78
PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 4.86
LONGEST FLOWPATH FROM NODE 1008.00 TO NODE 2025.00 = 1085.00 FEET.

*****
FLOW PROCESS FROM NODE 3042.50 TO NODE 3042.50 IS CODE = 11
-----
>>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<
=====

** MAIN STREAM CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
    1         18.78      4.86      9.485         2.20
LONGEST FLOWPATH FROM NODE 1008.00 TO NODE 3042.50 = 1085.00 FEET.

** MEMORY BANK # 2 CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA

```

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	50.02	11.99	5.395	23.70

LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3042.50 = 2398.00 FEET.

**\*\* PEAK FLOW RATE TABLE \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	39.05	4.86	9.485
2	60.70	11.99	5.395

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 60.70 Tc (MIN.) = 11.99  
 TOTAL AREA (ACRES) = 25.90

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3042.50 TO NODE 3042.50 IS CODE = 12  
 -----

>>>>CLEAR MEMORY BANK # 2 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 2025.00 TO NODE 3042.50 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 436.00 DOWNSTREAM (FEET) = 433.00  
 FLOW LENGTH (FEET) = 50.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.0 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 20.31  
 ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 60.70  
 PIPE TRAVEL TIME (MIN.) = 0.04 Tc (MIN.) = 12.03  
 LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3042.50 = 2448.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 3042.50 TO NODE 3043.70 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 433.00 DOWNSTREAM (FEET) = 431.00  
 CHANNEL LENGTH THRU SUBAREA (FEET) = 200.00 CHANNEL SLOPE = 0.0100  
 CHANNEL BASE (FEET) = 50.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.045 MAXIMUM DEPTH (FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 4.962  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 61.31  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 2.05  
 AVERAGE FLOW DEPTH (FEET) = 0.54 TRAVEL TIME (MIN.) = 1.62  
 Tc (MIN.) = 13.65  
 SUBAREA AREA (ACRES) = 0.70 SUBAREA RUNOFF (CFS) = 1.22  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.412  
 TOTAL AREA (ACRES) = 26.60 PEAK FLOW RATE (CFS) = 60.70



END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.54 FLOW VELOCITY(FEET/SEC.) = 2.04

LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3043.70 = 2648.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 3043.70 TO NODE 3043.70 IS CODE = 11

>>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

==  
\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	60.70	13.65	4.962	26.60

LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3043.70 = 2648.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	73.37	12.83	5.165	35.00

LONGEST FLOWPATH FROM NODE 3000.00 TO NODE 3043.70 = 2515.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	130.42	12.83	5.165
2	131.19	13.65	4.962

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 131.19 Tc(MIN.) = 13.65

TOTAL AREA(ACRES) = 61.60

\*\*\*\*\*

FLOW PROCESS FROM NODE 3043.70 TO NODE 3043.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 429.00 DOWNSTREAM(FEET) = 427.00

FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 42.0 INCH PIPE IS 33.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 16.00

ESTIMATED PIPE DIAMETER(INCH) = 42.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 131.19

PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 13.76

LONGEST FLOWPATH FROM NODE 3003.00 TO NODE 3043.00 = 2748.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 61.60 TC(MIN.) = 13.76

PEAK FLOW RATE(CFS) = 131.19

=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 4000**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Post-project (on-site) \*  
\* Drainage Basin 4000 \*  
\*\*\*\*\*

FILE NAME: MW\_4K100.DAT  
TIME/DATE OF STUDY: 12:14 07/13/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH	LIP	HIKE	MANNING FACTOR
NO.	(FT)	(FT)		(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.020/0.020/0.020	0.50	1.50	0.0100	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = -0.10 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4000.00 TO NODE 4001.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 462.50  
 DOWNSTREAM ELEVATION(FEET) = 437.00  
 ELEVATION DIFFERENCE(FEET) = 25.50  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 4001.00 TO NODE 4002.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 437.00 DOWNSTREAM(FEET) = 390.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 700.00 CHANNEL SLOPE = 0.0671  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 2.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.630  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.08  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.57  
 AVERAGE FLOW DEPTH(FEET) = 0.12 TRAVEL TIME(MIN.) = 4.54  
 Tc(MIN.) = 11.22  
 SUBAREA AREA(ACRES) = 3.00 SUBAREA RUNOFF(CFS) = 5.07  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 3.20 PEAK FLOW RATE(CFS) = 5.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.16 FLOW VELOCITY(FEET/SEC.) = 3.21  
 LONGEST FLOWPATH FROM NODE 4000.00 TO NODE 4002.00 = 800.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 4002.00 TO NODE 4002.10 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 390.00 DOWNSTREAM(FEET) = 384.00  
 FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 15.40  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 5.40  
 PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 11.27  
 LONGEST FLOWPATH FROM NODE 4000.00 TO NODE 4002.10 = 840.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 4002.10 TO NODE 4003.50 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 384.00 DOWNSTREAM(FEET) = 383.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 80.00 CHANNEL SLOPE = 0.0125
CHANNEL BASE(FEET) = 30.00 "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.045 MAXIMUM DEPTH(FEET) = 10.00
CHANNEL FLOW THRU SUBAREA(CFS) = 5.40
FLOW VELOCITY(FEET/SEC.) = 1.05 FLOW DEPTH(FEET) = 0.16
TRAVEL TIME(MIN.) = 1.27 Tc(MIN.) = 12.54
LONGEST FLOWPATH FROM NODE 4000.00 TO NODE 4003.50 = 920.00 FEET.

*****
FLOW PROCESS FROM NODE 4002.10 TO NODE 4002.10 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.54
RAINFALL INTENSITY(INCH/HR) = 5.24
TOTAL STREAM AREA(ACRES) = 3.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.40

*****
FLOW PROCESS FROM NODE 4004.00 TO NODE 4005.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6200
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 455.00
DOWNSTREAM ELEVATION(FEET) = 442.50
ELEVATION DIFFERENCE(FEET) = 12.50
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.011
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.76
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.76

*****
FLOW PROCESS FROM NODE 4005.00 TO NODE 4003.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 442.50 DOWNSTREAM ELEVATION(FEET) = 383.00
STREET LENGTH(FEET) = 800.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 30.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 20.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

```

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0150  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.06  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 11.68  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.57  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 2.22  
STREET FLOW TRAVEL TIME(MIN.) = 2.03 Tc(MIN.) = 6.04  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.397  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6200  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.620  
SUBAREA AREA(ACRES) = 6.60 SUBAREA RUNOFF(CFS) = 34.36  
TOTAL AREA(ACRES) = 6.90 PEAK FLOW RATE(CFS) = 35.92

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 15.04  
FLOW VELOCITY(FEET/SEC.) = 7.65 DEPTH\*VELOCITY(FT\*FT/SEC.) = 3.10  
LONGEST FLOWPATH FROM NODE 4004.00 TO NODE 4003.00 = 900.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4003.00 TO NODE 4003.50 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPE SIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	385.00	DOWNSTREAM(FEET) =	383.00
FLOW LENGTH(FEET) =	100.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	27.0 INCH PIPE IS	19.4 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	11.77		
ESTIMATED PIPE DIAMETER(INCH) =	27.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	35.92		
PIPE TRAVEL TIME(MIN.) =	0.14	Tc(MIN.) =	6.18
LONGEST FLOWPATH FROM NODE	4004.00 TO NODE	4003.50 =	1000.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4003.50 TO NODE 4003.50 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	6.18
RAINFALL INTENSITY(INCH/HR) =	8.27
TOTAL STREAM AREA(ACRES) =	6.90
PEAK FLOW RATE(CFS) AT CONFLUENCE =	35.92

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	5.40	12.54	5.242	3.20
2	35.92	6.18	8.272	6.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	38.58	6.18	8.272
2	28.17	12.54	5.242

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 38.58 Tc(MIN.) = 6.18

TOTAL AREA(ACRES) = 10.10

LONGEST FLOWPATH FROM NODE 4004.00 TO NODE 4003.50 = 1000.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4003.50 TO NODE 4006.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 382.50 DOWNSTREAM(FEET) = 380.00

FLOW LENGTH(FEET) = 210.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 22.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 9.80

ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 38.58

PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 6.54

LONGEST FLOWPATH FROM NODE 4004.00 TO NODE 4006.00 = 1210.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4006.00 TO NODE 4006.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 6.54

RAINFALL INTENSITY(INCH/HR) = 7.98

TOTAL STREAM AREA(ACRES) = 10.10

PEAK FLOW RATE(CFS) AT CONFLUENCE = 38.58

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4007.00 TO NODE 4008.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 445.50

DOWNSTREAM ELEVATION(FEET) = 425.00

ELEVATION DIFFERENCE(FEET) = 20.50

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865

SUBAREA RUNOFF(CFS) = 0.47

TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 0.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4008.00 TO NODE 4006.00 IS CODE = 51  
-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) =	425.00	DOWNSTREAM (FEET) =	381.00
CHANNEL LENGTH THRU SUBAREA (FEET) =	910.00	CHANNEL SLOPE =	0.0484
CHANNEL BASE (FEET) =	10.00	"Z" FACTOR =	2.000
MANNING'S FACTOR =	0.035	MAXIMUM DEPTH (FEET) =	10.00
100 YEAR RAINFALL INTENSITY (INCH/HOUR) =	4.424		

\*USER SPECIFIED (SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 1.05  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 1.57  
AVERAGE FLOW DEPTH (FEET) = 0.07 TRAVEL TIME (MIN.) = 9.63  
Tc (MIN.) = 16.31  
SUBAREA AREA (ACRES) = 0.90 SUBAREA RUNOFF (CFS) = 1.11  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.284  
TOTAL AREA (ACRES) = 1.10 PEAK FLOW RATE (CFS) = 1.38

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH (FEET) = 0.08 FLOW VELOCITY (FEET/SEC.) = 1.72  
LONGEST FLOWPATH FROM NODE 4007.00 TO NODE 4006.00 = 1010.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 4006.00 TO NODE 4006.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION (MIN.) = 16.31  
RAINFALL INTENSITY (INCH/HR) = 4.42  
TOTAL STREAM AREA (ACRES) = 1.10  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 1.38

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	38.58	6.54	7.978	10.10
2	1.38	16.31	4.424	1.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	39.14	6.54	7.978
2	22.77	16.31	4.424

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:



PEAK FLOW RATE(CFS) = 39.14 Tc(MIN.) = 6.54  
 TOTAL AREA(ACRES) = 11.20  
 LONGEST FLOWPATH FROM NODE 4004.00 TO NODE 4006.00 = 1210.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 4006.00 TO NODE 4009.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 381.00 DOWNSTREAM(FEET) = 380.00

FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 15.49

ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 39.14

PIPE TRAVEL TIME(MIN.) = 0.03 Tc(MIN.) = 6.57

LONGEST FLOWPATH FROM NODE 4004.00 TO NODE 4009.00 = 1235.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 11.20 TC(MIN.) = 6.57

PEAK FLOW RATE(CFS) = 39.14

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 7000A**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003, 1985, 1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 07/16/09 \*  
\* 100-yr Post-project (on-site) \*  
\* Drainage Basin 7000 \*  
\*\*\*\*\*

FILE NAME: MW\_7K10A.DAT  
TIME/DATE OF STUDY: 10:37 07/20/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	18.0	13.0	0.020/0.020/0.020	0.50	1.50	0.0100	0.125	0.0180

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7000.00 TO NODE 7000.10 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA) :  
USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 758.00  
 DOWNSTREAM ELEVATION(FEET) = 748.00  
 ELEVATION DIFFERENCE(FEET) = 10.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.431  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.992  
 SUBAREA RUNOFF(CFS) = 2.83  
 TOTAL AREA(ACRES) = 0.70 TOTAL RUNOFF(CFS) = 2.83

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7000.10 TO NODE 7001.20 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<

=====  
 UPSTREAM ELEVATION(FEET) = 748.00 DOWNSTREAM ELEVATION(FEET) = 670.00  
 STREET LENGTH(FEET) = 700.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.15  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.28  
 HALFSTREET FLOOD WIDTH(FEET) = 8.99  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.76  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.64  
 STREET FLOW TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 7.46  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.331  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.450  
 SUBAREA AREA(ACRES) = 1.40 SUBAREA RUNOFF(CFS) = 4.62  
 TOTAL AREA(ACRES) = 2.10 PEAK FLOW RATE(CFS) = 6.93

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 10.15  
 FLOW VELOCITY(FEET/SEC.) = 6.20 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.91  
 LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7001.20 = 800.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7001.20 TO NODE 7001.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.46

RAINFALL INTENSITY(INCH/HR) = 7.33  
 TOTAL STREAM AREA(ACRES) = 2.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.93

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7001.00 TO NODE 7001.10 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 760.00  
 DOWNSTREAM ELEVATION(FEET) = 730.00  
 ELEVATION DIFFERENCE(FEET) = 30.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7001.10 TO NODE 7001.20 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 730.00 DOWNSTREAM(FEET) = 670.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 200.00 CHANNEL SLOPE = 0.3000  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.056

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.22  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.72  
 AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 1.23  
 Tc(MIN.) = 7.91  
 SUBAREA AREA(ACRES) = 0.70 SUBAREA RUNOFF(CFS) = 1.48  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 1.91

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.06 FLOW VELOCITY(FEET/SEC.) = 3.21  
 LONGEST FLOWPATH FROM NODE 7001.00 TO NODE 7001.20 = 300.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7001.20 TO NODE 7001.20 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.91

RAINFALL INTENSITY (INCH/HR) = 7.06  
TOTAL STREAM AREA (ACRES) = 0.90  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 1.91

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.93	7.46	7.331	2.10
2	1.91	7.91	7.056	0.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	8.72	7.46	7.331
2	8.57	7.91	7.056

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 8.72 Tc (MIN.) = 7.46  
TOTAL AREA (ACRES) = 3.00  
LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7001.20 = 800.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7001.20 TO NODE 7002.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 670.00 DOWNSTREAM (FEET) = 620.00  
CHANNEL LENGTH THRU SUBAREA (FEET) = 170.00 CHANNEL SLOPE = 0.2941  
CHANNEL BASE (FEET) = 3.00 "Z" FACTOR = 1.500  
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00  
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.148  
\*USER SPECIFIED (SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 10.76  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 9.55  
AVERAGE FLOW DEPTH (FEET) = 0.32 TRAVEL TIME (MIN.) = 0.30  
Tc (MIN.) = 7.75  
SUBAREA AREA (ACRES) = 1.90 SUBAREA RUNOFF (CFS) = 4.07  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.364  
TOTAL AREA (ACRES) = 4.90 PEAK FLOW RATE (CFS) = 12.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 0.36 FLOW VELOCITY (FEET/SEC.) = 10.15  
LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7002.00 = 970.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7002.00 TO NODE 7015.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 610.00 DOWNSTREAM (FEET) = 554.00

FLOW LENGTH(FEET) = 320.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 20.74  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 12.76  
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 8.01  
 LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7015.00 = 1290.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7015.00 TO NODE 7015.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====  
 TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.01  
 RAINFALL INTENSITY(INCH/HR) = 7.00  
 TOTAL STREAM AREA(ACRES) = 4.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.76

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7004.00 TO NODE 7005.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00  
 UPSTREAM ELEVATION(FEET) = 680.00  
 DOWNSTREAM ELEVATION(FEET) = 660.00  
 ELEVATION DIFFERENCE(FEET) = 20.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.178  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.274  
 SUBAREA RUNOFF(CFS) = 0.56  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.56

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7005.00 TO NODE 7006.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 660.00 DOWNSTREAM(FEET) = 603.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 300.00 CHANNEL SLOPE = 0.1900  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.022  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.31  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.83  
 AVERAGE FLOW DEPTH(FEET) = 0.10 TRAVEL TIME(MIN.) = 1.31  
 Tc(MIN.) = 6.48

SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 7.46  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
TOTAL AREA(ACRES) = 3.30 PEAK FLOW RATE(CFS) = 7.94

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.15 FLOW VELOCITY(FEET/SEC.) = 4.68  
LONGEST FLOWPATH FROM NODE 7004.00 TO NODE 7006.00 = 360.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7006.00 TO NODE 7015.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 603.00 DOWNSTREAM ELEVATION(FEET) = 564.00  
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.01  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.28  
HALFSTREET FLOOD WIDTH(FEET) = 8.73  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 6.49  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.81  
STREET FLOW TRAVEL TIME(MIN.) = 0.69 Tc(MIN.) = 7.18  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.513

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.393  
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 6.15  
TOTAL AREA(ACRES) = 4.60 PEAK FLOW RATE(CFS) = 13.59

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 9.54  
FLOW VELOCITY(FEET/SEC.) = 6.81 DEPTH\*VELOCITY(FT\*FT/SEC.) = 2.02  
LONGEST FLOWPATH FROM NODE 7004.00 TO NODE 7015.00 = 630.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7015.00 TO NODE 7015.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.18  
RAINFALL INTENSITY(INCH/HR) = 7.51  
TOTAL STREAM AREA(ACRES) = 4.60



PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.59

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7007.00 TO NODE 7008.00 IS CODE = 21  
-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 85.00  
UPSTREAM ELEVATION(FEET) = 790.00  
DOWNSTREAM ELEVATION(FEET) = 750.00  
ELEVATION DIFFERENCE(FEET) = 40.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.163  
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.288  
SUBAREA RUNOFF(CFS) = 0.50  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.50

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7008.00 TO NODE 7015.00 IS CODE = 51  
-----

>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 750.00 DOWNSTREAM(FEET) = 600.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 440.00 CHANNEL SLOPE = 0.3409  
CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.962  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.94  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.83  
AVERAGE FLOW DEPTH(FEET) = 0.07 TRAVEL TIME(MIN.) = 1.91  
Tc(MIN.) = 8.08  
SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 4.80  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 5.22

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 4.94  
LONGEST FLOWPATH FROM NODE 7007.00 TO NODE 7015.00 = 525.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7015.00 TO NODE 7015.00 IS CODE = 1  
-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
TIME OF CONCENTRATION(MIN.) = 8.08  
RAINFALL INTENSITY(INCH/HR) = 6.96  
TOTAL STREAM AREA(ACRES) = 2.50

PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.22

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	12.76	8.01	6.999	4.90
2	13.59	7.18	7.513	4.60
3	5.22	8.08	6.962	2.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	30.12	7.18	7.513
2	30.60	8.01	6.999
3	30.51	8.08	6.962

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 30.60 Tc(MIN.) = 8.01

TOTAL AREA(ACRES) = 12.00

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7015.00 = 1290.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7015.00 TO NODE 7022.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<< .

=====

ELEVATION DATA: UPSTREAM( FEET) =	554.00	DOWNSTREAM( FEET) =	510.00
FLOW LENGTH( FEET) =	280.00	MANNING'S N =	0.013
DEPTH OF FLOW IN . 18.0 INCH PIPE IS	11.9 INCHES		
PIPE-FLOW VELOCITY( FEET/SEC.) =	24.69		
ESTIMATED PIPE DIAMETER( INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW( CFS) =	30.60		
PIPE TRAVEL TIME( MIN.) =	0.19	Tc( MIN.) =	8.20
LONGEST FLOWPATH FROM NODE	7000.00	TO NODE	7022.00 = 1570.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7022.00 TO NODE 7022.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION( MIN.) =	8.20
RAINFALL INTENSITY( INCH/HR) =	6.89
TOTAL STREAM AREA( ACRES) =	12.00
PEAK FLOW RATE( CFS) AT CONFLUENCE =	30.60

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7017.00 TO NODE 7018.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED (SUBAREA) :

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 630.00  
 DOWNSTREAM ELEVATION(FEET) = 565.00  
 ELEVATION DIFFERENCE(FEET) = 65.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7018.00 TO NODE 7022.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 565.00 DOWNSTREAM(FEET) = 515.00  
 FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.016  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.09  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.47  
 PIPE TRAVEL TIME(MIN.) = 1.09 Tc(MIN.) = 7.78  
 LONGEST FLOWPATH FROM NODE 7017.00 TO NODE 7022.00 = 500.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7018.00 TO NODE 7022.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<  
 =====  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.132  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3000  
 SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 1.93  
 TOTAL AREA(ACRES) = 1.10 TOTAL RUNOFF(CFS) = 2.35  
 TC(MIN.) = 7.78

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7022.00 TO NODE 7022.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 =====  
 TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.78  
 RAINFALL INTENSITY(INCH/HR) = 7.13  
 TOTAL STREAM AREA(ACRES) = 1.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.35

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7020.00 TO NODE 7021.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 551.00  
DOWNSTREAM ELEVATION(FEET) = 550.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517  
SUBAREA RUNOFF(CFS) = 1.07  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.07

\*\*\*\*\*

FLOW PROCESS FROM NODE 7021.00 TO NODE 7022.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 550.00 DOWNSTREAM ELEVATION(FEET) = 515.00  
STREET LENGTH(FEET) = 300.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.00  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.20  
HALFSTREET FLOOD WIDTH(FEET) = 4.97  
AVERAGE FLOW VELOCITY(FT/SEC.) = 4.49  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.92  
STREET FLOW TRAVEL TIME(MIN.) = 1.11 Tc(MIN.) = 7.02  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.619

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 3.84  
TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 4.80

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.23 HALFSTREET FLOOD WIDTH(FEET) = 6.29  
FLOW VELOCITY(FT/SEC.) = 4.97 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.15  
LONGEST FLOWPATH FROM NODE 7020.00 TO NODE 7022.00 = 365.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7022.00 TO NODE 7022.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

```
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION (MIN.) = 7.02
RAINFALL INTENSITY (INCH/HR) = 7.62
TOTAL STREAM AREA (ACRES) = 1.00
PEAK FLOW RATE (CFS) AT CONFLUENCE = 4.80
```

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	30.60	8.20	6.895	12.00
2	2.35	7.78	7.132	1.10
3	4.80	7.02	7.619	1.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	34.62	7.02	7.619
2	36.43	7.78	7.132
3	37.22	8.20	6.895

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE (CFS) = 37.22 Tc (MIN.) = 8.20
TOTAL AREA (ACRES) = 14.10
LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7022.00 = 1570.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 7022.00 TO NODE 7022.50 IS CODE = 31
-----
```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

```
=====
ELEVATION DATA: UPSTREAM (FEET) = 508.00 DOWNSTREAM (FEET) = 507.00
FLOW LENGTH (FEET) = 200.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.0 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 7.09
ESTIMATED PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 37.22
PIPE TRAVEL TIME (MIN.) = 0.47 Tc (MIN.) = 8.67
LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7022.50 = 1770.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE 7022.50 TO NODE 7022.50 IS CODE = 10
-----
```

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

```
*****
FLOW PROCESS FROM NODE 7024.00 TO NODE 7025.00 IS CODE = 21
-----
```

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

*USER SPECIFIED (SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00
UPSTREAM ELEVATION (FEET) = 680.00
DOWNSTREAM ELEVATION (FEET) = 643.00
ELEVATION DIFFERENCE (FEET) = 37.00
SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.684
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 7.865
SUBAREA RUNOFF (CFS) = 0.71
TOTAL AREA (ACRES) = 0.30 TOTAL RUNOFF (CFS) = 0.71

*****
FLOW PROCESS FROM NODE 7025.00 TO NODE 7026.00 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<
=====
ELEVATION DATA: UPSTREAM (FEET) = 643.00 DOWNSTREAM (FEET) = 510.00
CHANNEL LENGTH THRU SUBAREA (FEET) = 740.00 CHANNEL SLOPE = 0.1797
CHANNEL BASE (FEET) = 2.00 "Z" FACTOR = 1.000
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 2.00
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.727
*USER SPECIFIED (SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 4.16
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 6.73
AVERAGE FLOW DEPTH (FEET) = 0.27 TRAVEL TIME (MIN.) = 1.83
Tc (MIN.) = 8.52
SUBAREA AREA (ACRES) = 3.40 SUBAREA RUNOFF (CFS) = 6.86
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
TOTAL AREA (ACRES) = 3.70 PEAK FLOW RATE (CFS) = 7.47

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH (FEET) = 0.39 FLOW VELOCITY (FEET/SEC.) = 8.10
LONGEST FLOWPATH FROM NODE 7024.00 TO NODE 7026.00 = 840.00 FEET.

*****
FLOW PROCESS FROM NODE 7026.00 TO NODE 7023.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM (FEET) = 510.00 DOWNSTREAM (FEET) = 508.00
FLOW LENGTH (FEET) = 340.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.4 INCHES
PIPE-FLOW VELOCITY (FEET/SEC.) = 4.94
ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW (CFS) = 7.47
PIPE TRAVEL TIME (MIN.) = 1.15 Tc (MIN.) = 9.66
LONGEST FLOWPATH FROM NODE 7024.00 TO NODE 7023.00 = 1180.00 FEET.

*****
FLOW PROCESS FROM NODE 7023.00 TO NODE 7023.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.66
RAINFALL INTENSITY(INCH/HR) = 6.20
TOTAL STREAM AREA(ACRES) = 3.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.47

*****
FLOW PROCESS FROM NODE 7040.00 TO NODE 7041.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 515.00
DOWNSTREAM ELEVATION(FEET) = 514.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517
SUBAREA RUNOFF(CFS) = 1.61
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.61

*****
FLOW PROCESS FROM NODE 7041.00 TO NODE 7023.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 514.00 DOWNSTREAM ELEVATION(FEET) = 508.00
STREET LENGTH(FEET) = 300.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.89
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.31
HALFSTREET FLOOD WIDTH(FEET) = 10.15
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.64
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.81
STREET FLOW TRAVEL TIME(MIN.) = 1.90 Tc(MIN.) = 7.81
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.117
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630

```

SUBAREA AREA (ACRES) = 1.90 SUBAREA RUNOFF (CFS) = 8.52  
 TOTAL AREA (ACRES) = 2.20 PEAK FLOW RATE (CFS) = 9.86

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.36 HALFSTREET FLOOD WIDTH (FEET) = 12.54  
 FLOW VELOCITY (FEET/SEC.) = 2.97 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.06  
 LONGEST FLOWPATH FROM NODE 7040.00 TO NODE 7023.00 = 365.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7023.00 TO NODE 7023.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION (MIN.) =	7.81
RAINFALL INTENSITY (INCH/HR) =	7.12
TOTAL STREAM AREA (ACRES) =	2.20
PEAK FLOW RATE (CFS) AT CONFLUENCE =	9.86

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.47	9.66	6.201	3.70
2	9.86	7.81	7.117	2.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	15.89	7.81	7.117
2	16.06	9.66	6.201

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 16.06 Tc (MIN.) = 9.66  
 TOTAL AREA (ACRES) = 5.90  
 LONGEST FLOWPATH FROM NODE 7024.00 TO NODE 7023.00 = 1180.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7023.00 TO NODE 7022.50 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) =	508.00	DOWNSTREAM (FEET) =	507.00
FLOW LENGTH (FEET) =	70.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS	15.5 INCHES		
PIPE-FLOW VELOCITY (FEET/SEC.) =	8.46		
ESTIMATED PIPE DIAMETER (INCH) =	21.00	NUMBER OF PIPES =	1
PIPE-FLOW (CFS) =	16.06		
PIPE TRAVEL TIME (MIN.) =	0.14	Tc (MIN.) =	9.80
LONGEST FLOWPATH FROM NODE 7024.00 TO NODE 7022.50 =	1250.00 FEET.		

\*\*\*\*\*



FLOW PROCESS FROM NODE 7022.50 TO NODE 7022.50 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	16.06	9.80	6.144	5.90

LONGEST FLOWPATH FROM NODE 7024.00 TO NODE 7022.50 = 1250.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	37.22	8.67	6.651	14.10

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7022.50 = 1770.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	51.42	8.67	6.651
2	50.44	9.80	6.144

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 51.42 Tc(MIN.) = 8.67

TOTAL AREA(ACRES) = 20.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7022.50 TO NODE 7022.50 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7022.50 TO NODE 7030.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM( FEET) = 507.00 DOWNSTREAM( FEET) = 458.00

FLOW LENGTH( FEET) = 550.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.3 INCHES

PIPE-FLOW VELOCITY( FEET/SEC.) = 22.71

ESTIMATED PIPE DIAMETER( INCH) = 24.00 NUMBER OF PIPES = 1

PIPE-FLOW( CFS) = 51.42

PIPE TRAVEL TIME( MIN.) = 0.40 Tc( MIN.) = 9.07

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7030.00 = 2320.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7030.00 TO NODE 7030.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION( MIN.) = 9.07

RAINFALL INTENSITY( INCH/HR) = 6.46

TOTAL STREAM AREA(ACRES) = 20.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 51.42

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7028.00 TO NODE 7029.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 511.00  
DOWNSTREAM ELEVATION(FEET) = 510.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517  
SUBAREA RUNOFF(CFS) = 1.07  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.07

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7029.00 TO NODE 7030.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 510.00 DOWNSTREAM ELEVATION(FEET) = 468.00  
STREET LENGTH(FEET) = 490.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.25  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 8.17  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.81  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.29  
STREET FLOW TRAVEL TIME(MIN.) = 1.70 Tc(MIN.) = 7.61  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.236

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
SUBAREA AREA(ACRES) = 2.70 SUBAREA RUNOFF(CFS) = 12.31  
TOTAL AREA(ACRES) = 2.90 PEAK FLOW RATE(CFS) = 13.22

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 10.51  
FLOW VELOCITY(FEET/SEC.) = 5.55 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.75

LONGEST FLOWPATH FROM NODE 7028.00 TO NODE 7030.00 = 555.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7030.00 TO NODE 7030.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.61  
RAINFALL INTENSITY(INCH/HR) = 7.24  
TOTAL STREAM AREA(ACRES) = 2.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.22

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	51.42	9.07	6.459	20.00
2	13.22	7.61	7.236	2.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	56.34	7.61	7.236
2	63.22	9.07	6.459

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 63.22 Tc(MIN.) = 9.07

TOTAL AREA(ACRES) = 22.90

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7030.00 = 2320.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7030.00 TO NODE 7043.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 458.00 DOWNSTREAM(FEET) = 453.00  
FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.97  
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 63.22  
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 9.12  
LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7043.00 = 2390.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7043.00 TO NODE 7043.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 9.12  
 RAINFALL INTENSITY(INCH/HR) = 6.43  
 TOTAL STREAM AREA(ACRES) = 22.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 63.22

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7042.00 TO NODE 7042.50 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 520.00  
 DOWNSTREAM ELEVATION(FEET) = 508.00  
 ELEVATION DIFFERENCE(FEET) = 12.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.979  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.452  
 SUBAREA RUNOFF(CFS) = 3.55  
 TOTAL AREA(ACRES) = 1.40 TOTAL RUNOFF(CFS) = 3.55

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7042.50 TO NODE 7043.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 460.00 DOWNSTREAM(FEET) = 453.00  
 FLOW LENGTH(FEET) = 270.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.31  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.55  
 PIPE TRAVEL TIME(MIN.) = 0.62 Tc(MIN.) = 6.59  
 LONGEST FLOWPATH FROM NODE 7042.00 TO NODE 7043.00 = 350.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7043.00 TO NODE 7043.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.59  
 RAINFALL INTENSITY(INCH/HR) = 7.93  
 TOTAL STREAM AREA(ACRES) = 1.40  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.55

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	63.22	9.12	6.435	22.90
2	3.55	6.59	7.934	1.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	54.82	6.59	7.934
2	66.10	9.12	6.435

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 66.10 Tc(MIN.) = 9.12

TOTAL AREA(ACRES) = 24.30

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7043.00 = 2390.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7043.00 TO NODE 7043.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 7032.00 TO NODE 7033.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00

UPSTREAM ELEVATION(FEET) = 499.00

DOWNSTREAM ELEVATION(FEET) = 498.00

ELEVATION DIFFERENCE(FEET) = 1.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517

SUBAREA RUNOFF(CFS) = 1.61

TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.61

\*\*\*\*\*

FLOW PROCESS FROM NODE 7033.00 TO NODE 7034.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 498.00 DOWNSTREAM ELEVATION(FEET) = 482.00

STREET LENGTH(FEET) = 350.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.75  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.27  
 HALFSTREET FLOOD WIDTH(FEET) = 8.48  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.57  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.98  
 STREET FLOW TRAVEL TIME(MIN.) = 1.63 Tc(MIN.) = 7.54  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.276  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
 SUBAREA AREA(ACRES) = 1.80 SUBAREA RUNOFF(CFS) = 8.25  
 TOTAL AREA(ACRES) = 2.10 PEAK FLOW RATE(CFS) = 9.63

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 10.51  
 FLOW VELOCITY(FEET/SEC.) = 4.04 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.27  
 LONGEST FLOWPATH FROM NODE 7032.00 TO NODE 7034.00 = 415.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7034.00 TO NODE 7038.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 472.00 DOWNSTREAM(FEET) = 455.00  
 FLOW LENGTH(FEET) = 460.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.85  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 9.63  
 PIPE TRAVEL TIME(MIN.) = 0.71 Tc(MIN.) = 8.25  
 LONGEST FLOWPATH FROM NODE 7032.00 TO NODE 7038.00 = 875.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7038.00 TO NODE 7038.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.25  
 RAINFALL INTENSITY(INCH/HR) = 6.87  
 TOTAL STREAM AREA(ACRES) = 2.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.63

\*\*\*\*\*

FLOW PROCESS FROM NODE 7036.00 TO NODE 7037.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00

```

UPSTREAM ELEVATION(FEET) = 492.00
DOWNSTREAM ELEVATION(FEET) = 491.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517
SUBAREA RUNOFF(CFS) = 1.07
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.07

*****
FLOW PROCESS FROM NODE 7037.00 TO NODE 7038.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 491.00 DOWNSTREAM ELEVATION(FEET) = 465.00
STREET LENGTH(FEET) = 640.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.10
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 10.51
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.82
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.20
STREET FLOW TRAVEL TIME(MIN.) = 2.79 Tc(MIN.) = 8.70
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.635
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630
SUBAREA AREA(ACRES) = 3.80 SUBAREA RUNOFF(CFS) = 15.88
TOTAL AREA(ACRES) = 4.00 PEAK FLOW RATE(CFS) = 16.72

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 13.46
FLOW VELOCITY(FEET/SEC.) = 4.41 DEPTH*VELOCITY(FT*FT/SEC.) = 1.65
LONGEST FLOWPATH FROM NODE 7036.00 TO NODE 7038.00 = 705.00 FEET.

*****
FLOW PROCESS FROM NODE 7038.00 TO NODE 7038.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.70
RAINFALL INTENSITY(INCH/HR) = 6.64

```

TOTAL STREAM AREA (ACRES) = 4.00  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 16.72

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.63	8.25	6.868	2.10
2	16.72	8.70	6.635	4.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	25.48	8.25	6.868
2	26.02	8.70	6.635

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 26.02 Tc (MIN.) = 8.70  
 TOTAL AREA (ACRES) = 6.10  
 LONGEST FLOWPATH FROM NODE 7032.00 TO NODE 7038.00 = 875.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7038.00 TO NODE 7043.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 465.00 DOWNSTREAM (FEET) = 453.00  
 FLOW LENGTH (FEET) = 60.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER (INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.9 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 26.19  
 ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 26.02  
 PIPE TRAVEL TIME (MIN.) = 0.04 Tc (MIN.) = 8.74  
 LONGEST FLOWPATH FROM NODE 7032.00 TO NODE 7043.00 = 935.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7043.00 TO NODE 7043.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	26.02	8.74	6.616	6.10

LONGEST FLOWPATH FROM NODE 7032.00 TO NODE 7043.00 = 935.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	66.10	9.12	6.435	24.30

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7043.00 = 2390.00 FEET.



\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	89.33	8.74	6.616
2	91.41	9.12	6.435

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 91.41 Tc (MIN.) = 9.12  
 TOTAL AREA (ACRES) = 30.40

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7043.00 TO NODE 7043.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7043.00 TO NODE 7047.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

ELEVATION DATA: UPSTREAM (FEET) = 463.00 DOWNSTREAM (FEET) = 407.00  
 FLOW LENGTH (FEET) = 510.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.8 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 27.84  
 ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 91.41  
 PIPE TRAVEL TIME (MIN.) = 0.31 Tc (MIN.) = 9.43  
 LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7047.00 = 2900.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7047.00 TO NODE 4047.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 9.43  
 RAINFALL INTENSITY (INCH/HR) = 6.30  
 TOTAL STREAM AREA (ACRES) = 30.40  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 91.41

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7045.00 TO NODE 7046.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 65.00  
 UPSTREAM ELEVATION (FEET) = 461.00  
 DOWNSTREAM ELEVATION (FEET) = 460.00  
 ELEVATION DIFFERENCE (FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.160  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.291

```

SUBAREA RUNOFF(CFS) =          2.02
TOTAL AREA(ACRES) =          0.40   TOTAL RUNOFF(CFS) =          2.02

*****
FLOW PROCESS FROM NODE    7046.00 TO NODE    7047.00 IS CODE =    62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #    1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =  460.00  DOWNSTREAM ELEVATION(FEET) =  417.00
STREET LENGTH(FEET) =    470.00   CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =    18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =    13.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =    0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    2
STREET PARKWAY CROSSFALL(DECIMAL) =    0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) =    0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =    0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =          9.88
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =    0.29
HALFSTREET FLOOD WIDTH( FEET) =    9.19
AVERAGE FLOW VELOCITY( FEET/SEC.) =    5.31
PRODUCT OF DEPTH&VELOCITY( FT*FT/SEC.) =    1.53
STREET FLOW TRAVEL TIME(MIN.) =    1.48   Tc(MIN.) =    7.64
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    7.218
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT =    .6200
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT =    0.619
SUBAREA AREA(ACRES) =    3.50   SUBAREA RUNOFF(CFS) =    15.66
TOTAL AREA(ACRES) =    3.90   PEAK FLOW RATE(CFS) =    17.43

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH( FEET) =    0.34   HALFSTREET FLOOD WIDTH( FEET) =    11.63
FLOW VELOCITY( FEET/SEC.) =    6.06   DEPTH*VELOCITY( FT*FT/SEC.) =    2.04
LONGEST FLOWPATH FROM NODE    7045.00 TO NODE    7047.00 =    535.00 FEET.

*****
FLOW PROCESS FROM NODE    7047.00 TO NODE    7047.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    2 ARE:
TIME OF CONCENTRATION(MIN.) =    7.64
RAINFALL INTENSITY(INCH/HR) =    7.22
TOTAL STREAM AREA(ACRES) =    3.90
PEAK FLOW RATE(CFS) AT CONFLUENCE =    17.43

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA

```

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	91.41	9.43	6.300	30.40
2	17.43	7.64	7.218	3.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

**\*\* PEAK FLOW RATE TABLE \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	91.44	7.64	7.218
2	106.62	9.43	6.300

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 106.62 Tc (MIN.) = 9.43

TOTAL AREA (ACRES) = 34.30

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7047.00 = 2900.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7047.00 TO NODE 7056.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 407.00 DOWNSTREAM (FEET) = 402.00

FLOW LENGTH (FEET) = 70.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 33.0 INCH PIPE IS 22.2 INCHES

PIPE-FLOW VELOCITY (FEET/SEC.) = 25.05

ESTIMATED PIPE DIAMETER (INCH) = 33.00 NUMBER OF PIPES = 1

PIPE-FLOW (CFS) = 106.62

PIPE TRAVEL TIME (MIN.) = 0.05 Tc (MIN.) = 9.48

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7056.00 = 2970.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7056.00 TO NODE 7056.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7049.00 TO NODE 7050.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00

UPSTREAM ELEVATION (FEET) = 474.00

DOWNSTREAM ELEVATION (FEET) = 452.00

ELEVATION DIFFERENCE (FEET) = 22.00

SUBAREA OVERLAND TIME OF FLOW (MIN.) = 4.094

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF (CFS) = 1.16

TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 1.16

```

*****
FLOW PROCESS FROM NODE    7050.00 TO NODE    7051.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   452.00  DOWNSTREAM(FEET) =   425.00
FLOW LENGTH(FEET) =   240.00  MANNING'S N =  0.016
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   2.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    7.63
ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =      1.16
PIPE TRAVEL TIME(MIN.) =    0.52    Tc(MIN.) =    4.62
LONGEST FLOWPATH FROM NODE    7049.00 TO NODE    7051.00 =   340.00 FEET.

*****
FLOW PROCESS FROM NODE    7050.00 TO NODE    7051.00 IS CODE =  81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3900
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.4300
SUBAREA AREA(ACRES) =    0.90  SUBAREA RUNOFF(CFS) =    3.33
TOTAL AREA(ACRES) =    1.10  TOTAL RUNOFF(CFS) =    4.49
TC(MIN.) =    4.62

*****
FLOW PROCESS FROM NODE    7051.00 TO NODE    7051.20 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   420.00  DOWNSTREAM(FEET) =   410.00
FLOW LENGTH(FEET) =   100.00  MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   4.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   12.63
ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =      4.49
PIPE TRAVEL TIME(MIN.) =    0.13    Tc(MIN.) =    4.75
LONGEST FLOWPATH FROM NODE    7049.00 TO NODE    7051.20 =   440.00 FEET.

*****
FLOW PROCESS FROM NODE    7051.20 TO NODE    7051.20 IS CODE =   1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    4.75
RAINFALL INTENSITY(INCH/HR) =    9.49

```

TOTAL STREAM AREA(ACRES) = 1.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.49

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+-----+
| Flow information for Node 6010 |
+-----+
  
```

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6010.00 TO NODE 6010.00 IS CODE = 7  
 -----

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:

TC(MIN) = 9.04 RAIN INTENSITY(INCH/HOUR) = 6.47  
 TOTAL AREA(ACRES) = 4.00 TOTAL RUNOFF(CFS) = 15.17

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6010.00 TO NODE 7051.20 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 411.00 DOWNSTREAM( FEET) = 410.00  
 FLOW LENGTH( FEET) = 80.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.6 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 7.93  
 ESTIMATED PIPE DIAMETER( INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 15.17  
 PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 9.21  
 LONGEST FLOWPATH FROM NODE 7045.00 TO NODE 7051.20 = 615.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7051.20 TO NODE 7051.20 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.21  
 RAINFALL INTENSITY(INCH/HR) = 6.40  
 TOTAL STREAM AREA(ACRES) = 4.00  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.17

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.49	4.75	9.485	1.10
2	15.17	9.21	6.397	4.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM	RUNOFF	Tc	INTENSITY
--------	--------	----	-----------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)
1	12.31	4.75	9.485
2	18.20	9.21	6.397

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 18.20 Tc(MIN.) = 9.21  
 TOTAL AREA(ACRES) = 5.10  
 LONGEST FLOWPATH FROM NODE 7045.00 TO NODE 7051.20 = 615.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7051.20 TO NODE 7055.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 410.00 DOWNSTREAM(FEET) = 405.00  
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 16.25  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 18.20  
 PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 9.28  
 LONGEST FLOWPATH FROM NODE 7045.00 TO NODE 7055.00 = 685.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7055.00 TO NODE 7055.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 =====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.28  
 RAINFALL INTENSITY(INCH/HR) = 6.37  
 TOTAL STREAM AREA(ACRES) = 5.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.20

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7053.00 TO NODE 7054.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 =====  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 418.00  
 DOWNSTREAM ELEVATION(FEET) = 417.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.657  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.759  
 SUBAREA RUNOFF(CFS) = 1.14  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.14

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7054.00 TO NODE 7055.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 417.00 DOWNSTREAM ELEVATION(FEET) = 415.00  
STREET LENGTH(FEET) = 90.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.73  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.25  
HALFSTREET FLOOD WIDTH(FEET) = 7.16  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.28  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.57  
STREET FLOW TRAVEL TIME(MIN.) = 0.66 Tc(MIN.) = 6.31  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.159  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6500  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.650  
SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 3.18  
TOTAL AREA(ACRES) = 0.80 PEAK FLOW RATE(CFS) = 4.24

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.28 HALFSTREET FLOOD WIDTH(FEET) = 8.68  
FLOW VELOCITY(FEET/SEC.) = 2.53 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.70  
LONGEST FLOWPATH FROM NODE 7053.00 TO NODE 7055.00 = 155.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7055.00 TO NODE 7055.00 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.31  
RAINFALL INTENSITY(INCH/HR) = 8.16  
TOTAL STREAM AREA(ACRES) = 0.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.24

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	18.20	9.28	6.365	5.10
2	4.24	6.31	8.159	0.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	18.44	6.31	8.159
2	21.51	9.28	6.365

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 21.51 Tc(MIN.) = 9.28  
 TOTAL AREA(ACRES) = 5.90  
 LONGEST FLOWPATH FROM NODE 7045.00 TO NODE 7055.00 = 685.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7055.00 TO NODE 7056.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 405.00 DOWNSTREAM( FEET) = 402.00  
 FLOW LENGTH( FEET) = 40.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.0 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 17.11  
 ESTIMATED PIPE DIAMETER( INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 21.51  
 PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 9.32  
 LONGEST FLOWPATH FROM NODE 7045.00 TO NODE 7056.00 = 725.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7056.00 TO NODE 7056.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	21.51	9.32	6.348	5.90

LONGEST FLOWPATH FROM NODE 7045.00 TO NODE 7056.00 = 725.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	106.62	9.48	6.280	34.30

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7056.00 = 2970.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	126.35	9.32	6.348
2	127.89	9.48	6.280

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 127.89 Tc(MIN.) = 9.48  
 TOTAL AREA(ACRES) = 40.20

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7056.00 TO NODE 7056.00 IS CODE = 12



```

>>>>>CLEAR MEMORY BANK # 1 <<<<<
=====
*****
FLOW PROCESS FROM NODE    7056.00 TO NODE    7060.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   402.00 DOWNSTREAM(FEET) =   346.00
FLOW LENGTH(FEET) =   535.00 MANNING'S N =   0.013
DEPTH OF FLOW IN  33.0 INCH PIPE IS  22.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   30.28
ESTIMATED PIPE DIAMETER(INCH) =   33.00 NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =   127.89
PIPE TRAVEL TIME(MIN.) =    0.29 Tc(MIN.) =    9.77
LONGEST FLOWPATH FROM NODE    7000.00 TO NODE    7060.00 =  3505.00 FEET.

*****
FLOW PROCESS FROM NODE    7060.00 TO NODE    7060.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    9.77
RAINFALL INTENSITY(INCH/HR) =    6.16
TOTAL STREAM AREA(ACRES) =    40.20
PEAK FLOW RATE(CFS) AT CONFLUENCE =    127.89

*****
FLOW PROCESS FROM NODE    7058.00 TO NODE    7059.00 IS CODE =   21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =   100.00
UPSTREAM ELEVATION(FEET) =   417.00
DOWNSTREAM ELEVATION(FEET) =   411.00
ELEVATION DIFFERENCE(FEET) =    6.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =   4.656
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) =    1.20
TOTAL AREA(ACRES) =    0.20 TOTAL RUNOFF(CFS) =    1.20

*****
FLOW PROCESS FROM NODE    7059.00 TO NODE    7060.00 IS CODE =   62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #  1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =   411.00 DOWNSTREAM ELEVATION(FEET) =   356.00
STREET LENGTH(FEET) =   500.00 CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =   18.00

```

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 13.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 4.45  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.23  
 HALFSTREET FLOOD WIDTH (FEET) = 6.14  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 4.80  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 1.09  
 STREET FLOW TRAVEL TIME (MIN.) = 1.74 Tc (MIN.) = 6.39  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.095  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.851  
 SUBAREA AREA (ACRES) = 0.90 SUBAREA RUNOFF (CFS) = 6.56  
 TOTAL AREA (ACRES) = 1.10 PEAK FLOW RATE (CFS) = 7.58

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.26 HALFSTREET FLOOD WIDTH (FEET) = 7.87  
 FLOW VELOCITY (FEET/SEC.) = 5.37 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.41  
 LONGEST FLOWPATH FROM NODE 7058.00 TO NODE 7060.00 = 600.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7060.00 TO NODE 7060.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 6.39  
 RAINFALL INTENSITY (INCH/HR) = 8.10  
 TOTAL STREAM AREA (ACRES) = 1.10  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 7.58

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	127.89	9.77	6.157	40.20
2	7.58	6.39	8.095	1.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	91.24	6.39	8.095
2	133.65	9.77	6.157

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 133.65 Tc(MIN.) = 9.77

TOTAL AREA(ACRES) = 41.30

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7060.00 = 3505.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7060.00 TO NODE 7064.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 346.00 DOWNSTREAM(FEET) = 326.00

FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.9 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 31.94

ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 133.65

PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 9.85

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7064.00 = 3665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7060.00 TO NODE 7064.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 9.85

RAINFALL INTENSITY(INCH/HR) = 6.12

TOTAL STREAM AREA(ACRES) = 41.30

PEAK FLOW RATE(CFS) AT CONFLUENCE = 133.65

\*\*\*\*\*

FLOW PROCESS FROM NODE 7061.00 TO NODE 7062.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 383.00

DOWNSTREAM ELEVATION(FEET) = 340.00

ELEVATION DIFFERENCE(FEET) = 43.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.094

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.16

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.16

\*\*\*\*\*

FLOW PROCESS FROM NODE 7062.00 TO NODE 7063.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 340.00 DOWNSTREAM(FEET) = 333.00
FLOW LENGTH(FEET) = 380.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.67
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 1.16
PIPE TRAVEL TIME(MIN.) = 1.36 Tc(MIN.) = 5.45
LONGEST FLOWPATH FROM NODE 7061.00 TO NODE 7063.00 = 480.00 FEET.

*****
FLOW PROCESS FROM NODE 7062.00 TO NODE 7063.00 IS CODE = 81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.971
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6100
SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 3.28
TOTAL AREA(ACRES) = 0.80 TOTAL RUNOFF(CFS) = 4.38
TC(MIN.) = 5.45

*****
FLOW PROCESS FROM NODE 7063.00 TO NODE 7064.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 328.00 DOWNSTREAM(FEET) = 326.00
FLOW LENGTH(FEET) = 115.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.69
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 4.38
PIPE TRAVEL TIME(MIN.) = 0.29 Tc(MIN.) = 5.74
LONGEST FLOWPATH FROM NODE 7061.00 TO NODE 7064.00 = 595.00 FEET.

*****
FLOW PROCESS FROM NODE 7064.00 TO NODE 7064.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.74
RAINFALL INTENSITY(INCH/HR) = 8.68
TOTAL STREAM AREA(ACRES) = 0.80
PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.38

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

```

1	133.65	9.85	6.123	41.30
2	4.38	5.74	8.680	0.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	98.67	5.74	8.680
2	136.74	9.85	6.123

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 136.74 Tc (MIN.) = 9.85

TOTAL AREA (ACRES) = 42.10

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7064.00 = 3665.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7064.00 TO NODE 7068.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 326.00 DOWNSTREAM (FEET) = 298.00

FLOW LENGTH (FEET) = 200.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.1 INCHES

PIPE-FLOW VELOCITY (FEET/SEC.) = 33.72

ESTIMATED PIPE DIAMETER (INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW (CFS) = 136.74

PIPE TRAVEL TIME (MIN.) = 0.10 Tc (MIN.) = 9.95

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7068.00 = 3865.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7068.00 TO NODE 7068.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION (MIN.) = 9.95

RAINFALL INTENSITY (INCH/HR) = 6.08

TOTAL STREAM AREA (ACRES) = 42.10

PEAK FLOW RATE (CFS) AT CONFLUENCE = 136.74

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7066.00 TO NODE 7067.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .5100

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00

UPSTREAM ELEVATION (FEET) = 370.00

DOWNSTREAM ELEVATION (FEET) = 357.00

ELEVATION DIFFERENCE (FEET) = 13.00

SUBAREA OVERLAND TIME OF FLOW (MIN.) = 4.930

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.97  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.97

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7067.00 TO NODE 7067.50 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) =	357.00	DOWNSTREAM ELEVATION(FEET) =	299.00
STREET LENGTH(FEET) =	480.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	18.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.70  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.21  
 HALFSTREET FLOOD WIDTH(FEET) = 5.48  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.78  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.03  
 STREET FLOW TRAVEL TIME(MIN.) = 1.67 Tc(MIN.) = 6.60  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.926  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6900  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.660  
 SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 5.47  
 TOTAL AREA(ACRES) = 1.20 PEAK FLOW RATE(CFS) = 6.28

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.25 HALFSTREET FLOOD WIDTH(FEET) = 7.11  
 FLOW VELOCITY(FEET/SEC.) = 5.31 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.31  
 LONGEST FLOWPATH FROM NODE 7066.00 TO NODE 7067.50 = 580.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7067.50 TO NODE 7068.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	299.00	DOWNSTREAM(FEET) =	298.00
FLOW LENGTH(FEET) =	240.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS	14.3 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	4.16		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	6.28		

PIPE TRAVEL TIME(MIN.) = 0.96 Tc(MIN.) = 7.57  
 LONGEST FLOWPATH FROM NODE 7066.00 TO NODE 7068.00 = 820.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7068.00 TO NODE 7068.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	7.57
RAINFALL INTENSITY(INCH/HR) =	7.26
TOTAL STREAM AREA(ACRES) =	1.20
PEAK FLOW RATE(CFS) AT CONFLUENCE =	6.28

+-----+  
 | Flow Information for Node 7068 |  
 +-----+

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7068.00 TO NODE 7068.00 IS CODE = 7

>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

=====

USER-SPECIFIED VALUES ARE AS FOLLOWS:	
TC(MIN) =	8.37
RAIN INTENSITY(INCH/HOUR) =	6.80
TOTAL AREA(ACRES) =	114.30
TOTAL RUNOFF(CFS) =	311.62

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7068.00 TO NODE 7068.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:	
TIME OF CONCENTRATION(MIN.) =	8.37
RAINFALL INTENSITY(INCH/HR) =	6.80
TOTAL STREAM AREA(ACRES) =	114.30
PEAK FLOW RATE(CFS) AT CONFLUENCE =	311.62

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	136.74	9.95	6.084	42.10
2	6.28	7.57	7.261	1.20
3	311.62	8.37	6.803	114.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	402.57	7.57	7.261

2	439.78	8.37	6.803
3	420.67	9.95	6.084

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 439.78 Tc(MIN.) = 8.37

TOTAL AREA(ACRES) = 157.60

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7068.00 = 3865.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7068.00 TO NODE 7079.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 298.00 DOWNSTREAM(FEET) = 294.00

FLOW LENGTH(FEET) = 105.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 60.0 INCH PIPE IS 45.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 27.84

ESTIMATED PIPE DIAMETER(INCH) = 60.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 439.78

PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 8.43

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7079.00 = 3970.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7079.00 TO NODE 7079.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5102.00 TO NODE 5103.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 393.00

DOWNSTREAM ELEVATION(FEET) = 385.00

ELEVATION DIFFERENCE(FEET) = 8.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.800

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 2.56

TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 2.56

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5103.00 TO NODE 5105.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

UPSTREAM ELEVATION(FEET) = 385.00 DOWNSTREAM ELEVATION(FEET) = 308.00

STREET LENGTH(FEET) = 1030.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(FEET) = 18.00



DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.56  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.29  
HALFSTREET FLOOD WIDTH(FEET) = 9.44  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.89  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.44  
STREET FLOW TRAVEL TIME(MIN.) = 3.51 Tc(MIN.) = 5.31  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.121  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 13.96  
TOTAL AREA(ACRES) = 2.00 PEAK FLOW RATE(CFS) = 16.42

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 11.83  
FLOW VELOCITY(FEET/SEC.) = 5.53 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.89  
LONGEST FLOWPATH FROM NODE 5102.00 TO NODE 5105.00 = 1130.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5105.00 TO NODE 7072.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 308.00 DOWNSTREAM(FEET) = 296.00  
FLOW LENGTH(FEET) = 1700.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 17.9 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.52  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 16.42  
PIPE TRAVEL TIME(MIN.) = 4.35 Tc(MIN.) = 9.66  
LONGEST FLOWPATH FROM NODE 5102.00 TO NODE 7072.00 = 2830.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7072.00 TO NODE 7072.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.66  
RAINFALL INTENSITY(INCH/HR) = 6.20  
TOTAL STREAM AREA(ACRES) = 2.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 16.42

\*\*\*\*\*

FLOW PROCESS FROM NODE 7070.00 TO NODE 7071.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(Feet) = 60.00

UPSTREAM ELEVATION(Feet) = 311.60

DOWNSTREAM ELEVATION(Feet) = 311.00

ELEVATION DIFFERENCE(Feet) = 0.60

SUBAREA OVERLAND TIME OF FLOW(Min.) = 4.183

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.52

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 7071.00 TO NODE 7072.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

UPSTREAM ELEVATION(Feet) = 311.00 DOWNSTREAM ELEVATION(Feet) = 310.00

STREET LENGTH(Feet) = 1380.00 CURB HEIGHT(INCHES) = 6.0

STREET HALFWIDTH(Feet) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(Feet) = 13.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.55

\*\*\*STREET FLOWING FULL\*\*\*

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(Feet) = 0.51

HALFSTREET FLOOD WIDTH(Feet) = 18.29

AVERAGE FLOW VELOCITY(Feet/Sec.) = 0.81

PRODUCT OF DEPTH&VELOCITY(Ft\*Ft/Sec.) = 0.41

STREET FLOW TRAVEL TIME(Min.) = 28.53 Tc(Min.) = 32.71

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 2.824

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8000

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.800

SUBAREA AREA(ACRES) = 3.80 SUBAREA RUNOFF(CFS) = 8.58

TOTAL AREA(ACRES) = 4.00 PEAK FLOW RATE(CFS) = 9.04

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(Feet) = 0.55 HALFSTREET FLOOD WIDTH(Feet) = 20.68

FLOW VELOCITY(Feet/Sec.) = 0.91 DEPTH\*VELOCITY(Ft\*Ft/Sec.) = 0.50

\*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,

AND L = 1380.0 FT WITH ELEVATION-DROP = 1.0 FT, IS 28.8 CFS,

WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 7072.00  
 LONGEST FLOWPATH FROM NODE 7070.00 TO NODE 7072.00 = 1440.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7072.00 TO NODE 7072.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	32.71
RAINFALL INTENSITY(INCH/HR) =	2.82
TOTAL STREAM AREA(ACRES) =	4.00
PEAK FLOW RATE(CFS) AT CONFLUENCE =	9.04

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	16.42	9.66	6.203	2.00
2	9.04	32.71	2.824	4.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	19.09	9.66	6.203
2	16.51	32.71	2.824

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =	19.09	Tc(MIN.) =	9.66
TOTAL AREA(ACRES) =	6.00		
LONGEST FLOWPATH FROM NODE	5102.00	TO NODE	7072.00 = 2830.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7072.00 TO NODE 7079.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	296.00	DOWNSTREAM(FEET) =	294.00
FLOW LENGTH(FEET) =	280.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS	17.7 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	6.90		
ESTIMATED PIPE DIAMETER(INCH) =	27.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	19.09		
PIPE TRAVEL TIME(MIN.) =	0.68	Tc(MIN.) =	10.34
LONGEST FLOWPATH FROM NODE	5102.00	TO NODE	7079.00 = 3110.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7079.00 TO NODE 7079.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	19.09	10.34	5.938	6.00

LONGEST FLOWPATH FROM NODE 5102.00 TO NODE 7079.00 = 3110.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	439.78	8.43	6.771	157.60

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7079.00 = 3970.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	455.36	8.43	6.771
2	404.78	10.34	5.938

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 455.36 Tc(MIN.) = 8.43  
TOTAL AREA(ACRES) = 163.60

\*\*\*\*\*

FLOW PROCESS FROM NODE 7079.00 TO NODE 7079.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 7079.00 TO NODE 7098.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 294.00 DOWNSTREAM( FEET) = 290.00

CHANNEL LENGTH THRU SUBAREA( FEET) = 700.00 CHANNEL SLOPE = 0.0057

CHANNEL BASE( FEET) = 100.00 "Z" FACTOR = 3.000

MANNING'S FACTOR = 0.016 MAXIMUM DEPTH( FEET) = 15.00

100 YEAR RAINFALL INTENSITY( INCH/HOUR) = 5.903

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .4500

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 463.46

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 5.84

AVERAGE FLOW DEPTH( FEET) = 0.78 TRAVEL TIME( MIN.) = 2.00

Tc( MIN.) = 10.43

SUBAREA AREA( ACRES) = 6.10 SUBAREA RUNOFF( CFS) = 16.20

AREA-AVERAGE RUNOFF COEFFICIENT = 0.444

TOTAL AREA( ACRES) = 169.70 PEAK FLOW RATE( CFS) = 455.36

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH( FEET) = 0.77 FLOW VELOCITY( FEET/SEC.) = 5.80

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7098.00 = 4670.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 7098.00 TO NODE 7098.00 IS CODE = 10

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====
*****
FLOW PROCESS FROM NODE 7074.10 TO NODE 7074.20 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 855.00
DOWNSTREAM ELEVATION(FEET) = 800.00
ELEVATION DIFFERENCE(FEET) = 55.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.200
SUBAREA RUNOFF(CFS) = 0.86
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.86
*****
FLOW PROCESS FROM NODE 7074.20 TO NODE 7074.40 IS CODE = 51
-----
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 800.00 DOWNSTREAM(FEET) = 415.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1240.00 CHANNEL SLOPE = 0.3105
CHANNEL BASE(FEET) = 3.00 "Z" FACTOR = 3.000
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 5.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.847
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3200
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 15.61
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 10.23
AVERAGE FLOW DEPTH(FEET) = 0.37 TRAVEL TIME(MIN.) = 2.02
Tc(MIN.) = 8.29
SUBAREA AREA(ACRES) = 13.30 SUBAREA RUNOFF(CFS) = 29.14
AREA-AVERAGE RUNOFF COEFFICIENT = 0.321
TOTAL AREA(ACRES) = 13.60 PEAK FLOW RATE(CFS) = 29.86

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.52 FLOW VELOCITY(FEET/SEC.) = 12.48
LONGEST FLOWPATH FROM NODE 7074.10 TO NODE 7074.40 = 1340.00 FEET.
*****
FLOW PROCESS FROM NODE 7074.00 TO NODE 7076.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 415.00 DOWNSTREAM(FEET) = 338.00
FLOW LENGTH(FEET) = 540.00 MANNING'S N = 0.016
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.72

```

ESTIMATED PIPE DIAMETER(INCH) = 18.00      NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 29.86  
 PIPE TRAVEL TIME(MIN.) = 0.46      Tc(MIN.) = 8.74  
 LONGEST FLOWPATH FROM NODE 7074.10 TO NODE 7076.00 = 1880.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7076.00 TO NODE 7076.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.74  
 RAINFALL INTENSITY(INCH/HR) = 6.61  
 TOTAL STREAM AREA(ACRES) = 13.60  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 29.86

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7075.10 TO NODE 7075.20 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00  
 UPSTREAM ELEVATION(FEET) = 850.00  
 DOWNSTREAM ELEVATION(FEET) = 780.00  
 ELEVATION DIFFERENCE(FEET) = 70.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.945  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.483  
 SUBAREA RUNOFF(CFS) = 0.59  
 TOTAL AREA(ACRES) = 0.20      TOTAL RUNOFF(CFS) = 0.59

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7075.20 TO NODE 7076.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 780.00      DOWNSTREAM(FEET) = 338.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 1150.00      CHANNEL SLOPE = 0.3843  
 CHANNEL BASE(FEET) = 10.00      "Z" FACTOR = 4.000  
 MANNING'S FACTOR = 0.035      MAXIMUM DEPTH(FEET) = 4.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.750

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.83  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.58  
 AVERAGE FLOW DEPTH(FEET) = 0.17      TRAVEL TIME(MIN.) = 2.53  
 Tc(MIN.) = 8.47  
 SUBAREA AREA(ACRES) = 11.00      SUBAREA RUNOFF(CFS) = 25.99  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.350  
 TOTAL AREA(ACRES) = 11.20      PEAK FLOW RATE(CFS) = 26.46

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.25 FLOW VELOCITY(FEET/SEC.) = 9.75  
 LONGEST FLOWPATH FROM NODE 7075.10 TO NODE 7076.00 = 1240.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7076.00 TO NODE 7076.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.47  
 RAINFALL INTENSITY(INCH/HR) = 6.75  
 TOTAL STREAM AREA(ACRES) = 11.20  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 26.46

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	29.86	8.74	6.614	13.60
2	26.46	8.47	6.750	11.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	55.39	8.47	6.750
2	55.79	8.74	6.614

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 55.79 Tc(MIN.) = 8.74  
 TOTAL AREA(ACRES) = 24.80  
 LONGEST FLOWPATH FROM NODE 7074.10 TO NODE 7076.00 = 1880.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7076.00 TO NODE 7098.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 338.00 DOWNSTREAM(FEET) = 300.00  
 FLOW LENGTH(FEET) = 280.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 14.9 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 27.33  
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 55.79  
 PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 8.91  
 LONGEST FLOWPATH FROM NODE 7074.10 TO NODE 7098.00 = 2160.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7098.00 TO NODE 7098.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	55.79	8.91	6.532	24.80

LONGEST FLOWPATH FROM NODE 7074.10 TO NODE 7098.00 = 2160.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	455.36	10.43	5.903	169.70

LONGEST FLOWPATH FROM NODE 7000.00 TO NODE 7098.00 = 4670.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	444.97	8.91	6.532
2	505.77	10.43	5.903

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 505.77 Tc(MIN.) = 10.43

TOTAL AREA(ACRES) = 194.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 7098.00 TO NODE 7098.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 194.50 TC(MIN.) = 10.43

PEAK FLOW RATE(CFS) = 505.77

END OF RATIONAL METHOD ANALYSIS



**Flow Information For Drainage**

**Basin 7000A**

**(Node 6026)**

**(Node 5086)**

**(Node 5090.5)**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

RICK ENGINEERING COMPANY  
5620 Friars Road  
San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 07/16/09 \*  
\* 100-yr Post-project (on-site) \*  
\* \*  
\*\*\*\*\*

FILE NAME: MW\_5K100.DAT  
TIME/DATE OF STUDY: 10:17 07/20/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS  
\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*  
HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING  
WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR  
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)  
=== =====  
1 36.0 31.0 0.020/0.020/0.020 0.50 1.50 0.0100 0.125 0.0180

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5000.00 TO NODE 5000.10 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00  
 UPSTREAM ELEVATION(FEET) = 762.10  
 DOWNSTREAM ELEVATION(FEET) = 762.00  
 ELEVATION DIFFERENCE(FEET) = 0.10  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.207  
 WARNING: THE MINIMUM OVERLAND FLOW SLOPE, 0.5%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 4.27  
 TOTAL AREA(ACRES) = 0.50 TOTAL RUNOFF(CFS) = 4.27

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5000.10 TO NODE 5000.20 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 762.00 DOWNSTREAM(FEET) = 700.00  
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 18.58  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 4.27  
 PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 3.39  
 LONGEST FLOWPATH FROM NODE 5000.00 TO NODE 5000.20 = 250.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5000.10 TO NODE 5000.20 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.6333  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.14  
 TOTAL AREA(ACRES) = 0.90 TOTAL RUNOFF(CFS) = 5.41  
 TC(MIN.) = 3.39

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5000.20 TO NODE 5000.30 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 700.00 DOWNSTREAM(FEET) = 600.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 220.00 CHANNEL SLOPE = 0.4545  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.82  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(Feet/Sec.) = 6.61  
 AVERAGE FLOW DEPTH(Feet) = 0.12 TRAVEL TIME(Min.) = 0.55  
 Tc(Min.) = 3.94  
 SUBAREA AREA(ACRES) = 2.40 SUBAREA RUNOFF(CFS) = 6.83  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.391  
 TOTAL AREA(ACRES) = 3.30 PEAK FLOW RATE(CFS) = 12.24

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(Feet) = 0.15 FLOW VELOCITY(Feet/Sec.) = 7.21  
 LONGEST FLOWPATH FROM NODE 5000.00 TO NODE 5000.30 = 470.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5000.30 TO NODE 5003.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 600.00 DOWNSTREAM(Feet) = 522.00  
 CHANNEL LENGTH THRU SUBAREA(Feet) = 270.00 CHANNEL SLOPE = 0.2889  
 CHANNEL BASE(Feet) = 10.00 "Z" FACTOR = 7.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(Feet) = 3.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 16.50  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(Feet/Sec.) = 7.19  
 AVERAGE FLOW DEPTH(Feet) = 0.20 TRAVEL TIME(Min.) = 0.63  
 Tc(Min.) = 4.57  
 SUBAREA AREA(ACRES) = 3.00 SUBAREA RUNOFF(CFS) = 8.54  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.348  
 TOTAL AREA(ACRES) = 6.30 PEAK FLOW RATE(CFS) = 20.77

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(Feet) = 0.23 FLOW VELOCITY(Feet/Sec.) = 7.71  
 LONGEST FLOWPATH FROM NODE 5000.00 TO NODE 5003.00 = 740.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5003.00 TO NODE 5003.00 IS CODE = 10  
 -----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5001.00 TO NODE 5001.10 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(Feet) = 50.00  
 UPSTREAM ELEVATION(Feet) = 764.10  
 DOWNSTREAM ELEVATION(Feet) = 764.00  
 ELEVATION DIFFERENCE(Feet) = 0.10

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.207  
 WARNING: THE MINIMUM OVERLAND FLOW SLOPE, 0.5%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 8.54  
 TOTAL AREA(ACRES) = 1.00 TOTAL RUNOFF(CFS) = 8.54

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5001.10 TO NODE 5001.20 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 764.00 DOWNSTREAM(FEET) = 695.00  
 FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 24.54  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 8.54  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 3.33  
 LONGEST FLOWPATH FROM NODE 5001.00 TO NODE 5001.20 = 230.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5001.10 TO NODE 5001.20 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.7286  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.14  
 TOTAL AREA(ACRES) = 1.40 TOTAL RUNOFF(CFS) = 9.67  
 TC(MIN.) = 3.33

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5001.20 TO NODE 5002.30 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 695.00 DOWNSTREAM(FEET) = 580.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 260.00 CHANNEL SLOPE = 0.4423  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.67  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.99  
 AVERAGE FLOW DEPTH(FEET) = 0.13 TRAVEL TIME(MIN.) = 0.62  
 Tc(MIN.) = 3.95

SUBAREA AREA(ACRES) = 0.70 SUBAREA RUNOFF(CFS) = 1.99  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.586  
TOTAL AREA(ACRES) = 2.10 PEAK FLOW RATE(CFS) = 11.67

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.14 FLOW VELOCITY(FEET/SEC.) = 7.19  
LONGEST FLOWPATH FROM NODE 5001.00 TO NODE 5002.30 = 490.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5002.30 TO NODE 5002.30 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS	=	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:		
TIME OF CONCENTRATION(MIN.)	=	3.95
RAINFALL INTENSITY(INCH/HR)	=	9.49
TOTAL STREAM AREA(ACRES)	=	2.10
PEAK FLOW RATE(CFS) AT CONFLUENCE	=	11.67

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5002.00 TO NODE 5002.10 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT	=	.9000
S.C.S. CURVE NUMBER (AMC II)	=	0
INITIAL SUBAREA FLOW-LENGTH(FEET)	=	50.00
UPSTREAM ELEVATION(FEET)	=	764.10
DOWNSTREAM ELEVATION(FEET)	=	761.00
ELEVATION DIFFERENCE(FEET)	=	3.10
SUBAREA OVERLAND TIME OF FLOW(MIN.)	=	1.386
100 YEAR RAINFALL INTENSITY(INCH/HOUR)	=	9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.		
SUBAREA RUNOFF(CFS)	=	8.54
TOTAL AREA(ACRES)	=	1.00
TOTAL RUNOFF(CFS)	=	8.54

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5002.10 TO NODE 5002.20 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET)	=	764.00	DOWNSTREAM(FEET)	=	695.00
FLOW LENGTH(FEET)	=	190.00	MANNING'S N	=	0.013
ESTIMATED PIPE DIAMETER(INCH)	INCREASED TO 18.000				
DEPTH OF FLOW IN 18.0 INCH PIPE IS	4.6 INCHES				
PIPE-FLOW VELOCITY(FEET/SEC.)	= 24.06				
ESTIMATED PIPE DIAMETER(INCH)	=	18.00	NUMBER OF PIPES	=	1
PIPE-FLOW(CFS)	=	8.54			
PIPE TRAVEL TIME(MIN.)	=	0.13	Tc(MIN.)	=	1.52
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5002.20	= 240.00 FEET.				

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5002.10 TO NODE 5002.20 IS CODE = 81  
-----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED (SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6750  
SUBAREA AREA (ACRES) = 0.60 SUBAREA RUNOFF (CFS) = 1.71  
TOTAL AREA (ACRES) = 1.60 TOTAL RUNOFF (CFS) = 10.24  
TC (MIN.) = 1.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 5002.20 TO NODE 5002.30 IS CODE = 51

-----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 695.00 DOWNSTREAM (FEET) = 580.00  
CHANNEL LENGTH THRU SUBAREA (FEET) = 280.00 CHANNEL SLOPE = 0.4107  
CHANNEL BASE (FEET) = 5.00 "Z" FACTOR = 5.000  
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH (FEET) = 10.00  
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
\*USER SPECIFIED (SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 12.09  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 8.82  
AVERAGE FLOW DEPTH (FEET) = 0.22 TRAVEL TIME (MIN.) = 0.53  
Tc (MIN.) = 2.05  
SUBAREA AREA (ACRES) = 1.30 SUBAREA RUNOFF (CFS) = 3.70  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.507  
TOTAL AREA (ACRES) = 2.90 PEAK FLOW RATE (CFS) = 13.94

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH (FEET) = 0.24 FLOW VELOCITY (FEET/SEC.) = 9.31  
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5002.30 = 520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5002.30 TO NODE 5002.30 IS CODE = 1

-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION (MIN.) = 2.05  
RAINFALL INTENSITY (INCH/HR) = 9.49  
TOTAL STREAM AREA (ACRES) = 2.90  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 13.94

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	11.67	3.95	9.485	2.10
2	13.94	2.05	9.485	2.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	19.99	2.05	9.485
2	25.61	3.95	9.485

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 25.61 Tc(MIN.) = 3.95  
TOTAL AREA(ACRES) = 5.00  
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5002.30 = 520.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5002.30 TO NODE 5003.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 580.00 DOWNSTREAM(FEET) = 522.00

CHANNEL LENGTH THRU SUBAREA(FEET) = 240.00 CHANNEL SLOPE = 0.2417

CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 5.000

MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 28.74

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.50

AVERAGE FLOW DEPTH(FEET) = 0.29 TRAVEL TIME(MIN.) = 0.47

Tc(MIN.) = 4.42

SUBAREA AREA(ACRES) = 2.20 SUBAREA RUNOFF(CFS) = 6.26

AREA-AVERAGE RUNOFF COEFFICIENT = 0.467

TOTAL AREA(ACRES) = 7.20 PEAK FLOW RATE(CFS) = 31.87

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.32 FLOW VELOCITY(FEET/SEC.) = 8.72

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5003.00 = 760.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5003.00 TO NODE 5003.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	31.87	4.42	9.485	7.20

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5003.00 = 760.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
------------------	-----------------	--------------	--------------------------	----------------



1            20.77            4.57            9.485            6.30  
 LONGEST FLOWPATH FROM NODE 5000.00 TO NODE 5003.00 = 740.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	51.97	4.42	9.485
2	52.64	4.57	9.485

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 52.64 Tc(MIN.) = 4.57  
 TOTAL AREA(ACRES) = 13.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 5003.00 TO NODE 5003.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 5003.00 TO NODE 5006.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 512.00 DOWNSTREAM(FEET) = 487.00

FLOW LENGTH(FEET) = 380.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.8 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 19.95

ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 52.64

PIPE TRAVEL TIME(MIN.) = 0.32 Tc(MIN.) = 4.88

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5006.00 = 1140.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5006.00 TO NODE 5006.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 4.88

RAINFALL INTENSITY(INCH/HR) = 9.49

TOTAL STREAM AREA(ACRES) = 13.50

PEAK FLOW RATE(CFS) AT CONFLUENCE = 52.64

\*\*\*\*\*

FLOW PROCESS FROM NODE 5004.00 TO NODE 5005.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 526.00

DOWNSTREAM ELEVATION(FEET) = 520.00

ELEVATION DIFFERENCE (FEET) = 6.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 1.981  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON  $T_c$  = 5-MINUTE.  
 SUBAREA RUNOFF (CFS) = 1.71  
 TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 1.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5005.00 TO NODE 5006.00 IS CODE = 62  
 -----

>>>> COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA <<<<<  
 >>>> (STREET TABLE SECTION # 1 USED) <<<<<

=====

UPSTREAM ELEVATION (FEET) =	520.00	DOWNSTREAM ELEVATION (FEET) =	497.00
STREET LENGTH (FEET) =	245.00	CURB HEIGHT (INCHES) =	6.0
STREET HALFWIDTH (FEET) =	36.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 31.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 7.09  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.26  
 HALFSTREET FLOOD WIDTH (FEET) = 7.94  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 4.95  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 1.30  
 STREET FLOW TRAVEL TIME (MIN.) = 0.83  $T_c$  (MIN.) = 2.81  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON  $T_c$  = 5-MINUTE.  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.657  
 SUBAREA AREA (ACRES) = 1.80 SUBAREA RUNOFF (CFS) = 10.76  
 TOTAL AREA (ACRES) = 2.00 PEAK FLOW RATE (CFS) = 12.46

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.31 HALFSTREET FLOOD WIDTH (FEET) = 10.06  
 FLOW VELOCITY (FEET/SEC.) = 5.68 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.74  
 LONGEST FLOWPATH FROM NODE 5004.00 TO NODE 5006.00 = 345.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5006.00 TO NODE 5006.00 IS CODE = 1  
 -----

>>>> DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE <<<<<  
 >>>> AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES <<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 2.81  
 RAINFALL INTENSITY (INCH/HR) = 9.49

TOTAL STREAM AREA (ACRES) = 2.00  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 12.46

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	52.64	4.88	9.485	13.50
2	12.46	2.81	9.485	2.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	42.71	2.81	9.485
2	65.11	4.88	9.485

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 65.11 Tc (MIN.) = 4.88  
TOTAL AREA (ACRES) = 15.50  
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5006.00 = 1140.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5006.00 TO NODE 5019.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 487.00 DOWNSTREAM (FEET) = 480.00  
FLOW LENGTH (FEET) = 110.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.6 INCHES  
PIPE-FLOW VELOCITY (FEET/SEC.) = 21.03  
ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1  
PIPE-FLOW (CFS) = 65.11  
PIPE TRAVEL TIME (MIN.) = 0.09 Tc (MIN.) = 4.97  
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5019.00 = 1250.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5019.00 TO NODE 5019.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5008.00 TO NODE 5009.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED (SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH (FEET) = 100.00  
UPSTREAM ELEVATION (FEET) = 548.00  
DOWNSTREAM ELEVATION (FEET) = 510.00  
ELEVATION DIFFERENCE (FEET) = 38.00  
SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.684

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5009.00 TO NODE 5010.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	510.00	DOWNSTREAM ELEVATION(FEET) =	505.00
STREET LENGTH(FEET) =	230.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	36.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 31.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.50  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.21  
 HALFSTREET FLOOD WIDTH(FEET) = 5.39  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.99  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.42  
 STREET FLOW TRAVEL TIME(MIN.) = 1.92 Tc(MIN.) = 8.61  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.681  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.620  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 2.08  
 TOTAL AREA(ACRES) = 0.60 PEAK FLOW RATE(CFS) = 2.49

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.24 HALFSTREET FLOOD WIDTH(FEET) = 6.85  
 FLOW VELOCITY(FEET/SEC.) = 2.24 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.54  
 LONGEST FLOWPATH FROM NODE 5008.00 TO NODE 5010.00 = 330.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5010.00 TO NODE 5015.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	495.00	DOWNSTREAM(FEET) =	487.00
FLOW LENGTH(FEET) =	165.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO	18.000		
DEPTH OF FLOW IN 18.0 INCH PIPE IS	4.1 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	8.23		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	2.49		

PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 8.94  
LONGEST FLOWPATH FROM NODE 5008.00 TO NODE 5015.00 = 495.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5015.00 TO NODE 5015.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	8.94
RAINFALL INTENSITY(INCH/HR) =	6.52
TOTAL STREAM AREA(ACRES) =	0.60
PEAK FLOW RATE(CFS) AT CONFLUENCE =	2.49

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5012.00 TO NODE 5013.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.3000
S.C.S. CURVE NUMBER (AMC II) =	0
INITIAL SUBAREA FLOW-LENGTH(FEET) =	100.00
UPSTREAM ELEVATION(FEET) =	760.00
DOWNSTREAM ELEVATION(FEET) =	710.00
ELEVATION DIFFERENCE(FEET) =	50.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =	6.684
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!	
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	7.865
SUBAREA RUNOFF(CFS) =	0.47
TOTAL AREA(ACRES) =	0.20
TOTAL RUNOFF(CFS) =	0.47

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5013.00 TO NODE 5014.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	710.00	DOWNSTREAM(FEET) =	492.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	740.00	CHANNEL SLOPE =	0.2946
CHANNEL BASE(FEET) =	20.00	"Z" FACTOR =	2.500
MANNING'S FACTOR =	0.035	MAXIMUM DEPTH(FEET) =	5.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	6.162		
*USER SPECIFIED(SUBAREA):			
USER-SPECIFIED RUNOFF COEFFICIENT =	.3000		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	5.95		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	4.01		
AVERAGE FLOW DEPTH(FEET) =	0.07	TRAVEL TIME(MIN.) =	3.07
Tc(MIN.) =	9.76		
SUBAREA AREA(ACRES) =	5.80	SUBAREA RUNOFF(CFS) =	10.72
AREA-AVERAGE RUNOFF COEFFICIENT =	0.300		
TOTAL AREA(ACRES) =	6.00	PEAK FLOW RATE(CFS) =	11.09

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
DEPTH(FEET) = 0.10 FLOW VELOCITY(FEET/SEC.) = 5.27

LONGEST FLOWPATH FROM NODE 5012.00 TO NODE 5014.00 = 840.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5014.00 TO NODE 5015.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	489.00	DOWNSTREAM(FEET) =	487.00
FLOW LENGTH(FEET) =	160.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS	14.7 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	7.19		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	11.09		
PIPE TRAVEL TIME(MIN.) =	0.37	Tc(MIN.) =	10.13
LONGEST FLOWPATH FROM NODE 5012.00 TO NODE 5015.00 =	1000.00 FEET.		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5015.00 TO NODE 5015.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	10.13
RAINFALL INTENSITY(INCH/HR) =	6.02
TOTAL STREAM AREA(ACRES) =	6.00
PEAK FLOW RATE(CFS) AT CONFLUENCE =	11.09

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.49	8.94	6.519	0.60
2	11.09	10.13	6.016	6.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	12.28	8.94	6.519
2	13.39	10.13	6.016

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =	13.39	Tc(MIN.) =	10.13
TOTAL AREA(ACRES) =	6.60		
LONGEST FLOWPATH FROM NODE 5012.00 TO NODE 5015.00 =	1000.00 FEET.		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5015.00 TO NODE 5018.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	487.00	DOWNSTREAM(FEET) =	483.00
----------------------------------	--------	--------------------	--------

FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.09  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 13.39  
 PIPE TRAVEL TIME(MIN.) = 0.14 Tc(MIN.) = 10.27  
 LONGEST FLOWPATH FROM NODE 5012.00 TO NODE 5018.00 = 1100.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5018.00 TO NODE 5018.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.27  
 RAINFALL INTENSITY(INCH/HR) = 5.96  
 TOTAL STREAM AREA(ACRES) = 6.60  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.39

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5017.00 TO NODE 5018.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00  
 UPSTREAM ELEVATION(FEET) = 497.00  
 DOWNSTREAM ELEVATION(FEET) = 493.00  
 ELEVATION DIFFERENCE(FEET) = 4.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 1.883  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 5.12  
 TOTAL AREA(ACRES) = 0.60 TOTAL RUNOFF(CFS) = 5.12

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5018.00 TO NODE 5018.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 1.88  
 RAINFALL INTENSITY(INCH/HR) = 9.49  
 TOTAL STREAM AREA(ACRES) = 0.60  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.12

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	13.39	10.27	5.963	6.60
2	5.12	1.88	9.485	0.60

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	13.54	1.88	9.485
2	16.61	10.27	5.963

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 16.61 Tc (MIN.) = 10.27

TOTAL AREA (ACRES) = 7.20

LONGEST FLOWPATH FROM NODE 5012.00 TO NODE 5018.00 = 1100.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5018.00 TO NODE 5019.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 483.00 DOWNSTREAM (FEET) = 480.00

FLOW LENGTH (FEET) = 90.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.5 INCHES

PIPE-FLOW VELOCITY (FEET/SEC.) = 11.67

ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW (CFS) = 16.61

PIPE TRAVEL TIME (MIN.) = 0.13 Tc (MIN.) = 10.40

LONGEST FLOWPATH FROM NODE 5012.00 TO NODE 5019.00 = 1190.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5019.00 TO NODE 5019.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	16.61	10.40	5.916	7.20

LONGEST FLOWPATH FROM NODE 5012.00 TO NODE 5019.00 = 1190.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	65.11	4.97	9.485	15.50

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5019.00 = 1250.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	73.05	4.97	9.485
2	57.21	10.40	5.916

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 73.05 Tc (MIN.) = 4.97

TOTAL AREA (ACRES) = 22.70



```

*****
FLOW PROCESS FROM NODE    5019.00 TO NODE    5019.00 IS CODE = 12
-----
>>>>>CLEAR MEMORY BANK # 1 <<<<<
=====

*****
FLOW PROCESS FROM NODE    5019.00 TO NODE    5024.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 480.00 DOWNSTREAM(FEET) = 475.00
FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.86
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 73.05
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 5.06
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5024.00 = 1350.00 FEET.

*****
FLOW PROCESS FROM NODE    5024.00 TO NODE    5024.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 5.06
RAINFALL INTENSITY(INCH/HR) = 9.42
TOTAL STREAM AREA(ACRES) = 22.70
PEAK FLOW RATE(CFS) AT CONFLUENCE = 73.05

*****
FLOW PROCESS FROM NODE    5021.00 TO NODE    5022.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00
UPSTREAM ELEVATION(FEET) = 760.00
DOWNSTREAM ELEVATION(FEET) = 710.00
ELEVATION DIFFERENCE(FEET) = 50.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865
SUBAREA RUNOFF(CFS) = 0.47
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

*****
FLOW PROCESS FROM NODE    5022.00 TO NODE    5023.00 IS CODE = 51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====

```

ELEVATION DATA: UPSTREAM(FEET) = 710.00 DOWNSTREAM(FEET) = 482.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 850.00 CHANNEL SLOPE = 0.2682  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 2.500  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 6.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.647  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 14.58  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.11  
 AVERAGE FLOW DEPTH(FEET) = 0.20 TRAVEL TIME(MIN.) = 1.99  
 Tc(MIN.) = 8.68  
 SUBAREA AREA(ACRES) = 14.00 SUBAREA RUNOFF(CFS) = 27.92  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 14.20 PEAK FLOW RATE(CFS) = 28.32

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.29 FLOW VELOCITY(FEET/SEC.) = 9.20  
 LONGEST FLOWPATH FROM NODE 5021.00 TO NODE 5023.00 = 950.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5023.00 TO NODE 5024.00 IS CODE = 31  
 -----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 477.00 DOWNSTREAM(FEET) = 475.00  
 FLOW LENGTH(FEET) = 195.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 21.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.52  
 ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 28.32  
 PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 9.06  
 LONGEST FLOWPATH FROM NODE 5021.00 TO NODE 5024.00 = 1145.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5024.00 TO NODE 5024.00 IS CODE = 1  
 -----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
 =====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.06  
 RAINFALL INTENSITY(INCH/HR) = 6.47  
 TOTAL STREAM AREA(ACRES) = 14.20  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 28.32

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	73.05	5.06	9.418	22.70
2	28.32	9.06	6.465	14.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	88.85	5.06	9.418
2	78.46	9.06	6.465

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 88.85 Tc(MIN.) = 5.06

TOTAL AREA(ACRES) = 36.90

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5024.00 = 1350.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5024.00 TO NODE 5028.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM( FEET) = 475.00 DOWNSTREAM( FEET) = 468.00

FLOW LENGTH( FEET) = 120.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.2 INCHES

PIPE-FLOW VELOCITY( FEET/SEC.) = 21.78

ESTIMATED PIPE DIAMETER( INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 88.85

PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.15

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5028.00 = 1470.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5028.00 TO NODE 5028.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 5.15

RAINFALL INTENSITY( INCH/HR) = 9.31

TOTAL STREAM AREA(ACRES) = 36.90

PEAK FLOW RATE(CFS) AT CONFLUENCE = 88.85

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5026.00 TO NODE 5027.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6300

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH( FEET) = 65.00

UPSTREAM ELEVATION( FEET) = 495.00

DOWNSTREAM ELEVATION( FEET) = 494.00

ELEVATION DIFFERENCE( FEET) = 1.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908

100 YEAR RAINFALL INTENSITY( INCH/HOUR) = 8.517

SUBAREA RUNOFF(CFS) = 1.07

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.07

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5027.00 TO NODE 5028.00 IS CODE = 62

```

-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 494.00  DOWNSTREAM ELEVATION(FEET) = 478.00
STREET LENGTH(FEET) = 260.00  CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 31.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.41
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.26
HALFSTREET FLOOD WIDTH(FEET) = 7.69
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.99
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.03
STREET FLOW TRAVEL TIME(MIN.) = 1.09  Tc(MIN.) = 6.99
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.638
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630
SUBAREA AREA(ACRES) = 1.80  SUBAREA RUNOFF(CFS) = 8.66
TOTAL AREA(ACRES) = 2.00  PEAK FLOW RATE(CFS) = 9.62

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.30  HALFSTREET FLOOD WIDTH(FEET) = 9.87
FLOW VELOCITY(FEET/SEC.) = 4.53  DEPTH*VELOCITY(FT*FT/SEC.) = 1.37
LONGEST FLOWPATH FROM NODE 5026.00 TO NODE 5028.00 = 325.00 FEET.

*****
FLOW PROCESS FROM NODE 5028.00 TO NODE 5028.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.99
RAINFALL INTENSITY(INCH/HR) = 7.64
TOTAL STREAM AREA(ACRES) = 2.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.62

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HOUR)    (ACRE)
    1         88.85      5.15      9.309         36.90
    2          9.62      6.99      7.638          2.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

```

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	95.93	5.15	9.309
2	82.53	6.99	7.638

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 95.93 Tc(MIN.) = 5.15

TOTAL AREA(ACRES) = 38.90

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5028.00 = 1470.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5028.00 TO NODE 5037.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 468.00 DOWNSTREAM(FEET) = 464.00

FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 33.0 INCH PIPE IS 22.3 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 22.43

ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 95.93

PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 5.20

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5037.00 = 1540.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5037.00 TO NODE 5037.00 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*

FLOW PROCESS FROM NODE 5030.00 TO NODE 5031.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00

UPSTREAM ELEVATION(FEET) = 680.00

DOWNSTREAM ELEVATION(FEET) = 650.00

ELEVATION DIFFERENCE(FEET) = 30.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.341

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.137

SUBAREA RUNOFF(CFS) = 0.49

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.49

\*\*\*\*\*

FLOW PROCESS FROM NODE 5031.00 TO NODE 5032.00 IS CODE = 51

-----  
>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

```

=====
ELEVATION DATA: UPSTREAM( FEET) = 650.00 DOWNSTREAM( FEET) = 475.00
CHANNEL LENGTH THRU SUBAREA( FEET) = 490.00 CHANNEL SLOPE = 0.3571
CHANNEL BASE( FEET) = 5.00 "Z" FACTOR = 6.000
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH( FEET) = 4.00
100 YEAR RAINFALL INTENSITY( INCH/HOUR) = 7.176
*USER SPECIFIED( SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS) = 4.60
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 5.99
AVERAGE FLOW DEPTH( FEET) = 0.13 TRAVEL TIME( MIN.) = 1.36
Tc( MIN.) = 7.71
SUBAREA AREA( ACRES) = 3.80 SUBAREA RUNOFF( CFS) = 8.18
AREA-AVERAGE RUNOFF COEFFICIENT = 0.300
TOTAL AREA( ACRES) = 4.00 PEAK FLOW RATE( CFS) = 8.61

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH( FEET) = 0.19 FLOW VELOCITY( FEET/SEC.) = 7.48
LONGEST FLOWPATH FROM NODE 5030.00 TO NODE 5032.00 = 580.00 FEET.

*****
FLOW PROCESS FROM NODE 5032.00 TO NODE 5036.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 470.00 DOWNSTREAM( FEET) = 465.00
FLOW LENGTH( FEET) = 700.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.7 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 5.68
ESTIMATED PIPE DIAMETER( INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 8.61
PIPE TRAVEL TIME( MIN.) = 2.06 Tc( MIN.) = 9.76
LONGEST FLOWPATH FROM NODE 5030.00 TO NODE 5036.00 = 1280.00 FEET.

*****
FLOW PROCESS FROM NODE 5036.00 TO NODE 5036.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION( MIN.) = 9.76
RAINFALL INTENSITY( INCH/HR) = 6.16
TOTAL STREAM AREA( ACRES) = 4.00
PEAK FLOW RATE( CFS) AT CONFLUENCE = 8.61

*****
FLOW PROCESS FROM NODE 5034.00 TO NODE 5035.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED( SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH( FEET) = 65.00

```

UPSTREAM ELEVATION (FEET) = 485.00  
 DOWNSTREAM ELEVATION (FEET) = 484.00  
 ELEVATION DIFFERENCE (FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 5.908  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.517  
 SUBAREA RUNOFF (CFS) = 1.61  
 TOTAL AREA (ACRES) = 0.30 TOTAL RUNOFF (CFS) = 1.61

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5035.00 TO NODE 5036.00 IS CODE = 62  
 -----

>>>> COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA <<<<<  
 >>>> (STREET TABLE SECTION # 1 USED) <<<<<

=====  
 UPSTREAM ELEVATION (FEET) = 484.00 DOWNSTREAM ELEVATION (FEET) = 473.00  
 STREET LENGTH (FEET) = 700.00 CURB HEIGHT (INCHES) = 6.0  
 STREET HALFWIDTH (FEET) = 36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 31.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 11.50  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.38  
 HALFSTREET FLOOD WIDTH (FEET) = 13.99  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 2.81  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 1.08  
 STREET FLOW TRAVEL TIME (MIN.) = 4.15 Tc (MIN.) = 10.05  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.045  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
 SUBAREA AREA (ACRES) = 5.10 SUBAREA RUNOFF (CFS) = 19.42  
 TOTAL AREA (ACRES) = 5.40 PEAK FLOW RATE (CFS) = 20.56

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.46 HALFSTREET FLOOD WIDTH (FEET) = 17.56  
 FLOW VELOCITY (FEET/SEC.) = 3.24 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.48  
 LONGEST FLOWPATH FROM NODE 5034.00 TO NODE 5036.00 = 765.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5036.00 TO NODE 5036.00 IS CODE = 1  
 -----

>>>> DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE <<<<<  
 >>>> AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES <<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 10.05  
 RAINFALL INTENSITY (INCH/HR) = 6.04

TOTAL STREAM AREA(ACRES) = 5.40  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.56

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	8.61	9.76	6.161	4.00
2	20.56	10.05	6.045	5.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	28.58	9.76	6.161
2	29.01	10.05	6.045

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 29.01 Tc(MIN.) = 10.05  
TOTAL AREA(ACRES) = 9.40  
LONGEST FLOWPATH FROM NODE 5030.00 TO NODE 5036.00 = 1280.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5036.00 TO NODE 5037.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	465.00	DOWNSTREAM(FEET) =	464.00
FLOW LENGTH(FEET) =	80.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS	19.7 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	9.33		
ESTIMATED PIPE DIAMETER(INCH) =	27.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	29.01		
PIPE TRAVEL TIME(MIN.) =	0.14	Tc(MIN.) =	10.20
LONGEST FLOWPATH FROM NODE 5030.00 TO NODE 5037.00 =	1360.00 FEET.		

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5037.00 TO NODE 5037.00 IS CODE = 11  
-----

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	29.01	10.20	5.990	9.40

LONGEST FLOWPATH FROM NODE 5030.00 TO NODE 5037.00 = 1360.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	95.93	5.20	9.249	38.90

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5037.00 = 1540.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*



STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	110.73	5.20	9.249
2	91.14	10.20	5.990

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 110.73 Tc (MIN.) = 5.20  
TOTAL AREA (ACRES) = 48.30

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5037.00 TO NODE 5037.00 IS CODE = 12  
-----

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5037.00 TO NODE 5041.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 464.00 DOWNSTREAM (FEET) = 444.00  
FLOW LENGTH (FEET) = 350.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.0 INCHES  
PIPE-FLOW VELOCITY (FEET/SEC.) = 22.92  
ESTIMATED PIPE DIAMETER (INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW (CFS) = 110.73  
PIPE TRAVEL TIME (MIN.) = 0.25 Tc (MIN.) = 5.45  
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5041.00 = 1890.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5041.00 TO NODE 5041.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION (MIN.) = 5.45  
RAINFALL INTENSITY (INCH/HR) = 8.97  
TOTAL STREAM AREA (ACRES) = 48.30  
PEAK FLOW RATE (CFS) AT CONFLUENCE = 110.73

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5039.00 TO NODE 5040.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED (SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6200  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH (FEET) = 65.00  
UPSTREAM ELEVATION (FEET) = 476.00  
DOWNSTREAM ELEVATION (FEET) = 475.00  
ELEVATION DIFFERENCE (FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW (MIN.) = 6.034  
100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.402  
SUBAREA RUNOFF (CFS) = 1.04

```

TOTAL AREA(ACRES) =      0.20    TOTAL RUNOFF(CFS) =      1.04

*****
FLOW PROCESS FROM NODE    5040.00 TO NODE    5041.00 IS CODE =   62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #   1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =  475.00  DOWNSTREAM ELEVATION(FEET) =  454.00
STREET LENGTH(FEET) =    390.00    CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =    36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =   31.00
INSIDE STREET CROSSFALL(DECIMAL) =   0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =   0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    2
STREET PARKWAY CROSSFALL(DECIMAL) =   0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =   0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =   0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =      7.10
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =   0.28
HALFSTREET FLOOD WIDTH(FEET) =    8.97
AVERAGE FLOW VELOCITY(FEET/SEC.) =    3.99
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    1.13
STREET FLOW TRAVEL TIME(MIN.) =   1.63    Tc(MIN.) =    7.66
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   7.201
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT =   .6200
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT =   0.620
SUBAREA AREA(ACRES) =    2.70    SUBAREA RUNOFF(CFS) =   12.05
TOTAL AREA(ACRES) =    2.90    PEAK FLOW RATE(CFS) =   12.95

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.33    HALFSTREET FLOOD WIDTH(FEET) =   11.45
FLOW VELOCITY(FEET/SEC.) =  4.63    DEPTH*VELOCITY(FT*FT/SEC.) =   1.55
LONGEST FLOWPATH FROM NODE    5039.00 TO NODE    5041.00 =   455.00 FEET.

*****
FLOW PROCESS FROM NODE    5041.00 TO NODE    5041.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    2 ARE:
TIME OF CONCENTRATION(MIN.) =    7.66
RAINFALL INTENSITY(INCH/HR) =    7.20
TOTAL STREAM AREA(ACRES) =    2.90
PEAK FLOW RATE(CFS) AT CONFLUENCE =   12.95

** CONFLUENCE DATA **
STREAM    RUNOFF    Tc    INTENSITY    AREA
NUMBER    (CFS)    (MIN.)    (INCH/HOUR)    (ACRE)

```

1	110.73	5.45	8.968	48.30
2	12.95	7.66	7.201	2.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	119.94	5.45	8.968
2	101.85	7.66	7.201

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 119.94 Tc(MIN.) = 5.45

TOTAL AREA(ACRES) = 51.20

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5041.00 = 1890.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5041.00 TO NODE 5055.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 444.00 DOWNSTREAM(FEET) = 442.00

FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 39.0 INCH PIPE IS 29.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 18.08

ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 119.94

PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 5.52

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5055.00 = 1960.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5055.00 TO NODE 5055.00 IS CODE = 10  
-----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5043.00 TO NODE 5044.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 530.00

DOWNSTREAM ELEVATION(FEET) = 470.00

ELEVATION DIFFERENCE(FEET) = 60.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865

SUBAREA RUNOFF(CFS) = 0.47

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*

```

FLOW PROCESS FROM NODE    5044.00 TO NODE    5045.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   470.00  DOWNSTREAM(FEET) =   460.00
FLOW LENGTH(FEET) =  1220.00  MANNING'S N =  0.016
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   3.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   2.34
ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =           0.47
PIPE TRAVEL TIME(MIN.) =   8.68  , Tc(MIN.) =  15.37
LONGEST FLOWPATH FROM NODE    5043.00 TO NODE    5045.00 =  1320.00 FEET.

*****
FLOW PROCESS FROM NODE    5044.00 TO NODE    5045.00 IS CODE =  81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  4.598
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .3200
S.C.S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.3186
SUBAREA AREA(ACRES) =    2.70  SUBAREA RUNOFF(CFS) =    3.97
TOTAL AREA(ACRES) =    2.90  TOTAL RUNOFF(CFS) =    4.25
TC(MIN.) =  15.37

*****
FLOW PROCESS FROM NODE    5045.00 TO NODE    5050.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   450.00  DOWNSTREAM(FEET) =   442.00
FLOW LENGTH(FEET) =   150.00  MANNING'S N =  0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   5.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   9.93
ESTIMATED PIPE DIAMETER(INCH) =  18.00    NUMBER OF PIPES =   1
PIPE-FLOW(CFS) =           4.25
PIPE TRAVEL TIME(MIN.) =   0.25  , Tc(MIN.) =  15.62
LONGEST FLOWPATH FROM NODE    5043.00 TO NODE    5050.00 =  1470.00 FEET.

*****
FLOW PROCESS FROM NODE    5050.00 TO NODE    5050.00 IS CODE =   1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =  15.62
RAINFALL INTENSITY(INCH/HR) =   4.55
TOTAL STREAM AREA(ACRES) =    2.90
PEAK FLOW RATE(CFS) AT CONFLUENCE =    4.25

```

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*****
FLOW PROCESS FROM NODE    5047.00 TO NODE    5048.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) =  0
INITIAL SUBAREA FLOW-LENGTH(FEET) =    65.00
UPSTREAM ELEVATION(FEET) =    466.00
DOWNSTREAM ELEVATION(FEET) =    465.00
ELEVATION DIFFERENCE(FEET) =      1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    5.908
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  8.517
SUBAREA RUNOFF(CFS) =      1.61
TOTAL AREA(ACRES) =      0.30  TOTAL RUNOFF(CFS) =      1.61

*****
FLOW PROCESS FROM NODE    5048.00 TO NODE    5049.00 IS CODE =  62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #  1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =  465.00  DOWNSTREAM ELEVATION(FEET) =  456.00
STREET LENGTH(FEET) =  530.00  CURB HEIGHT(INCHES) =  6.0
STREET HALFWIDTH(FEET) =  36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =  31.00
INSIDE STREET CROSSFALL(DECIMAL) =  0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =  0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =  2
STREET PARKWAY CROSSFALL(DECIMAL) =  0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =  0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =  0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =      8.78
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =  0.35
HALFSTREET FLOOD WIDTH(FEET) =  12.36
AVERAGE FLOW VELOCITY(FEET/SEC.) =  2.72
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =  0.96
STREET FLOW TRAVEL TIME(MIN.) =  3.25  Tc(MIN.) =  9.15
  100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  6.421
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT =  0.630
SUBAREA AREA(ACRES) =  3.50  SUBAREA RUNOFF(CFS) =  14.16
TOTAL AREA(ACRES) =  3.80  PEAK FLOW RATE(CFS) =  15.37

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =  0.41  HALFSTREET FLOOD WIDTH(FEET) =  15.44
FLOW VELOCITY(FEET/SEC.) =  3.11  DEPTH*VELOCITY(FT*FT/SEC.) =  1.29
LONGEST FLOWPATH FROM NODE    5047.00 TO NODE    5049.00 =  595.00 FEET.
*****

```

FLOW PROCESS FROM NODE 5049.00 TO NODE 5050.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 450.00 DOWNSTREAM(FEET) = 442.00  
FLOW LENGTH(FEET) = 670.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.1 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.76  
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.37  
PIPE TRAVEL TIME(MIN.) = 1.44 Tc(MIN.) = 10.59  
LONGEST FLOWPATH FROM NODE 5047.00 TO NODE 5050.00 = 1265.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5050.00 TO NODE 5050.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.59  
RAINFALL INTENSITY(INCH/HR) = 5.84  
TOTAL STREAM AREA(ACRES) = 3.80  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.37

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.25	15.62	4.550	2.90
2	15.37	10.59	5.844	3.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	18.25	10.59	5.844
2	16.22	15.62	4.550

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 18.25 Tc(MIN.) = 10.59

TOTAL AREA(ACRES) = 6.70

LONGEST FLOWPATH FROM NODE 5043.00 TO NODE 5050.00 = 1470.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5050.00 TO NODE 5054.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 442.00 DOWNSTREAM(FEET) = 441.00  
FLOW LENGTH(FEET) = 25.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.5 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.79

ESTIMATED PIPE DIAMETER(INCH) = 18.00      NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 18.25  
 PIPE TRAVEL TIME(MIN.) = 0.03      Tc(MIN.) = 10.63  
 LONGEST FLOWPATH FROM NODE 5043.00 TO NODE 5054.00 = 1495.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5054.00 TO NODE 5054.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.63  
 RAINFALL INTENSITY(INCH/HR) = 5.83  
 TOTAL STREAM AREA(ACRES) = 6.70  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.25

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5052.00 TO NODE 5053.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 457.00  
 DOWNSTREAM ELEVATION(FEET) = 456.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517  
 SUBAREA RUNOFF(CFS) = 1.07  
 TOTAL AREA(ACRES) = 0.20      TOTAL RUNOFF(CFS) = 1.07

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5053.00 TO NODE 5054.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 456.00      DOWNSTREAM ELEVATION(FEET) = 448.00  
 STREET LENGTH(FEET) = 670.00      CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 31.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.97  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.37  
 HALFSTREET FLOOD WIDTH(FEET) = 13.39

AVERAGE FLOW VELOCITY (FEET/SEC.) = 2.39  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.89  
 STREET FLOW TRAVEL TIME (MIN.) = 4.67 Tc (MIN.) = 10.58  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 5.848  
 \*USER SPECIFIED (SUBAREA) :  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
 SUBAREA AREA (ACRES) = 4.20 SUBAREA RUNOFF (CFS) = 15.47  
 TOTAL AREA (ACRES) = 4.40 PEAK FLOW RATE (CFS) = 16.21

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.44 HALFSTREET FLOOD WIDTH (FEET) = 16.90  
 FLOW VELOCITY (FEET/SEC.) = 2.76 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.22  
 LONGEST FLOWPATH FROM NODE 5052.00 TO NODE 5054.00 = 735.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5054.00 TO NODE 5054.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 10.58  
 RAINFALL INTENSITY (INCH/HR) = 5.85  
 TOTAL STREAM AREA (ACRES) = 4.40  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 16.21

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	18.25	10.63	5.833	6.70
2	16.21	10.58	5.848	4.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	34.42	10.58	5.848
2	34.42	10.63	5.833

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 34.42 Tc (MIN.) = 10.63  
 TOTAL AREA (ACRES) = 11.10  
 LONGEST FLOWPATH FROM NODE 5043.00 TO NODE 5054.00 = 1495.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5054.00 TO NODE 5055.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 441.00 DOWNSTREAM (FEET) = 440.00  
 FLOW LENGTH (FEET) = 90.00 MANNING'S N = 0.013



DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.0 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 9.36  
 ESTIMATED PIPE DIAMETER (INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 34.42  
 PIPE TRAVEL TIME (MIN.) = 0.16 Tc (MIN.) = 10.79  
 LONGEST FLOWPATH FROM NODE 5043.00 TO NODE 5055.00 = 1585.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5055.00 TO NODE 5055.00 IS CODE = 11  
 -----  
 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	34.42	10.79	5.777	11.10

LONGEST FLOWPATH FROM NODE 5043.00 TO NODE 5055.00 = 1585.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	119.94	5.52	8.900	51.20

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5055.00 = 1960.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	137.55	5.52	8.900
2	112.27	10.79	5.777

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 137.55 Tc (MIN.) = 5.52  
 TOTAL AREA (ACRES) = 62.30

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5055.00 TO NODE 5055.00 IS CODE = 12  
 -----  
 >>>>CLEAR MEMORY BANK # 1 <<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5055.00 TO NODE 5059.00 IS CODE = 31  
 -----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM (FEET) = 440.00 DOWNSTREAM (FEET) = 420.00  
 FLOW LENGTH (FEET) = 330.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 26.3 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 24.88  
 ESTIMATED PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 137.55  
 PIPE TRAVEL TIME (MIN.) = 0.22 Tc (MIN.) = 5.74  
 LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5059.00 = 2290.00 FEET.

\*\*\*\*\*

```

FLOW PROCESS FROM NODE    5059.00 TO NODE    5059.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    5.74
RAINFALL INTENSITY(INCH/HR) =    8.68
TOTAL STREAM AREA(ACRES) =    62.30
PEAK FLOW RATE(CFS) AT CONFLUENCE =    137.55

*****
FLOW PROCESS FROM NODE    5057.00 TO NODE    5058.00 IS CODE =    21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =    65.00
UPSTREAM ELEVATION(FEET) =    451.00
DOWNSTREAM ELEVATION(FEET) =    450.00
ELEVATION DIFFERENCE(FEET) =    1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    6.160
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  8.291
SUBAREA RUNOFF(CFS) =    1.01
TOTAL AREA(ACRES) =    0.20  TOTAL RUNOFF(CFS) =    1.01

*****
FLOW PROCESS FROM NODE    5058.00 TO NODE    5059.00 IS CODE =    62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #  1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =  450.00  DOWNSTREAM ELEVATION(FEET) =  430.00
STREET LENGTH(FEET) =  350.00  CURB HEIGHT(INCHES) =  6.0
STREET HALFWIDTH(FEET) =  36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =  31.00
INSIDE STREET CROSSFALL(DECIMAL) =  0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =  0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =  2
STREET PARKWAY CROSSFALL(DECIMAL) =  0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =  0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =  0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    6.34
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =  0.27
HALFSTREET FLOOD WIDTH(FEET) =    8.42
AVERAGE FLOW VELOCITY(FEET/SEC.) =    3.99
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    1.09
STREET FLOW TRAVEL TIME(MIN.) =  1.46  Tc(MIN.) =  7.62
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  7.227
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6400

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S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.638  
 SUBAREA AREA (ACRES) = 2.30 SUBAREA RUNOFF (CFS) = 10.64  
 TOTAL AREA (ACRES) = 2.50 PEAK FLOW RATE (CFS) = 11.52

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.32 HALFSTREET FLOOD WIDTH (FEET) = 10.78  
 FLOW VELOCITY (FEET/SEC.) = 4.61 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.48  
 LONGEST FLOWPATH FROM NODE 5057.00 TO NODE 5059.00 = 415.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5059.00 TO NODE 5059.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 7.62  
 RAINFALL INTENSITY (INCH/HR) = 7.23  
 TOTAL STREAM AREA (ACRES) = 2.50  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 11.52

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	137.55	5.74	8.677	62.30
2	11.52	7.62	7.227	2.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	146.23	5.74	8.677
2	126.07	7.62	7.227

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 146.23 Tc (MIN.) = 5.74  
 TOTAL AREA (ACRES) = 64.80  
 LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5059.00 = 2290.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5059.00 TO NODE 5063.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 420.00 DOWNSTREAM (FEET) = 387.00  
 FLOW LENGTH (FEET) = 570.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 28.3 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 24.53  
 ESTIMATED PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 146.23  
 PIPE TRAVEL TIME (MIN.) = 0.39 Tc (MIN.) = 6.13  
 LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5063.00 = 2860.00 FEET.

```

*****
FLOW PROCESS FROM NODE    5063.00 TO NODE    5063.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    1 ARE:
TIME OF CONCENTRATION(MIN.) =    6.13
RAINFALL INTENSITY(INCH/HR) =    8.32
TOTAL STREAM AREA(ACRES) =    64.80
PEAK FLOW RATE(CFS) AT CONFLUENCE =    146.23

*****
FLOW PROCESS FROM NODE    5061.00 TO NODE    5062.00 IS CODE =    21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =    65.00
UPSTREAM ELEVATION(FEET) =    426.00
DOWNSTREAM ELEVATION(FEET) =    425.00
ELEVATION DIFFERENCE(FEET) =    1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    5.908
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    8.517
SUBAREA RUNOFF(CFS) =    1.07
TOTAL AREA(ACRES) =    0.20    TOTAL RUNOFF(CFS) =    1.07

*****
FLOW PROCESS FROM NODE    5062.00 TO NODE    5063.00 IS CODE =    62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION #    1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) =    425.00    DOWNSTREAM ELEVATION(FEET) =    397.00
STREET LENGTH(FEET) =    490.00    CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =    36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =    31.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =    0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    2
STREET PARKWAY CROSSFALL(DECIMAL) =    0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =    0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =    0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =    8.04
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =    0.29
HALFSTREET FLOOD WIDTH(FEET) =    9.33
AVERAGE FLOW VELOCITY(FEET/SEC.) =    4.20
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    1.23
STREET FLOW TRAVEL TIME(MIN.) =    1.94    Tc(MIN.) =    7.85
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    7.090

```

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.630  
 SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 13.85  
 TOTAL AREA(ACRES) = 3.30 PEAK FLOW RATE(CFS) = 14.74

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 11.93  
 FLOW VELOCITY(FEET/SEC.) = 4.88 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.68  
 LONGEST FLOWPATH FROM NODE 5061.00 TO NODE 5063.00 = 555.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5063.00 TO NODE 5063.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.85  
 RAINFALL INTENSITY(INCH/HR) = 7.09  
 TOTAL STREAM AREA(ACRES) = 3.30  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.74

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	146.23	6.13	8.320	64.80
2	14.74	7.85	7.090	3.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	157.73	6.13	8.320
2	139.35	7.85	7.090

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 157.73 Tc(MIN.) = 6.13  
 TOTAL AREA(ACRES) = 68.10  
 LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5063.00 = 2860.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5063.00 TO NODE 5090.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 387.00 DOWNSTREAM(FEET) = 319.50  
 FLOW LENGTH(FEET) = 860.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 26.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 28.34  
 ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 157.73

PIPE TRAVEL TIME(MIN.) = 0.51 Tc(MIN.) = 6.63  
LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5090.50 = 3720.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5090.50 TO NODE 5090.50 IS CODE = 10

-----  
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<  
=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5065.00 TO NODE 5066.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
=====

\*USER SPECIFIED(SUBAREA) :  
USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 500.00  
DOWNSTREAM ELEVATION(FEET) = 499.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517  
SUBAREA RUNOFF(CFS) = 1.07  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.07

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5066.00 TO NODE 5067.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<  
=====

UPSTREAM ELEVATION(FEET) = 499.00 DOWNSTREAM ELEVATION(FEET) = 491.00  
STREET LENGTH(FEET) = 420.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 31.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.73  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 11.51  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.74  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.92  
STREET FLOW TRAVEL TIME(MIN.) = 2.55 Tc(MIN.) = 8.46  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.755  
\*USER SPECIFIED(SUBAREA) :  
USER-SPECIFIED RUNOFF COEFFICIENT = .6300  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630

SUBAREA AREA(ACRES) = 3.10 SUBAREA RUNOFF(CFS) = 13.19  
TOTAL AREA(ACRES) = 3.30 PEAK FLOW RATE(CFS) = 14.04

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 14.60  
FLOW VELOCITY(FEET/SEC.) = 3.17 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.26  
LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5067.00 = 485.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5067.00 TO NODE 5068.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 481.00 DOWNSTREAM(FEET) = 440.00  
FLOW LENGTH(FEET) = 180.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 14.04  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 8.59  
LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5068.00 = 665.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 5068.00 TO NODE 5077.50 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 440.00 DOWNSTREAM(FEET) = 400.00  
CHANNEL LENGTH THRU SUBAREA(FEET) = 520.00 CHANNEL SLOPE = 0.0769  
CHANNEL BASE(FEET) = 5.00 "Z" FACTOR = 1.500  
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 3.00  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.093  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 17.91  
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.47  
AVERAGE FLOW DEPTH(FEET) = 0.48 TRAVEL TIME(MIN.) = 1.34  
Tc(MIN.) = 9.93  
SUBAREA AREA(ACRES) = 4.20 SUBAREA RUNOFF(CFS) = 7.68  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.445  
TOTAL AREA(ACRES) = 7.50 PEAK FLOW RATE(CFS) = 20.35

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.52 FLOW VELOCITY(FEET/SEC.) = 6.74  
LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5077.50 = 1185.00 FEET:

\*\*\*\*\*

FLOW PROCESS FROM NODE 5077.50 TO NODE 5077.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 9.93  
RAINFALL INTENSITY(INCH/HR) = 6.09  
TOTAL STREAM AREA(ACRES) = 7.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.35

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5070.00 TO NODE 5071.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6400  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 425.00  
DOWNSTREAM ELEVATION(FEET) = 424.00  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.783  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.636  
SUBAREA RUNOFF(CFS) = 1.11  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5071.00 TO NODE 5072.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 424.00 DOWNSTREAM ELEVATION(FEET) = 423.00  
STREET LENGTH(FEET) = 140.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 36.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 31.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.97  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 11.69  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.71  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.58  
STREET FLOW TRAVEL TIME(MIN.) = 1.36 Tc(MIN.) = 7.15  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.533

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6400  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.640  
SUBAREA AREA(ACRES) = 1.60 SUBAREA RUNOFF(CFS) = 7.71  
TOTAL AREA(ACRES) = 1.80 PEAK FLOW RATE(CFS) = 8.68

END OF SUBAREA STREET FLOW HYDRAULICS:



DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 14.60  
 FLOW VELOCITY(FEET/SEC.) = 1.96 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.78  
 LONGEST FLOWPATH FROM NODE 5070.00 TO NODE 5072.00 = 205.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5072.00 TO NODE 5077.50 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	413.00	DOWNSTREAM(FEET) =	392.00
FLOW LENGTH(FEET) =	110.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO	18.000		
DEPTH OF FLOW IN 18.0 INCH PIPE IS	5.5 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	19.22		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	8.68		
PIPE TRAVEL TIME(MIN.) =	0.10	Tc(MIN.) =	7.24
LONGEST FLOWPATH FROM NODE 5070.00 TO NODE 5077.50 =	315.00 FEET.		

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5077.50 TO NODE 5077.50 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	7.24
RAINFALL INTENSITY(INCH/HR) =	7.47
TOTAL STREAM AREA(ACRES) =	1.80
PEAK FLOW RATE(CFS) AT CONFLUENCE =	8.68

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5075.00 TO NODE 5076.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2700
S.C.S. CURVE NUMBER (AMC II) =	0
INITIAL SUBAREA FLOW-LENGTH(FEET) =	50.00
UPSTREAM ELEVATION(FEET) =	415.00
DOWNSTREAM ELEVATION(FEET) =	398.00
ELEVATION DIFFERENCE(FEET) =	17.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.904

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	9.485
--	-------

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) =	0.51		
TOTAL AREA(ACRES) =	0.20	TOTAL RUNOFF(CFS) =	0.51

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5076.00 TO NODE 5077.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 398.00 DOWNSTREAM(FEET) = 394.00  
 FLOW LENGTH(FEET) = 460.00 MANNING'S N = 0.016  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 3.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 2.44  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.51  
 PIPE TRAVEL TIME(MIN.) = 3.14 Tc(MIN.) = 8.05  
 LONGEST FLOWPATH FROM NODE 5075.00 TO NODE 5077.00 = 510.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5076.00 TO NODE 5077.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.978  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3100  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3020  
 SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 1.73  
 TOTAL AREA(ACRES) = 1.00 TOTAL RUNOFF(CFS) = 2.11  
 TC(MIN.) = 8.05

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5077.00 TO NODE 5077.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 385.00 DOWNSTREAM(FEET) = 384.00  
 FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.7 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.74  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 2.11  
 PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 8.19  
 LONGEST FLOWPATH FROM NODE 5075.00 TO NODE 5077.50 = 560.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5077.50 TO NODE 5077.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.19  
 RAINFALL INTENSITY(INCH/HR) = 6.90  
 TOTAL STREAM AREA(ACRES) = 1.00  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.11

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	20.35	9.93	6.093	7.50

2	8.68	7.24	7.469	1.80
3	2.11	8.19	6.898	1.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	25.38	7.24	7.469
2	26.91	8.19	6.898
3	29.29	9.93	6.093

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 29.29 Tc(MIN.) = 9.93  
TOTAL AREA(ACRES) = 10.30  
LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5077.50 = 1185.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5077.50 TO NODE 5073.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 384.00 DOWNSTREAM( FEET) = 381.00  
FLOW LENGTH( FEET) = 100.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.1 INCHES  
PIPE-FLOW VELOCITY( FEET/SEC.) = 13.11  
ESTIMATED PIPE DIAMETER( INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 29.29  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 10.06  
LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5073.00 = 1285.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5073.00 TO NODE 5073.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 10.06  
RAINFALL INTENSITY(INCH/HR) = 6.04  
TOTAL STREAM AREA(ACRES) = 10.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 29.29

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5072.30 TO NODE 5072.60 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH( FEET) = 100.00  
UPSTREAM ELEVATION( FEET) = 458.00  
DOWNSTREAM ELEVATION( FEET) = 440.00  
ELEVATION DIFFERENCE( FEET) = 18.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.684  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.865  
 SUBAREA RUNOFF(CFS) = 0.47  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.47

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5072.60 TO NODE 5073.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) =	440.00	DOWNSTREAM( FEET) =	400.00
CHANNEL LENGTH THRU SUBAREA( FEET) =	350.00	CHANNEL SLOPE =	0.1143
CHANNEL BASE( FEET) =	5.00	"Z" FACTOR =	1.500
MANNING'S FACTOR =	0.035	MAXIMUM DEPTH( FEET) =	3.00
100 YEAR RAINFALL INTENSITY( INCH/HOUR) =	6.721		

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.79  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC.) = 3.16  
 AVERAGE FLOW DEPTH( FEET) = 0.11 TRAVEL TIME(MIN.) = 1.85  
 Tc(MIN.) = 8.53  
 SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 2.62  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.300  
 TOTAL AREA(ACRES) = 1.50 PEAK FLOW RATE(CFS) = 3.02

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH( FEET) = 0.15 FLOW VELOCITY( FEET/SEC.) = 3.87  
 LONGEST FLOWPATH FROM NODE 5072.30 TO NODE 5073.00 = 450.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5073.00 TO NODE 5073.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 8.53  
 RAINFALL INTENSITY(INCH/HR) = 6.72  
 TOTAL STREAM AREA(ACRES) = 1.50  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.02

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	29.29	10.06	6.043	10.30
2	3.02	8.53	6.721	1.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
------------------	-----------------	--------------	--------------------------

1	29.36	8.53	6.721
2	32.01	10.06	6.043

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 32.01 Tc(MIN.) = 10.06

TOTAL AREA(ACRES) = 11.80

LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5073.00 = 1285.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5073.00 TO NODE 5082.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 381.00 DOWNSTREAM(FEET) = 330.00

FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 32.86

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 32.01

PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 10.14

LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5082.00 = 1445.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5082.00 TO NODE 5082.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 10.14

RAINFALL INTENSITY(INCH/HR) = 6.01

TOTAL STREAM AREA(ACRES) = 11.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 32.01

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5079.00 TO NODE 5080.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 397.00

DOWNSTREAM ELEVATION(FEET) = 350.00

ELEVATION DIFFERENCE(FEET) = 47.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 7.102

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.564

SUBAREA RUNOFF(CFS) = 0.38

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.38

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5080.00 TO NODE 5082.00 IS CODE = 31  
-----

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 350.00 DOWNSTREAM(FEET) = 343.00
FLOW LENGTH(FEET) = 780.00 MANNING'S N = 0.016
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.27
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.38
PIPE TRAVEL TIME(MIN.) = 5.73 Tc(MIN.) = 12.83
LONGEST FLOWPATH FROM NODE 5079.00 TO NODE 5082.00 = 880.00 FEET.

*****
FLOW PROCESS FROM NODE 5080.00 TO NODE 5082.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.165
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2800
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2773
SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 2.89
TOTAL AREA(ACRES) = 2.20 TOTAL RUNOFF(CFS) = 3.15
TC(MIN.) = 12.83

*****
FLOW PROCESS FROM NODE 5082.00 TO NODE 5082.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.83
RAINFALL INTENSITY(INCH/HR) = 5.17
TOTAL STREAM AREA(ACRES) = 2.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.15

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 32.01 10.14 6.012 11.80
2 3.15 12.83 5.165 2.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 34.50 10.14 6.012
2 30.65 12.83 5.165

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 34.50 Tc(MIN.) = 10.14

```

TOTAL AREA(ACRES) = 14.00  
LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 5082.00 = 1445.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5082.00 TO NODE 6026.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	333.00	DOWNSTREAM(FEET) =	330.00
FLOW LENGTH(FEET) =	60.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS	15.1 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	16.62		
ESTIMATED PIPE DIAMETER(INCH) =	24.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	34.50		
PIPE TRAVEL TIME(MIN.) =	0.06	Tc(MIN.) =	10.20
LONGEST FLOWPATH FROM NODE 5065.00 TO NODE 6026.00 =	1505.00 FEET.		

=====

+-----+  
| Information for Node 6026 |  
+-----+

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5084.00 TO NODE 5085.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.7700
S.C.S. CURVE NUMBER (AMC II) =	0
INITIAL SUBAREA FLOW-LENGTH(FEET) =	65.00
UPSTREAM ELEVATION(FEET) =	327.00
DOWNSTREAM ELEVATION(FEET) =	326.00
ELEVATION DIFFERENCE(FEET) =	1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =	4.148
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.	
SUBAREA RUNOFF(CFS) =	2.19
TOTAL AREA(ACRES) =	0.30
TOTAL RUNOFF(CFS) =	2.19

=====

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5085.00 TO NODE 5086.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) =	326.00	DOWNSTREAM ELEVATION(FEET) =	323.50
STREET LENGTH(FEET) =	200.00	CURB HEIGHT(INCHES) =	6.0
STREET HALFWIDTH(FEET) =	36.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =	31.00
INSIDE STREET CROSSFALL(DECIMAL) =	0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.60  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(Feet) = 0.34  
HALFSTREET FLOOD WIDTH(Feet) = 11.75  
AVERAGE FLOW VELOCITY(Feet/Sec.) = 2.25  
PRODUCT OF DEPTH&VELOCITY(Feet\*Feet/Sec.) = 0.76  
STREET FLOW TRAVEL TIME(Min.) = 1.48 Tc(Min.) = 5.63  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.785  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
SUBAREA AREA(ACRES) = 1.30 SUBAREA RUNOFF(CFS) = 8.79  
TOTAL AREA(ACRES) = 1.60 PEAK FLOW RATE(CFS) = 10.82

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(Feet) = 0.39 HALFSTREET FLOOD WIDTH(Feet) = 14.29  
FLOW VELOCITY(Feet/Sec.) = 2.54 DEPTH\*VELOCITY(Feet\*Feet/Sec.) = 0.99  
LONGEST FLOWPATH FROM NODE 5084.00 TO NODE 5086.00 = 265.00 FEET.

```

+-----+
| Flow Information for Node 5086 |
+-----+

```

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5088.00 TO NODE 5089.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(Feet) = 65.00
UPSTREAM ELEVATION(Feet) = 328.00
DOWNSTREAM ELEVATION(Feet) = 327.00
ELEVATION DIFFERENCE(Feet) = 1.00
SUBAREA OVERLAND TIME OF FLOW(Min.) = 4.148
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 4.38
TOTAL AREA(ACRES) = 0.60 TOTAL RUNOFF(CFS) = 4.38

```

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5089.00 TO NODE 5090.00 IS CODE = 62  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

```

=====
UPSTREAM ELEVATION(Feet) = 327.00 DOWNSTREAM ELEVATION(Feet) = 323.00
STREET LENGTH(Feet) = 360.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(Feet) = 36.00

```



DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 31.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.50  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.39  
HALFSTREET FLOOD WIDTH(FEET) = 14.48  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.41  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.95  
STREET FLOW TRAVEL TIME(MIN.) = 2.49 Tc(MIN.) = 6.64  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.899  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 12.16  
TOTAL AREA(ACRES) = 2.60 PEAK FLOW RATE(CFS) = 15.81

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 16.96  
FLOW VELOCITY(FEET/SEC.) = 2.67 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.19  
LONGEST FLOWPATH FROM NODE 5088.00 TO NODE 5090.00 = 425.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5090.00 TO NODE 5090.50 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<  
=====

ELEVATION DATA: UPSTREAM(FEET) = 320.00 DOWNSTREAM(FEET) = 319.50  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 7.47  
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 15.81  
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 6.75  
LONGEST FLOWPATH FROM NODE 5088.00 TO NODE 5090.50 = 475.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 5090.50 TO NODE 5090.50 IS CODE = 11

-----  
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<  
=====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	15.81	6.75	7.814	2.60

LONGEST FLOWPATH FROM NODE 5088.00 TO NODE 5090.50 = 475.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	157.73	6.63	7.905	68.10

LONGEST FLOWPATH FROM NODE 5002.00 TO NODE 5090.50 = 3720.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	173.26	6.63	7.905
2	171.73	6.75	7.814

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 173.26 Tc(MIN.) = 6.63

TOTAL AREA(ACRES) = 70.70

\*\*\*\*\*

FLOW PROCESS FROM NODE 5090.50 TO NODE 5090.50 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

Flow Information for Node 5090.5

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 70.70 TC(MIN.) = 6.63

PEAK FLOW RATE(CFS) = 173.26

END OF RATIONAL METHOD ANALYSIS

**Flow Information For Drainage  
Basin 7000A  
(Node 6010)  
(Node 7068)**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

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619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 07/16/09 \*  
\* 100-yr Post-project (on-site) \*  
\* \*  
\*\*\*\*\*

FILE NAME: MW\_6K100.DAT  
TIME/DATE OF STUDY: 10:36 07/20/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS  
\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*  
HALF- CROWN TO STREET-CROSSFALL: CURB GUTTER-GEOMETRIES: MANNING  
WIDTH CROSSFALL IN- / OUT-/PARK- HEIGHT WIDTH LIP HIKE FACTOR  
NO. (FT) (FT) SIDE / SIDE/ WAY (FT) (FT) (FT) (FT) (n)  
=== =====  
1 12.0 7.0 0.020/0.020/0.020 0.50 1.50 0.0100 0.125 0.0180

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6000.00 TO NODE 6001.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .2800  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00  
 UPSTREAM ELEVATION(FEET) = 480.00  
 DOWNSTREAM ELEVATION(FEET) = 455.00  
 ELEVATION DIFFERENCE(FEET) = 25.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.845  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 0.53  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.53

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6001.00 TO NODE 6002.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 455.00 DOWNSTREAM(FEET) = 449.00  
 FLOW LENGTH(FEET) = 170.00 MANNING'S N = 0.016  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 4.06  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 0.53  
 PIPE TRAVEL TIME(MIN.) = 0.70 Tc(MIN.) = 5.54  
 LONGEST FLOWPATH FROM NODE 6000.00 TO NODE 6002.00 = 220.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6001.00 TO NODE 6002.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.874  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.2933  
 SUBAREA AREA(ACRES) = 0.40 SUBAREA RUNOFF(CFS) = 1.06  
 TOTAL AREA(ACRES) = 0.60 TOTAL RUNOFF(CFS) = 1.56  
 TC(MIN.) = 5.54

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6002.00 TO NODE 6006.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====  
 ELEVATION DATA: UPSTREAM(FEET) = 439.00 DOWNSTREAM(FEET) = 415.00  
 FLOW LENGTH(FEET) = 65.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 14.67  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.56  
 PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 5.62  
 LONGEST FLOWPATH FROM NODE 6000.00 TO NODE 6006.00 = 285.00 FEET.

```

*****
FLOW PROCESS FROM NODE    6006.00 TO NODE    6006.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    5.62
RAINFALL INTENSITY(INCH/HR) =    8.80
TOTAL STREAM AREA(ACRES) =    0.60
PEAK FLOW RATE(CFS) AT CONFLUENCE =          1.56

*****
FLOW PROCESS FROM NODE    6004.00 TO NODE    6005.00 IS CODE =   21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2900
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =    40.00
UPSTREAM ELEVATION(FEET) =    447.00
DOWNSTREAM ELEVATION(FEET) =    427.00
ELEVATION DIFFERENCE(FEET) =    20.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.280
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) =          0.55
TOTAL AREA(ACRES) =          0.20  TOTAL RUNOFF(CFS) =          0.55

*****
FLOW PROCESS FROM NODE    6005.00 TO NODE    6006.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    427.00  DOWNSTREAM(FEET) =    425.00
FLOW LENGTH(FEET) =    100.00  MANNING'S N =    0.016
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS  2.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    3.35
ESTIMATED PIPE DIAMETER(INCH) =    18.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =          0.55
PIPE TRAVEL TIME(MIN.) =    0.50  Tc(MIN.) =    4.78
LONGEST FLOWPATH FROM NODE    6004.00 TO NODE    6006.00 =    140.00 FEET.

*****
FLOW PROCESS FROM NODE    6005.00 TO NODE    6006.00 IS CODE =   81
-----
>>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) =    0

```

AREA-AVERAGE RUNOFF COEFFICIENT = 0.2950  
 SUBAREA AREA(ACRES) = 0.20 SUBAREA RUNOFF(CFS) = 0.57  
 TOTAL AREA(ACRES) = 0.40 TOTAL RUNOFF(CFS) = 1.12  
 TC(MIN.) = 4.78

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6006.00 TO NODE 6006.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	4.78
RAINFALL INTENSITY(INCH/HR) =	9.49
TOTAL STREAM AREA(ACRES) =	0.40
PEAK FLOW RATE(CFS) AT CONFLUENCE =	1.12

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	1.56	5.62	8.799	0.60
2	1.12	4.78	9.485	0.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	2.45	4.78	9.485
2	2.60	5.62	8.799

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 2.60 Tc(MIN.) = 5.62  
 TOTAL AREA(ACRES) = 1.00  
 LONGEST FLOWPATH FROM NODE 6000.00 TO NODE 6006.00 = 285.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6006.00 TO NODE 6011.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	415.00	DOWNSTREAM(FEET) =	413.00
FLOW LENGTH(FEET) =	170.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO	18.000		
DEPTH OF FLOW IN 18.0 INCH PIPE IS	6.0 INCHES		
PIPE-FLOW VELOCITY(FEET/SEC.) =	5.04		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	2.60		
PIPE TRAVEL TIME(MIN.) =	0.56	Tc(MIN.) =	6.18
LONGEST FLOWPATH FROM NODE 6000.00 TO NODE 6011.00 =	455.00 FEET.		

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6011.00 TO NODE 6011.00 IS CODE = 1  
 -----

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.18
RAINFALL INTENSITY(INCH/HR) = 8.27
TOTAL STREAM AREA(ACRES) = 1.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.60

*****
FLOW PROCESS FROM NODE 6012.00 TO NODE 6013.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 429.00
DOWNSTREAM ELEVATION(FEET) = 428.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.908
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.517
SUBAREA RUNOFF(CFS) = 1.07
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.07

*****
FLOW PROCESS FROM NODE 6013.00 TO NODE 6014.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 428.00 DOWNSTREAM ELEVATION(FEET) = 424.00
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.33
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.31
HALFSTREET FLOOD WIDTH(FEET) = 10.39
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.29
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.72
STREET FLOW TRAVEL TIME(MIN.) = 1.97 Tc(MIN.) = 7.88
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.076
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6300
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.630

```



SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 8.47  
 TOTAL AREA(ACRES) = 2.10 PEAK FLOW RATE(CFS) = 9.36

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 12.00  
 FLOW VELOCITY(FEET/SEC.) = 2.71 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.98  
 LONGEST FLOWPATH FROM NODE 6012.00 TO NODE 6014.00 = 335.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 6014.00 TO NODE 6011.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 413.50 DOWNSTREAM(FEET) = 413.00

FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.96

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 9.36

PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 7.94

LONGEST FLOWPATH FROM NODE 6012.00 TO NODE 6011.00 = 365.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 6011.00 TO NODE 6011.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 7.94

RAINFALL INTENSITY(INCH/HR) = 7.04

TOTAL STREAM AREA(ACRES) = 2.10

PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.36

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	2.60	6.18	8.274	1.00
2	9.36	7.94	7.039	2.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	9.89	6.18	8.274
2	11.57	7.94	7.039

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.57 Tc(MIN.) = 7.94

TOTAL AREA(ACRES) = 3.10

LONGEST FLOWPATH FROM NODE 6000.00 TO NODE 6011.00 = 455.00 FEET.

\*\*\*\*\*

```

FLOW PROCESS FROM NODE    6011.00 TO NODE    6010.00 IS CODE =   31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   413.00  DOWNSTREAM(FEET) =   411.00
FLOW LENGTH(FEET) =   365.00  MANNING'S N =   0.013
DEPTH OF FLOW IN  24.0 INCH PIPE IS  15.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    5.53
ESTIMATED PIPE DIAMETER(INCH) =   24.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =    11.57
PIPE TRAVEL TIME(MIN.) =    1.10  Tc(MIN.) =    9.04
LONGEST FLOWPATH FROM NODE    6000.00 TO NODE    6010.00 =   820.00 FEET.

*****
FLOW PROCESS FROM NODE    6010.00 TO NODE    6010.00 IS CODE =    1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =    2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    9.04
RAINFALL INTENSITY(INCH/HR) =    6.47
TOTAL STREAM AREA(ACRES) =    3.10
PEAK FLOW RATE(CFS) AT CONFLUENCE =   11.57

*****
FLOW PROCESS FROM NODE    6008.00 TO NODE    6009.00 IS CODE =   21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =   65.00
UPSTREAM ELEVATION(FEET) =   429.00
DOWNSTREAM ELEVATION(FEET) =   428.00
ELEVATION DIFFERENCE(FEET) =    1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    6.160
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  8.291
SUBAREA RUNOFF(CFS) =    1.01
TOTAL AREA(ACRES) =    0.20  TOTAL RUNOFF(CFS) =    1.01

*****
FLOW PROCESS FROM NODE    6009.00 TO NODE    6010.00 IS CODE =   62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION #  1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) =   428.00  DOWNSTREAM ELEVATION(FEET) =   421.00
STREET LENGTH(FEET) =   155.00  CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =   12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =    7.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =    0.020

```

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.67  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(Feet) = 0.22  
 HALFSTREET FLOOD WIDTH(Feet) = 5.96  
 AVERAGE FLOW VELOCITY(Feet/Sec.) = 3.02  
 PRODUCT OF DEPTH&VELOCITY(Feet\*Feet/Sec.) = 0.68  
 STREET FLOW TRAVEL TIME(Min.) = 0.85 Tc(Min.) = 7.01  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.625  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6200  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.618  
 SUBAREA AREA(ACRES) = 0.70 SUBAREA RUNOFF(CFS) = 3.31  
 TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 4.24

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(Feet) = 0.25 HALFSTREET FLOOD WIDTH(Feet) = 7.43  
 FLOW VELOCITY(Feet/Sec.) = 3.32 DEPTH\*VELOCITY(Feet\*Feet/Sec.) = 0.84  
 LONGEST FLOWPATH FROM NODE 6008.00 TO NODE 6010.00 = 220.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6010.00 TO NODE 6010.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(Min.) = 7.01  
 RAINFALL INTENSITY(INCH/HR) = 7.62  
 TOTAL STREAM AREA(ACRES) = 0.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.24

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (Min.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	11.57	9.04	6.474	3.10
2	4.24	7.01	7.625	0.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (Min.)	INTENSITY (INCH/HOUR)
1	14.07	7.01	7.625
2	15.17	9.04	6.474

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 15.17 Tc(Min.) = 9.04  
 TOTAL AREA(ACRES) = 4.00  
 LONGEST FLOWPATH FROM NODE 6000.00 TO NODE 6010.00 = 820.00 FEET.

Flow Information for Node 6010

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6014.10 TO NODE 6014.20 IS CODE = 21  
\*\*\*\*\*

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .3500

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00

UPSTREAM ELEVATION(FEET) = 422.00

DOWNSTREAM ELEVATION(FEET) = 397.00

ELEVATION DIFFERENCE(FEET) = 25.00

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.431

WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.00

TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 1.00

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6014.20 TO NODE 6015.00 IS CODE = 31  
\*\*\*\*\*

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 397.00 DOWNSTREAM(FEET) = 390.00

FLOW LENGTH(FEET) = 690.00 MANNING'S N = 0.016

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.3 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 3.12

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 1.00

PIPE TRAVEL TIME(MIN.) = 3.68 Tc(MIN.) = 8.11

LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6015.00 = 740.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6014.20 TO NODE 6015.00 IS CODE = 81  
\*\*\*\*\*

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.942

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .2900

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.2978

SUBAREA AREA(ACRES) = 2.00 SUBAREA RUNOFF(CFS) = 4.03

TOTAL AREA(ACRES) = 2.30 TOTAL RUNOFF(CFS) = 4.76

TC(MIN.) = 8.11

```

FLOW PROCESS FROM NODE    6015.00 TO NODE    6019.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   390.00  DOWNSTREAM(FEET) =   345.00
FLOW LENGTH(FEET) =   115.00  MANNING'S N =   0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   3.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   20.84
ESTIMATED PIPE DIAMETER(INCH) =   18.00    NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =         4.76
PIPE TRAVEL TIME(MIN.) =    0.09    Tc(MIN.) =    8.20
LONGEST FLOWPATH FROM NODE    6014.10 TO NODE    6019.00 =   855.00 FEET.

*****
FLOW PROCESS FROM NODE    6019.00 TO NODE    6019.00 IS CODE =   1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    8.20
RAINFALL INTENSITY(INCH/HR) =    6.89
TOTAL STREAM AREA(ACRES) =    2.30
PEAK FLOW RATE(CFS) AT CONFLUENCE =         4.76

*****
FLOW PROCESS FROM NODE    6017.00 TO NODE    6018.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6100
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =    50.00
UPSTREAM ELEVATION(FEET) =    382.00
DOWNSTREAM ELEVATION(FEET) =    357.00
ELEVATION DIFFERENCE(FEET) =    25.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    2.895
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) =         1.16
TOTAL AREA(ACRES) =         0.20  TOTAL RUNOFF(CFS) =         1.16

*****
FLOW PROCESS FROM NODE    6018.00 TO NODE    6019.00 IS CODE =  31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    357.00  DOWNSTREAM(FEET) =    350.00
FLOW LENGTH(FEET) =    675.00  MANNING'S N =   0.016
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN  18.0 INCH PIPE IS   4.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    3.29

```

ESTIMATED PIPE DIAMETER(INCH) = 18.00      NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.16  
 PIPE TRAVEL TIME(MIN.) = 3.42      Tc(MIN.) = 6.32  
 LONGEST FLOWPATH FROM NODE 6017.00 TO NODE 6019.00 = 725.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6018.00 TO NODE 6019.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.158  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .2900  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3178  
 SUBAREA AREA(ACRES) = 2.10      SUBAREA RUNOFF(CFS) = 4.97  
 TOTAL AREA(ACRES) = 2.30      TOTAL RUNOFF(CFS) = 5.96  
 TC(MIN.) = 6.32

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6019.00 TO NODE 6019.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.32  
 RAINFALL INTENSITY(INCH/HR) = 8.16  
 TOTAL STREAM AREA(ACRES) = 2.30  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.96

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.76	8.20	6.891	2.30
2	5.96	6.32	8.158	2.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	9.62	6.32	8.158
2	9.79	8.20	6.891

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.79      Tc(MIN.) = 8.20  
 TOTAL AREA(ACRES) = 4.60  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6019.00 = 855.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6019.00 TO NODE 6030.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 340.00 DOWNSTREAM(FEET) = 309.00
FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.01
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 9.79
PIPE TRAVEL TIME(MIN.) = 0.24 Tc(MIN.) = 8.45
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6030.00 = 1105.00 FEET.

*****
FLOW PROCESS FROM NODE 6030.00 TO NODE 6030.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.45
RAINFALL INTENSITY(INCH/HR) = 6.76
TOTAL STREAM AREA(ACRES) = 4.60
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.79

*****
FLOW PROCESS FROM NODE 6021.00 TO NODE 6022.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00
UPSTREAM ELEVATION(FEET) = 355.00
DOWNSTREAM ELEVATION(FEET) = 320.50
ELEVATION DIFFERENCE(FEET) = 34.50
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.593
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.824
SUBAREA RUNOFF(CFS) = 0.79
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.79

*****
FLOW PROCESS FROM NODE 6022.00 TO NODE 6030.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 320.50 DOWNSTREAM ELEVATION(FEET) = 319.00
STREET LENGTH(FEET) = 150.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

```

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.54  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.27  
HALFSTREET FLOOD WIDTH(FEET) = 8.25  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.65  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.45  
STREET FLOW TRAVEL TIME(MIN.) = 1.51 Tc(MIN.) = 7.10  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.562  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7800  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.620  
SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 3.54  
TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 4.22

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 10.22  
FLOW VELOCITY(FEET/SEC.) = 1.86 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.58  
LONGEST FLOWPATH FROM NODE 6021.00 TO NODE 6030.00 = 220.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6030.00 TO NODE 6030.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2	
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	7.10
RAINFALL INTENSITY(INCH/HR) =	7.56
TOTAL STREAM AREA(ACRES) =	0.90
PEAK FLOW RATE(CFS) AT CONFLUENCE =	4.22

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.79	8.45	6.762	4.60
2	4.22	7.10	7.562	0.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	12.98	7.10	7.562
2	13.57	8.45	6.762

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 13.57 Tc(MIN.) = 8.45  
TOTAL AREA(ACRES) = 5.50  
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6030.00 = 1105.00 FEET.

\*\*\*\*\*



```

FLOW PROCESS FROM NODE    6030.00 TO NODE    6030.00 IS CODE =   10
-----
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<
=====

+-----+
| Flow Information for node 5086 |
+-----+

*****
FLOW PROCESS FROM NODE    5086.00 TO NODE    5086.00 IS CODE =    7
-----
>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<
=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN) =    5.63    RAIN INTENSITY(INCH/HOUR) =    8.79
TOTAL AREA(ACRES) =    1.60    TOTAL RUNOFF(CFS) =    10.82

*****
FLOW PROCESS FROM NODE    5086.00 TO NODE    6026.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) =    323.50 DOWNSTREAM( FEET) =    319.00
FLOW LENGTH( FEET) =    500.00    MANNING'S N =    0.013
DEPTH OF FLOW IN  21.0 INCH PIPE IS  13.7 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) =    6.53
ESTIMATED PIPE DIAMETER( INCH) =    21.00    NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =    10.82
PIPE TRAVEL TIME(MIN.) =    1.28    Tc(MIN.) =    6.91
LONGEST FLOWPATH FROM NODE    6014.10 TO NODE    6026.00 =  1605.00 FEET.

*****
FLOW PROCESS FROM NODE    6026.00 TO NODE    6026.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =    3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =    6.91
RAINFALL INTENSITY(INCH/HR) =    7.70
TOTAL STREAM AREA(ACRES) =    1.60
PEAK FLOW RATE(CFS) AT CONFLUENCE =    10.82

+-----+
| Flow Information for node 6026 |
+-----+

*****
FLOW PROCESS FROM NODE    6026.00 TO NODE    6026.00 IS CODE =    7
-----
>>>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<

```

```

=====
USER-SPECIFIED VALUES ARE AS FOLLOWS:
TC(MIN) = 10.20    RAIN INTENSITY(INCH/HOUR) = 5.99
TOTAL AREA(ACRES) = 14.00    TOTAL RUNOFF(CFS) = 34.50

*****
FLOW PROCESS FROM NODE 6026.00 TO NODE 6026.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.20
RAINFALL INTENSITY(INCH/HR) = 5.99
TOTAL STREAM AREA(ACRES) = 14.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 34.50

*****
FLOW PROCESS FROM NODE 6024.00 TO NODE 6025.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 322.50
DOWNSTREAM ELEVATION(FEET) = 321.50
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.148
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.46
TOTAL AREA(ACRES) = 0.20    TOTAL RUNOFF(CFS) = 1.46

*****
FLOW PROCESS FROM NODE 6025.00 TO NODE 6026.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 321.50    DOWNSTREAM ELEVATION(FEET) = 319.00
STREET LENGTH(FEET) = 190.00    CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.64
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.34

```

HALFSTREET FLOOD WIDTH (FEET) = 11.64  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 2.30  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.78  
 STREET FLOW TRAVEL TIME (MIN.) = 1.38 Tc (MIN.) = 5.52  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 8.894  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6800  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.689  
 SUBAREA AREA (ACRES) = 1.70 SUBAREA RUNOFF (CFS) = 10.28  
 TOTAL AREA (ACRES) = 1.90 PEAK FLOW RATE (CFS) = 11.65

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.39 HALFSTREET FLOOD WIDTH (FEET) = 12.00  
 FLOW VELOCITY (FEET/SEC.) = 2.85 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.11  
 LONGEST FLOWPATH FROM NODE 6024.00 TO NODE 6026.00 = 255.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6026.00 TO NODE 6026.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====  
 TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION (MIN.) = 5.52  
 RAINFALL INTENSITY (INCH/HR) = 8.89  
 TOTAL STREAM AREA (ACRES) = 1.90  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 11.65

# \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	10.82	6.91	7.702	1.60
2	34.50	10.20	5.989	14.00
3	11.65	5.52	8.894	1.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

# \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	38.99	5.52	8.894
2	44.27	6.91	7.702
3	50.76	10.20	5.989

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 50.76 Tc (MIN.) = 10.20  
 TOTAL AREA (ACRES) = 17.50  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6026.00 = 1605.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6026.00 TO NODE 6030.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 311.00 DOWNSTREAM(FEET) = 309.00
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 33.0 INCH PIPE IS 24.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.69
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 50.76
PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 10.45
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6030.00 = 1765.00 FEET.

*****
FLOW PROCESS FROM NODE 6030.00 TO NODE 6030.00 IS CODE = 11
-----
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<
=====

** MAIN STREAM CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 50.76 10.45 5.896 17.50
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6030.00 = 1765.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)
1 13.57 8.45 6.762 5.50
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6030.00 = 1105.00 FEET.

** PEAK FLOW RATE TABLE **
STREAM RUNOFF Tc INTENSITY
NUMBER (CFS) (MIN.) (INCH/HOUR)
1 54.61 8.45 6.762
2 62.59 10.45 5.896

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 62.59 Tc(MIN.) = 10.45
TOTAL AREA(ACRES) = 23.00

*****
FLOW PROCESS FROM NODE 6030.00 TO NODE 6030.00 IS CODE = 12
-----
>>>>CLEAR MEMORY BANK # 1 <<<<
=====

*****
FLOW PROCESS FROM NODE 6030.00 TO NODE 6034.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 309.00 DOWNSTREAM(FEET) = 307.50
FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 36.0 INCH PIPE IS 28.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.55
ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 62.59
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 10.67

```

```

LONGEST FLOWPATH FROM NODE    6014.10 TO NODE    6034.00 = 1905.00 FEET.

*****
FLOW PROCESS FROM NODE    6034.00 TO NODE    6034.00 IS CODE =    1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 10.67
RAINFALL INTENSITY(INCH/HR) = 5.82
TOTAL STREAM AREA(ACRES) = 23.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 62.59

*****
FLOW PROCESS FROM NODE    6032.00 TO NODE    6033.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 40.00
UPSTREAM ELEVATION(FEET) = 348.00
DOWNSTREAM ELEVATION(FEET) = 328.00
ELEVATION DIFFERENCE(FEET) = 20.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.228
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 0.57
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.57

*****
FLOW PROCESS FROM NODE    6033.00 TO NODE    6034.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 319.00 DOWNSTREAM ELEVATION(FEET) = 317.50
STREET LENGTH(FEET) = 120.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.28
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.25
HALFSTREET FLOOD WIDTH(FEET) = 7.49
AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.77

```

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.45  
 STREET FLOW TRAVEL TIME(MIN.) = 1.13 Tc(MIN.) = 5.36  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.069  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.636  
 SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 3.49  
 TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 4.04

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.30 HALFSTREET FLOOD WIDTH(FEET) = 9.57  
 FLOW VELOCITY(FEET/SEC.) = 2.01 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.60  
 LONGEST FLOWPATH FROM NODE 6032.00 TO NODE 6034.00 = 160.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6034.00 TO NODE 6034.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.36  
 RAINFALL INTENSITY(INCH/HR) = 9.07  
 TOTAL STREAM AREA(ACRES) = 0.70  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.04

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	62.59	10.67	5.817	23.00
2	4.04	5.36	9.069	0.70

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	35.48	5.36	9.069
2	65.18	10.67	5.817

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE(CFS) = 65.18 Tc(MIN.) = 10.67  
 TOTAL AREA(ACRES) = 23.70  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6034.00 = 1905.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6034.00 TO NODE 6034.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 307.50 DOWNSTREAM(FEET) = 305.50  
 FLOW LENGTH(FEET) = 175.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 28.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 10.90  
 ESTIMATED PIPE DIAMETER(INCH) = 36.00      NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 65.18  
 PIPE TRAVEL TIME(MIN.) = 0.27      Tc(MIN.) = 10.94  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6034.50 = 2080.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6034.50 TO NODE 6034.50 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.94  
 RAINFALL INTENSITY(INCH/HR) = 5.72  
 TOTAL STREAM AREA(ACRES) = 23.70  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 65.18

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6036.00 TO NODE 6037.00 IS CODE = 21

-----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 =====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 319.00  
 DOWNSTREAM ELEVATION(FEET) = 318.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.148  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.46  
 TOTAL AREA(ACRES) = 0.20      TOTAL RUNOFF(CFS) = 1.46

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6037.00 TO NODE 6034.50 IS CODE = 62

-----  
 >>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<  
 =====

UPSTREAM ELEVATION(FEET) = 318.00      DOWNSTREAM ELEVATION(FEET) = 313.50  
 STREET LENGTH(FEET) = 100.00      CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.48  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH (FEET) = 0.27  
 HALFSTREET FLOOD WIDTH (FEET) = 8.31  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 3.53  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.96  
 STREET FLOW TRAVEL TIME (MIN.) = 0.47 Tc (MIN.) = 4.62  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA (ACRES) = 1.10 SUBAREA RUNOFF (CFS) = 8.03  
 TOTAL AREA (ACRES) = 1.30 PEAK FLOW RATE (CFS) = 9.49

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.31 HALFSTREET FLOOD WIDTH (FEET) = 10.50  
 FLOW VELOCITY (FEET/SEC.) = 4.00 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.26  
 LONGEST FLOWPATH FROM NODE 6036.00 TO NODE 6034.50 = 165.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6034.50 TO NODE 6034.50 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 4.62  
 RAINFALL INTENSITY (INCH/HR) = 9.49  
 TOTAL STREAM AREA (ACRES) = 1.30  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 9.49

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	65.18	10.94	5.725	23.70
2	9.49	4.62	9.485	1.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	48.83	4.62	9.485
2	70.91	10.94	5.725

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 70.91 Tc (MIN.) = 10.94  
 TOTAL AREA (ACRES) = 25.00  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6034.50 = 2080.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6034.50 TO NODE 6066.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<



```

=====
ELEVATION DATA: UPSTREAM( FEET) = 305.50 DOWNSTREAM( FEET) = 303.50
FLOW LENGTH( FEET) = 175.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 39.0 INCH PIPE IS 27.5 INCHES
PIPE-FLOW VELOCITY( FEET/SEC.) = 11.35
ESTIMATED PIPE DIAMETER( INCH) = 39.00 NUMBER OF PIPES = 1
PIPE-FLOW( CFS) = 70.91
PIPE TRAVEL TIME( MIN.) = 0.26 Tc( MIN.) = 11.20
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6066.00 = 2255.00 FEET.

*****
FLOW PROCESS FROM NODE 6066.00 TO NODE 6066.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION( MIN.) = 11.20
RAINFALL INTENSITY( INCH/HR) = 5.64
TOTAL STREAM AREA( ACRES) = 25.00
PEAK FLOW RATE( CFS) AT CONFLUENCE = 70.91

*****
FLOW PROCESS FROM NODE 6038.00 TO NODE 6039.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED( SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .6700
S.C.S. CURVE NUMBER ( AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH( FEET) = 65.00
UPSTREAM ELEVATION( FEET) = 316.00
DOWNSTREAM ELEVATION( FEET) = 315.00
ELEVATION DIFFERENCE( FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW( MIN.) = 5.406
100 YEAR RAINFALL INTENSITY( INCH/HOUR) = 9.020
SUBAREA RUNOFF( CFS) = 1.21
TOTAL AREA( ACRES) = 0.20 TOTAL RUNOFF( CFS) = 1.21

*****
FLOW PROCESS FROM NODE 6039.00 TO NODE 6066.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>( STREET TABLE SECTION # 1 USED) <<<<
=====
UPSTREAM ELEVATION( FEET) = 315.00 DOWNSTREAM ELEVATION( FEET) = 313.50
STREET LENGTH( FEET) = 260.00 CURB HEIGHT( INCHES) = 6.0
STREET HALFWIDTH( FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK( FEET) = 7.00
INSIDE STREET CROSSFALL( DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL( DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL( DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section( curb-to-curb) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

```

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.12  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH( FEET) = 0.33  
 HALFSTREET FLOOD WIDTH( FEET) = 11.32  
 AVERAGE FLOW VELOCITY( FEET/SEC.) = 1.51  
 PRODUCT OF DEPTH&VELOCITY( FT\*FT/SEC.) = 0.50  
 STREET FLOW TRAVEL TIME( MIN.) = 2.88 Tc( MIN.) = 8.28  
 100 YEAR RAINFALL INTENSITY( INCH/HOUR) = 6.850  
 \*USER SPECIFIED( SUBAREA) :  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.755  
 SUBAREA AREA( ACRES) = 1.10 SUBAREA RUNOFF( CFS) = 5.80  
 TOTAL AREA( ACRES) = 1.30 PEAK FLOW RATE( CFS) = 6.72

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH( FEET) = 0.37 HALFSTREET FLOOD WIDTH( FEET) = 12.00  
 FLOW VELOCITY( FEET/SEC.) = 1.78 DEPTH\*VELOCITY( FT\*FT/SEC.) = 0.67  
 LONGEST FLOWPATH FROM NODE 6038.00 TO NODE 6066.00 = 325.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6066.00 TO NODE 6066.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION( MIN.) = 8.28  
 RAINFALL INTENSITY( INCH/HR) = 6.85  
 TOTAL STREAM AREA( ACRES) = 1.30  
 PEAK FLOW RATE( CFS) AT CONFLUENCE = 6.72

# \*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	70.91	11.20	5.640	25.00
2	6.72	8.28	6.850	1.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

# \*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	65.09	8.28	6.850
2	76.44	11.20	5.640

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE( CFS) = 76.44 Tc( MIN.) = 11.20  
 TOTAL AREA( ACRES) = 26.30  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6066.00 = 2255.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6066.00 TO NODE 6066.00 IS CODE = 10

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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE    6040.00 TO NODE    6041.00 IS CODE =  21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) =  0
INITIAL SUBAREA FLOW-LENGTH(FEET) =  50.00
UPSTREAM ELEVATION(FEET) =  348.00
DOWNSTREAM ELEVATION(FEET) =  323.00
ELEVATION DIFFERENCE(FEET) =  25.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =  5.022
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  9.458
SUBAREA RUNOFF(CFS) =  0.47
TOTAL AREA(ACRES) =  0.20  TOTAL RUNOFF(CFS) =  0.47

*****
FLOW PROCESS FROM NODE    6041.00 TO NODE    6044.00 IS CODE =  62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION #  1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) =  322.50  DOWNSTREAM ELEVATION(FEET) =  321.00
STREET LENGTH(FEET) =  160.00  CURB HEIGHT(INCHES) =  6.0
STREET HALFWIDTH(FEET) =  12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =  7.00
INSIDE STREET CROSSFALL(DECIMAL) =  0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =  0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =  2
STREET PARKWAY CROSSFALL(DECIMAL) =  0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =  0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =  0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =  2.27
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =  0.26
HALFSTREET FLOOD WIDTH(FEET) =  7.98
AVERAGE FLOW VELOCITY(FEET/SEC.) =  1.57
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =  0.42
STREET FLOW TRAVEL TIME(MIN.) =  1.70  Tc(MIN.) =  6.72
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =  7.839
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6700
S.C.S. CURVE NUMBER (AMC II) =  0
AREA-AVERAGE RUNOFF COEFFICIENT =  0.577
SUBAREA AREA(ACRES) =  0.70  SUBAREA RUNOFF(CFS) =  3.68
TOTAL AREA(ACRES) =  0.90  PEAK FLOW RATE(CFS) =  4.07

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =  0.31  HALFSTREET FLOOD WIDTH(FEET) =  10.22

```

FLOW VELOCITY (FEET/SEC.) = 1.80 DEPTH\*VELOCITY (FT\*FT/SEC.) = 0.56  
LONGEST FLOWPATH FROM NODE 6040.00 TO NODE 6044.00 = 210.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6044.00 TO NODE 6044.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION (MIN.) =	6.72
RAINFALL INTENSITY (INCH/HR) =	7.84
TOTAL STREAM AREA (ACRES) =	0.90
PEAK FLOW RATE (CFS) AT CONFLUENCE =	4.07

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6042.00 TO NODE 6043.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED (SUBAREA) :

USER-SPECIFIED RUNOFF COEFFICIENT =	.6700
S.C.S. CURVE NUMBER (AMC II) =	0
INITIAL SUBAREA FLOW-LENGTH (FEET) =	65.00
UPSTREAM ELEVATION (FEET) =	325.00
DOWNSTREAM ELEVATION (FEET) =	324.00
ELEVATION DIFFERENCE (FEET) =	1.00
SUBAREA OVERLAND TIME OF FLOW (MIN.) =	5.406
100 YEAR RAINFALL INTENSITY (INCH/HOUR) =	9.020
SUBAREA RUNOFF (CFS) =	1.81
TOTAL AREA (ACRES) =	0.30
TOTAL RUNOFF (CFS) =	1.81

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6043.00 TO NODE 6044.00 IS CODE = 62

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION (FEET) =	324.00	DOWNSTREAM ELEVATION (FEET) =	321.00
STREET LENGTH (FEET) =	200.00	CURB HEIGHT (INCHES) =	6.0
STREET HALFWIDTH (FEET) =	12.00		

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) =	7.00
INSIDE STREET CROSSFALL (DECIMAL) =	0.020
OUTSIDE STREET CROSSFALL (DECIMAL) =	0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =	2
STREET PARKWAY CROSSFALL (DECIMAL) =	0.020
Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) =	0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =	0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) =	3.61
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:	
STREET FLOW DEPTH (FEET) =	0.28
HALFSTREET FLOOD WIDTH (FEET) =	8.80
AVERAGE FLOW VELOCITY (FEET/SEC.) =	2.10
PRODUCT OF DEPTH&VELOCITY (FT*FT/SEC.) =	0.59

STREET FLOW TRAVEL TIME(MIN.) = 1.59 Tc(MIN.) = 7.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.638  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.670  
 SUBAREA AREA(ACRES) = 0.70 SUBAREA RUNOFF(CFS) = 3.58  
 TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 5.12

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(Feet) = 0.31 HALFSTREET FLOOD WIDTH(Feet) = 10.17  
 FLOW VELOCITY(Feet/Sec.) = 2.28 DEPTH\*VELOCITY(Ft\*Ft/Sec.) = 0.70  
 LONGEST FLOWPATH FROM NODE 6042.00 TO NODE 6044.00 = 265.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6044.00 TO NODE 6044.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2				
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:				
TIME OF CONCENTRATION(MIN.) = 7.00				
RAINFALL INTENSITY(INCH/HR) = 7.64				
TOTAL STREAM AREA(ACRES) = 1.00				
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.12				

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.07	6.72	7.839	0.90
2	5.12	7.00	7.638	1.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	8.98	6.72	7.839
2	9.08	7.00	7.638

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 9.08 Tc(MIN.) = 7.00  
 TOTAL AREA(ACRES) = 1.90  
 LONGEST FLOWPATH FROM NODE 6042.00 TO NODE 6044.00 = 265.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6044.00 TO NODE 6058.20 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(Feet) = 313.00		DOWNSTREAM(Feet) = 310.00	
FLOW LENGTH(Feet) = 320.00		MANNING'S N = 0.013	
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.9 INCHES			
PIPE-FLOW VELOCITY(Feet/Sec.) = 6.21			

ESTIMATED PIPE DIAMETER(INCH) = 18.00      NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 9.08  
 PIPE TRAVEL TIME(MIN.) = 0.86      Tc(MIN.) = 7.85  
 LONGEST FLOWPATH FROM NODE 6042.00 TO NODE 6058.20 = 585.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6058.20 TO NODE 6058.20 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.85  
 RAINFALL INTENSITY(INCH/HR) = 7.09  
 TOTAL STREAM AREA(ACRES) = 1.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.08

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6047.00 TO NODE 6048.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 322.50  
 DOWNSTREAM ELEVATION(FEET) = 321.50  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.406  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.020  
 SUBAREA RUNOFF(CFS) = 1.21  
 TOTAL AREA(ACRES) = 0.20      TOTAL RUNOFF(CFS) = 1.21

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6048.00 TO NODE 6058.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 321.50      DOWNSTREAM ELEVATION(FEET) = 318.00  
 STREET LENGTH(FEET) = 360.00      CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.39  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.33  
 HALFSTREET FLOOD WIDTH(FEET) = 11.37

AVERAGE FLOW VELOCITY (FEET/SEC.) = 1.95  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.65  
 STREET FLOW TRAVEL TIME (MIN.) = 3.07 Tc (MIN.) = 8.48  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.748  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.759  
 SUBAREA AREA (ACRES) = 1.60 SUBAREA RUNOFF (CFS) = 8.31  
 TOTAL AREA (ACRES) = 1.80 PEAK FLOW RATE (CFS) = 9.22

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.38 HALFSTREET FLOOD WIDTH (FEET) = 12.00  
 FLOW VELOCITY (FEET/SEC.) = 2.37 DEPTH\*VELOCITY (FT\*FT/SEC.) = 0.90  
 LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6058.00 = 425.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6058.20 TO NODE 6058.20 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 8.48  
 RAINFALL INTENSITY (INCH/HR) = 6.75  
 TOTAL STREAM AREA (ACRES) = 1.80  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 9.22

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.08	7.85	7.088	1.90
2	9.22	8.48	6.748	1.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	17.62	7.85	7.088
2	17.86	8.48	6.748

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 17.86 Tc (MIN.) = 8.48  
 TOTAL AREA (ACRES) = 3.70  
 LONGEST FLOWPATH FROM NODE 6042.00 TO NODE 6058.20 = 585.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6058.20 TO NODE 6058.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 310.00 DOWNSTREAM (FEET) = 308.00  
 FLOW LENGTH (FEET) = 100.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.7 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 9.92  
 ESTIMATED PIPE DIAMETER (INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 17.86  
 PIPE TRAVEL TIME (MIN.) = 0.17 Tc (MIN.) = 8.64  
 LONGEST FLOWPATH FROM NODE 6042.00 TO NODE 6058.00 = 685.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6058.00 TO NODE 6058.00 IS CODE = 10  
 -----  
 >>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6049.00 TO NODE 6050.00 IS CODE = 21  
 -----  
 >>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
 =====

\*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 35.00  
 UPSTREAM ELEVATION (FEET) = 322.50  
 DOWNSTREAM ELEVATION (FEET) = 321.50  
 ELEVATION DIFFERENCE (FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 3.227  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF (CFS) = 3.81  
 TOTAL AREA (ACRES) = 0.60 TOTAL RUNOFF (CFS) = 3.81

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6050.00 TO NODE 6050.00 IS CODE = 1  
 -----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 3.23  
 RAINFALL INTENSITY (INCH/HR) = 9.49  
 TOTAL STREAM AREA (ACRES) = 0.60  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 3.81

+-----+  
 | Flow Information for node 5090.5 |  
 | |  
 | |  
 +-----+

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 5090.50 TO NODE 5090.50 IS CODE = 7  
 -----  
 >>>>USER SPECIFIED HYDROLOGY INFORMATION AT NODE<<<<<  
 =====

USER-SPECIFIED VALUES ARE AS FOLLOWS:  
 TC (MIN) = 6.63 RAIN INTENSITY (INCH/HOUR) = 7.91  
 TOTAL AREA (ACRES) = 70.70 TOTAL RUNOFF (CFS) = 173.26



```
*****
FLOW PROCESS FROM NODE    6090.50 TO NODE    6050.00 IS CODE =   31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
```

```
ELEVATION DATA: UPSTREAM(FEET) =   312.00 DOWNSTREAM(FEET) =   311.50
FLOW LENGTH(FEET) =   50.00 MANNING'S N =   0.013
DEPTH OF FLOW IN  54.0 INCH PIPE IS  41.1 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   13.35
ESTIMATED PIPE DIAMETER(INCH) =   54.00 NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =   173.26
PIPE TRAVEL TIME(MIN.) =    0.06 Tc(MIN.) =    6.69
LONGEST FLOWPATH FROM NODE    6047.00 TO NODE    6050.00 =   475.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE    6050.00 TO NODE    6050.00 IS CODE =    1
-----
```

```
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
```

```
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) =    6.69
RAINFALL INTENSITY(INCH/HR) =    7.86
TOTAL STREAM AREA(ACRES) =    70.70
PEAK FLOW RATE(CFS) AT CONFLUENCE =   173.26
```

**\*\* CONFLUENCE DATA \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	3.81	3.23	9.485	0.60
2	173.26	6.69	7.859	70.70

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

**\*\* PEAK FLOW RATE TABLE \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	87.36	3.23	9.485
2	176.42	6.69	7.859

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```
PEAK FLOW RATE(CFS) =   176.42 Tc(MIN.) =    6.69
TOTAL AREA(ACRES) =    71.30
LONGEST FLOWPATH FROM NODE    6047.00 TO NODE    6050.00 =   475.00 FEET.
```

```
*****
FLOW PROCESS FROM NODE    6050.00 TO NODE    6053.00 IS CODE =   31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
```

```
ELEVATION DATA: UPSTREAM(FEET) =   311.50 DOWNSTREAM(FEET) =   310.80
FLOW LENGTH(FEET) =   100.00 MANNING'S N =   0.013
```

DEPTH OF FLOW IN 57.0 INCH PIPE IS 45.6 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 11.60  
 ESTIMATED PIPE DIAMETER (INCH) = 57.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 176.42  
 PIPE TRAVEL TIME (MIN.) = 0.14 Tc (MIN.) = 6.84  
 LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6053.00 = 575.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6053.00 TO NODE 6053.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 6.84  
 RAINFALL INTENSITY (INCH/HR) = 7.75  
 TOTAL STREAM AREA (ACRES) = 71.30  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 176.42

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6052.00 TO NODE 6053.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH (FEET) = 65.00  
 UPSTREAM ELEVATION (FEET) = 321.80  
 DOWNSTREAM ELEVATION (FEET) = 320.80  
 ELEVATION DIFFERENCE (FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 4.148  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF (CFS) = 4.38  
 TOTAL AREA (ACRES) = 0.60 TOTAL RUNOFF (CFS) = 4.38

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6053.00 TO NODE 6053.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 4.15  
 RAINFALL INTENSITY (INCH/HR) = 9.49  
 TOTAL STREAM AREA (ACRES) = 0.60  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 4.38

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	176.42	6.84	7.752	71.30
2	4.38	4.15	9.485	0.60

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

**\*\* PEAK FLOW RATE TABLE \*\***

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	148.57	4.15	9.485
2	180.00	6.84	7.752

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 180.00 Tc (MIN.) = 6.84

TOTAL AREA (ACRES) = 71.90

LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6053.00 = 575.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 6053.00 TO NODE 5057.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 310.80 DOWNSTREAM (FEET) = 309.20

FLOW LENGTH (FEET) = 170.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 54.0 INCH PIPE IS 44.0 INCHES

PIPE-FLOW VELOCITY (FEET/SEC.) = 12.97

ESTIMATED PIPE DIAMETER (INCH) = 54.00 NUMBER OF PIPES = 1

PIPE-FLOW (CFS) = 180.00

PIPE TRAVEL TIME (MIN.) = 0.22 Tc (MIN.) = 7.05

LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 5057.00 = 745.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 6057.00 TO NODE 6057.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION (MIN.) = 7.05

RAINFALL INTENSITY (INCH/HR) = 7.60

TOTAL STREAM AREA (ACRES) = 71.90

PEAK FLOW RATE (CFS) AT CONFLUENCE = 180.00

\*\*\*\*\*

FLOW PROCESS FROM NODE 6056.00 TO NODE 6057.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 65.00

UPSTREAM ELEVATION (FEET) = 320.20

DOWNSTREAM ELEVATION (FEET) = 319.20

ELEVATION DIFFERENCE (FEET) = 1.00

SUBAREA OVERLAND TIME OF FLOW (MIN.) = 4.148

100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF (CFS) = 3.65

TOTAL AREA (ACRES) = 0.50 TOTAL RUNOFF (CFS) = 3.65

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6057.00 TO NODE 6057.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 4.15  
 RAINFALL INTENSITY(INCH/HR) = 9.49  
 TOTAL STREAM AREA(ACRES) = 0.50  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.65

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	180.00	7.05	7.596	71.90
2	3.65	4.15	9.485	0.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	147.81	4.15	9.485
2	182.93	7.05	7.596

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 182.93 Tc(MIN.) = 7.05  
 TOTAL AREA(ACRES) = 72.40  
 LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6057.00 = 745.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6057.00 TO NODE 6058.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 309.20 DOWNSTREAM(FEET) = 308.00  
 FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 57.0 INCH PIPE IS 41.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.19  
 ESTIMATED PIPE DIAMETER(INCH) = 57.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 182.93  
 PIPE TRAVEL TIME(MIN.) = 0.16 Tc(MIN.) = 7.22  
 LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6058.00 = 875.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6058.00 TO NODE 6058.00 IS CODE = 11  
 -----

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM	RUNOFF	Tc	INTENSITY	AREA
--------	--------	----	-----------	------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	182.93	7.22	7.485	72.40

LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6058.00 = 875.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	17.86	8.64	6.663	3.70

LONGEST FLOWPATH FROM NODE 6042.00 TO NODE 6058.00 = 685.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	197.84	7.22	7.485
2	180.72	8.64	6.663

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 197.84 Tc(MIN.) = 7.22  
TOTAL AREA(ACRES) = 76.10

\*\*\*\*\*

FLOW PROCESS FROM NODE 6058.00 TO NODE 6058.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<

=====

\*\*\*\*\*

FLOW PROCESS FROM NODE 6058.00 TO NODE 6065.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM( FEET) = 308.00 DOWNSTREAM( FEET) = 305.20

FLOW LENGTH( FEET) = 265.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 57.0 INCH PIPE IS 42.0 INCHES

PIPE-FLOW VELOCITY( FEET/SEC.) = 14.13

ESTIMATED PIPE DIAMETER( INCH) = 57.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 197.84

PIPE TRAVEL TIME(MIN.) = 0.31 Tc(MIN.) = 7.53

LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6065.00 = 1140.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 6065.00 TO NODE 6065.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.53

RAINFALL INTENSITY(INCH/HR) = 7.28

TOTAL STREAM AREA(ACRES) = 76.10

PEAK FLOW RATE(CFS) AT CONFLUENCE = 197.84

\*\*\*\*\*

FLOW PROCESS FROM NODE 6059.00 TO NODE 6060.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

```

=====
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 319.20
DOWNSTREAM ELEVATION(FEET) = 318.20
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.148
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 2.19
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 2.19

*****
FLOW PROCESS FROM NODE 6060.00 TO NODE 6065.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 318.20 DOWNSTREAM ELEVATION(FEET) = 315.20
STREET LENGTH(FEET) = 320.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.43
***STREET FLOWING FULL***
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.36
HALFSTREET FLOOD WIDTH(FEET) = 12.00
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.15
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.78
STREET FLOW TRAVEL TIME(MIN.) = 2.48 Tc(MIN.) = 6.62
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.912
*USER SPECIFIED(SUBAREA) :
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.770
SUBAREA AREA(ACRES) = 1.70 SUBAREA RUNOFF(CFS) = 10.36
TOTAL AREA(ACRES) = 2.00 PEAK FLOW RATE(CFS) = 12.18

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.41 HALFSTREET FLOOD WIDTH(FEET) = 12.00
FLOW VELOCITY(FEET/SEC.) = 2.62 DEPTH*VELOCITY(FT*FT/SEC.) = 1.08
LONGEST FLOWPATH FROM NODE 6059.00 TO NODE 6065.00 = 385.00 FEET.

*****
FLOW PROCESS FROM NODE 6065.00 TO NODE 6065.00 IS CODE = 1
-----

```

```

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.62
RAINFALL INTENSITY(INCH/HR) = 7.91
TOTAL STREAM AREA(ACRES) = 2.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.18

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/HR)      (ACRE)
    1      197.84      7.53      7.283      76.10
    2       12.18      6.62      7.912       2.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/HR)
    1      186.18      6.62      7.912
    2      209.06      7.53      7.283

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 209.06 Tc(MIN.) = 7.53
TOTAL AREA(ACRES) = 78.10
LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6065.00 = 1140.00 FEET.

*****
FLOW PROCESS FROM NODE 6065.00 TO NODE 6065.00 IS CODE = 10
-----
>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<
=====

*****
FLOW PROCESS FROM NODE 6061.00 TO NODE 6062.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 319.20
DOWNSTREAM ELEVATION(FEET) = 318.20
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.148
100 YEAR RAINFALL INTENSITY(INCH/HR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.46
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.46

*****
FLOW PROCESS FROM NODE 6062.00 TO NODE 6065.00 IS CODE = 62
-----

```

```

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 318.20 DOWNSTREAM ELEVATION(FEET) = 315.20
STREET LENGTH(FEET) = 245.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curb) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.35
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 10.82
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.13
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.68
STREET FLOW TRAVEL TIME(MIN.) = 1.92 Tc(MIN.) = 6.07
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.370
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.770
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 7.73
TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 9.02

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 12.00
FLOW VELOCITY(FEET/SEC.) = 2.51 DEPTH*VELOCITY(FT*FT/SEC.) = 0.92
LONGEST FLOWPATH FROM NODE 6061.00 TO NODE 6065.00 = 310.00 FEET.

*****
FLOW PROCESS FROM NODE 6065.00 TO NODE 6065.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
-----
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.07
RAINFALL INTENSITY(INCH/HR) = 8.37
TOTAL STREAM AREA(ACRES) = 1.40
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.02

*****
FLOW PROCESS FROM NODE 6063.00 TO NODE 6064.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
-----
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00

```



UPSTREAM ELEVATION(FEET) = 318.00  
 DOWNSTREAM ELEVATION(FEET) = 317.00  
 ELEVATION DIFFERENCE(FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.406  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.020  
 SUBAREA RUNOFF(CFS) = 3.02  
 TOTAL AREA(ACRES) = 0.50 TOTAL RUNOFF(CFS) = 3.02

\*\*\*\*\*

FLOW PROCESS FROM NODE 6064.00 TO NODE 6065.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 317.00 DOWNSTREAM(FEET) = 305.20  
 FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.1 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.12  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 3.02  
 PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 5.67  
 LONGEST FLOWPATH FROM NODE 6063.00 TO NODE 6065.00 = 225.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 6065.00 TO NODE 6065.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.67  
 RAINFALL INTENSITY(INCH/HR) = 8.75  
 TOTAL STREAM AREA(ACRES) = 0.50  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 3.02

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	9.02	6.07	8.370	1.40
2	3.02	5.67	8.747	0.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.45	5.67	8.747
2	11.91	6.07	8.370

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.91 Tc(MIN.) = 6.07

TOTAL AREA(ACRES) = 1.90

LONGEST FLOWPATH FROM NODE 6061.00 TO NODE 6065.00 = 310.00 FEET.

```
*****
FLOW PROCESS FROM NODE 6065.00 TO NODE 6065.00 IS CODE = 11
-----
```

```
>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<
=====
```

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	11.91	6.07	8.370	1.90

LONGEST FLOWPATH FROM NODE 6061.00 TO NODE 6065.00 = 310.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	209.06	7.53	7.283	78.10

LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6065.00 = 1140.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	180.41	6.07	8.370
2	219.43	7.53	7.283

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 219.43 Tc(MIN.) = 7.53  
TOTAL AREA(ACRES) = 80.00

```
*****
FLOW PROCESS FROM NODE 6065.00 TO NODE 6065.00 IS CODE = 12
-----
```

```
>>>>CLEAR MEMORY BANK # 2 <<<<
=====
```

```
*****
FLOW PROCESS FROM NODE 6065.00 TO NODE 6066.00 IS CODE = 31
-----
```

```
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
```

ELEVATION DATA: UPSTREAM( FEET ) = 305.20 DOWNSTREAM( FEET ) = 303.50  
FLOW LENGTH( FEET ) = 160.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 57.0 INCH PIPE IS 46.1 INCHES  
PIPE-FLOW VELOCITY( FEET/SEC. ) = 14.29  
ESTIMATED PIPE DIAMETER( INCH ) = 57.00 NUMBER OF PIPES = 1  
PIPE-FLOW( CFS ) = 219.43  
PIPE TRAVEL TIME( MIN. ) = 0.19 Tc( MIN. ) = 7.72  
LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6066.00 = 1300.00 FEET.

```
*****
FLOW PROCESS FROM NODE 6066.00 TO NODE 6066.00 IS CODE = 11
-----
```

```
>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<
=====
```

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM	RUNOFF	Tc	INTENSITY	AREA
--------	--------	----	-----------	------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)	(ACRE)
1	219.43	7.72	7.169	80.00

LONGEST FLOWPATH FROM NODE 6047.00 TO NODE 6066.00 = 1300.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	76.44	11.20	5.640	26.30

LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6066.00 = 2255.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	272.12	7.72	7.169
2	249.06	11.20	5.640

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
 PEAK FLOW RATE (CFS) = 272.12 Tc (MIN.) = 7.72  
 TOTAL AREA (ACRES) = 106.30

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6066.00 TO NODE 6066.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6066.00 TO NODE 6085.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 303.60 DOWNSTREAM (FEET) = 301.50  
 FLOW LENGTH (FEET) = 170.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 60.0 INCH PIPE IS 48.7 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 15.94  
 ESTIMATED PIPE DIAMETER (INCH) = 60.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 272.12  
 PIPE TRAVEL TIME (MIN.) = 0.18 Tc (MIN.) = 7.90  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6085.00 = 2425.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6085.00 TO NODE 6085.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION (MIN.) = 7.90  
 RAINFALL INTENSITY (INCH/HR) = 7.06  
 TOTAL STREAM AREA (ACRES) = 106.30  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 272.12

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6087.00 TO NODE 6088.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 313.20
DOWNSTREAM ELEVATION(FEET) = 312.50
ELEVATION DIFFERENCE(FEET) = 0.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.672
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.46
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.46

*****
FLOW PROCESS FROM NODE 6088.00 TO NODE 6089.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 312.50 DOWNSTREAM ELEVATION(FEET) = 309.00
STREET LENGTH(FEET) = 230.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.24
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.31
HALFSTREET FLOOD WIDTH(FEET) = 10.28
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.29
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.71
STREET FLOW TRAVEL TIME(MIN.) = 1.67 Tc(MIN.) = 6.34
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.135
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.770
SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 7.52
TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 8.77

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.36 HALFSTREET FLOOD WIDTH(FEET) = 12.00
FLOW VELOCITY(FEET/SEC.) = 2.66 DEPTH*VELOCITY(FT*FT/SEC.) = 0.94
LONGEST FLOWPATH FROM NODE 6087.00 TO NODE 6089.00 = 295.00 FEET.

*****
FLOW PROCESS FROM NODE 6089.00 TO NODE 6085.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

```

```

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 303.00 DOWNSTREAM(FEET) = 301.50
FLOW LENGTH(FEET) = 190.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 14.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.72
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.77
PIPE TRAVEL TIME(MIN.) = 0.55 Tc(MIN.) = 6.90
LONGEST FLOWPATH FROM NODE 6087.00 TO NODE 6085.00 = 485.00 FEET.

*****
FLOW PROCESS FROM NODE 6085.00 TO NODE 6085.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.90
RAINFALL INTENSITY(INCH/HR) = 7.71
TOTAL STREAM AREA(ACRES) = 1.40
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.77

*****
FLOW PROCESS FROM NODE 6066.00 TO NODE 6085.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 312.20
DOWNSTREAM ELEVATION(FEET) = 311.50
ELEVATION DIFFERENCE(FEET) = 0.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.672
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 7.30
TOTAL AREA(ACRES) = 1.00 TOTAL RUNOFF(CFS) = 7.30

*****
FLOW PROCESS FROM NODE 6085.00 TO NODE 6085.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:
TIME OF CONCENTRATION(MIN.) = 4.67
RAINFALL INTENSITY(INCH/HR) = 9.49
TOTAL STREAM AREA(ACRES) = 1.00
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.30

** CONFLUENCE DATA **
STREAM RUNOFF Tc INTENSITY AREA
NUMBER (CFS) (MIN.) (INCH/HOUR) (ACRE)

```

1	272.12	7.90	7.064	106.30
2	8.77	6.90	7.708	1.40
3	7.30	4.67	9.485	1.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	174.27	4.67	9.485
2	252.42	6.90	7.708
3	285.60	7.90	7.064

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 285.60 Tc(MIN.) = 7.90

TOTAL AREA(ACRES) = 108.70

LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6085.00 = 2425.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6085.00 TO NODE 6083.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 301.50 DOWNSTREAM(FEET) = 300.00

FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 63.0 INCH PIPE IS 50.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 15.37

ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 285.60

PIPE TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 8.05

LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6083.00 = 2565.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6083.00 TO NODE 6083.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 8.05

RAINFALL INTENSITY(INCH/HR) = 6.98

TOTAL STREAM AREA(ACRES) = 108.70

PEAK FLOW RATE(CFS) AT CONFLUENCE = 285.60

\*\*\*\*\*  
FLOW PROCESS FROM NODE 6082.00 TO NODE 6083.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00

UPSTREAM ELEVATION(FEET) = 314.00

DOWNSTREAM ELEVATION(FEET) = 313.00

ELEVATION DIFFERENCE (FEET) = 1.00  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 4.148  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF (CFS) = 3.65  
 TOTAL AREA (ACRES) = 0.50 TOTAL RUNOFF (CFS) = 3.65

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6083.00 TO NODE 6083.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 4.15  
 RAINFALL INTENSITY (INCH/HR) = 9.49  
 TOTAL STREAM AREA (ACRES) = 0.50  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 3.65

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	285.60	8.05	6.978	108.70
2	3.65	4.15	9.485	0.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	213.76	4.15	9.485
2	288.29	8.05	6.978

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 288.29 Tc (MIN.) = 8.05  
 TOTAL AREA (ACRES) = 109.20  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6083.00 = 2565.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6083.00 TO NODE 6080.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 300.00 DOWNSTREAM (FEET) = 299.00  
 FLOW LENGTH (FEET) = 125.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 69.0 INCH PIPE IS 51.0 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 14.01  
 ESTIMATED PIPE DIAMETER (INCH) = 69.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 288.29  
 PIPE TRAVEL TIME (MIN.) = 0.15 Tc (MIN.) = 8.20  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6080.00 = 2690.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6080.00 TO NODE 6080.00 IS CODE = 1

```

-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.20
RAINFALL INTENSITY(INCH/HR) = 6.90
TOTAL STREAM AREA(ACRES) = 109.20
PEAK FLOW RATE(CFS) AT CONFLUENCE = 288.29

*****
FLOW PROCESS FROM NODE 6068.00 TO NODE 6069.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00
UPSTREAM ELEVATION(FEET) = 360.00
DOWNSTREAM ELEVATION(FEET) = 320.00
ELEVATION DIFFERENCE(FEET) = 40.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.501
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.918
SUBAREA RUNOFF(CFS) = 0.45
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.45

*****
FLOW PROCESS FROM NODE 6069.00 TO NODE 6070.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 320.00 DOWNSTREAM(FEET) = 318.00
FLOW LENGTH(FEET) = 250.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 2.7 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 2.64
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 0.45
PIPE TRAVEL TIME(MIN.) = 1.58 Tc(MIN.) = 7.08
LONGEST FLOWPATH FROM NODE 6068.00 TO NODE 6070.00 = 310.00 FEET.

*****
FLOW PROCESS FROM NODE 6069.00 TO NODE 6070.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.578
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .2900
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.2800
SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 1.32
TOTAL AREA(ACRES) = 0.80 TOTAL RUNOFF(CFS) = 1.70
TC(MIN.) = 7.08

```



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*****
FLOW PROCESS FROM NODE    6070.00 TO NODE    6071.00 IS CODE =   62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #   1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =   317.50  DOWNSTREAM ELEVATION(FEET) =   315.80
STREET LENGTH(FEET) =    150.00  CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =    12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =    7.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =    0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    2
STREET PARKWAY CROSSFALL(DECIMAL) =    0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =    0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =    0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =          5.61
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =    0.33
HALFSTREET FLOOD WIDTH(FEET) =    11.21
AVERAGE FLOW VELOCITY(FEET/SEC.) =    2.09
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    0.69
STREET FLOW TRAVEL TIME(MIN.) =    1.20  Tc(MIN.) =    8.28
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    6.851
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT =    .7700
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT =    0.600
SUBAREA AREA(ACRES) =    1.50  SUBAREA RUNOFF(CFS) =    7.91
TOTAL AREA(ACRES) =    2.30  PEAK FLOW RATE(CFS) =    9.45

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) =    0.37  HALFSTREET FLOOD WIDTH(FEET) =    12.00
FLOW VELOCITY(FEET/SEC.) =    2.51  DEPTH*VELOCITY(FT*FT/SEC.) =    0.94
LONGEST FLOWPATH FROM NODE    6068.00 TO NODE    6071.00 =    460.00 FEET.

*****
FLOW PROCESS FROM NODE    6071.00 TO NODE    6080.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =    307.00  DOWNSTREAM(FEET) =    305.00
FLOW LENGTH(FEET) =    180.00  MANNING'S N =    0.013
DEPTH OF FLOW IN  18.0 INCH PIPE IS  13.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =    6.73
ESTIMATED PIPE DIAMETER(INCH) =    18.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =    9.45
PIPE TRAVEL TIME(MIN.) =    0.45  Tc(MIN.) =    8.72
LONGEST FLOWPATH FROM NODE    6068.00 TO NODE    6080.00 =    640.00 FEET.

*****
FLOW PROCESS FROM NODE    6080.00 TO NODE    6080.00 IS CODE =    1

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-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.72
RAINFALL INTENSITY(INCH/HR) = 6.62
TOTAL STREAM AREA(ACRES) = 2.30
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.45

** CONFLUENCE DATA **
STREAM      RUNOFF      Tc      INTENSITY      AREA
NUMBER      (CFS)      (MIN.)  (INCH/ HOUR)  (ACRE)
    1      288.29      8.20      6.896      109.20
    2       9.45      8.72      6.623       2.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **
STREAM      RUNOFF      Tc      INTENSITY
NUMBER      (CFS)      (MIN.)  (INCH/ HOUR)
    1      297.16      8.20      6.896
    2      286.34      8.72      6.623

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
PEAK FLOW RATE(CFS) = 297.16 Tc(MIN.) = 8.20
TOTAL AREA(ACRES) = 111.50
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6080.00 = 2690.00 FEET.

*****
FLOW PROCESS FROM NODE 6080.00 TO NODE 6079.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM( FEET) = 299.00 DOWNSTREAM( FEET) = 298.00
FLOW LENGTH( FEET) = 60.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 60.0 INCH PIPE IS 45.8 INCHES
PIPE-FLOW VELOCITY( FEET/ SEC.) = 18.49
ESTIMATED PIPE DIAMETER( INCH) = 60.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 297.16
PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 8.25
LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6079.00 = 2750.00 FEET.

*****
FLOW PROCESS FROM NODE 6079.00 TO NODE 6079.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 8.25
RAINFALL INTENSITY(INCH/HR) = 6.87
TOTAL STREAM AREA(ACRES) = 111.50
PEAK FLOW RATE(CFS) AT CONFLUENCE = 297.16

```

```

*****
FLOW PROCESS FROM NODE 6077.00 TO NODE 6078.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 317.70
DOWNSTREAM ELEVATION(FEET) = 316.70
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.406
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.020
SUBAREA RUNOFF(CFS) = 3.02
TOTAL AREA(ACRES) = 0.50 TOTAL RUNOFF(CFS) = 3.02

*****
FLOW PROCESS FROM NODE 6078.00 TO NODE 6079.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 316.70 DOWNSTREAM ELEVATION(FEET) = 313.80
STREET LENGTH(FEET) = 320.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 12.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 7.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.41
***STREET FLOWING FULL***
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.39
HALFSTREET FLOOD WIDTH(FEET) = 12.00
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.33
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.90
STREET FLOW TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 7.69
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.184
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.752
SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 12.72
TOTAL AREA(ACRES) = 2.80 PEAK FLOW RATE(CFS) = 15.13

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.44 HALFSTREET FLOOD WIDTH(FEET) = 12.00
FLOW VELOCITY(FEET/SEC.) = 2.83 DEPTH*VELOCITY(FT*FT/SEC.) = 1.25
LONGEST FLOWPATH FROM NODE 6077.00 TO NODE 6079.00 = 385.00 FEET.

```

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6079.00 TO NODE 6079.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 7.69  
 RAINFALL INTENSITY(INCH/HR) = 7.18  
 TOTAL STREAM AREA(ACRES) = 2.80  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.13

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	297.16	8.25	6.867	111.50
2	15.13	7.69	7.184	2.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	299.16	7.69	7.184
2	311.62	8.25	6.867

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 311.62 Tc(MIN.) = 8.25  
 TOTAL AREA(ACRES) = 114.30  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 6079.00 = 2750.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 6079.00 TO NODE 7068.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 298.00 DOWNSTREAM(FEET) = 296.00  
 FLOW LENGTH(FEET) = 130.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 63.0 INCH PIPE IS 46.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 18.23  
 ESTIMATED PIPE DIAMETER(INCH) = 63.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 311.62  
 PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 8.37  
 LONGEST FLOWPATH FROM NODE 6014.10 TO NODE 7068.00 = 2880.00 FEET.

+-----+  
 | Flow Information for Node 7068 |  
 +-----+

=====

END OF STUDY SUMMARY:  
 TOTAL AREA(ACRES) = 114.30 TC(MIN.) = 8.37

PEAK FLOW RATE(CFS) = 311.62

=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 7000B**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

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San Diego, California 92110  
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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Post-project (on-site) \*  
\* Drainage Basin 7000B \*  
\*\*\*\*\*

FILE NAME: MW\_7BK00.DAT  
TIME/DATE OF STUDY: 14:49 07/16/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	18.0	13.0	0.020/0.020/0.020	0.50	1.50	0.0100	0.125	0.0180

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 7079.00 TO NODE 7080.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00  
 UPSTREAM ELEVATION(FEET) = 300.60  
 DOWNSTREAM ELEVATION(FEET) = 300.00  
 ELEVATION DIFFERENCE(FEET) = 0.60  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.789  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.71  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.71

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7080.00 TO NODE 7081.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>(STREET TABLE SECTION # 1 USED)<<<<<

UPSTREAM ELEVATION(FEET) = 300.00 DOWNSTREAM ELEVATION(FEET) = 282.00  
 STREET LENGTH(FEET) = 1530.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 12.60  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.41  
 HALFSTREET FLOOD WIDTH(FEET) = 15.33  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.58  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 1.06  
 STREET FLOW TRAVEL TIME(MIN.) = 9.87 Tc(MIN.) = 12.66  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.211  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .6700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.678  
 SUBAREA AREA(ACRES) = 5.60 SUBAREA RUNOFF(CFS) = 19.55  
 TOTAL AREA(ACRES) = 5.80 PEAK FLOW RATE(CFS) = 20.49

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 18.00  
 FLOW VELOCITY(FEET/SEC.) = 2.93 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.39  
 \*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,  
 AND L = 1530.0 FT WITH ELEVATION-DROP = 18.0 FT, IS 31.5 CFS,  
 WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 7081.00  
 LONGEST FLOWPATH FROM NODE 7079.00 TO NODE 7081.00 = 1590.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7081.00 TO NODE 7099.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<



```

=====
ELEVATION DATA: UPSTREAM(FEET) = 282.00 DOWNSTREAM(FEET) = 280.00
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 15.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.14
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 20.49
PIPE TRAVEL TIME(MIN.) = 0.12 Tc(MIN.) = 12.78
LONGEST FLOWPATH FROM NODE 7079.00 TO NODE 7099.00 = 1670.00 FEET.

*****
FLOW PROCESS FROM NODE 7099.00 TO NODE 7099.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.78
RAINFALL INTENSITY(INCH/HR) = 5.18
TOTAL STREAM AREA(ACRES) = 5.80
PEAK FLOW RATE(CFS) AT CONFLUENCE = 20.49

*****
FLOW PROCESS FROM NODE 7093.00 TO NODE 7094.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 90.00
UPSTREAM ELEVATION(FEET) = 860.00
DOWNSTREAM ELEVATION(FEET) = 800.00
ELEVATION DIFFERENCE(FEET) = 60.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.945
WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.483
SUBAREA RUNOFF(CFS) = 0.59
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.59

*****
FLOW PROCESS FROM NODE 7094.00 TO NODE 7095.00 IS CODE = 51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 800.00 DOWNSTREAM(FEET) = 318.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1200.00 CHANNEL SLOPE = 0.4017
CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000
MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.095
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .3400
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.74
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 5.02
AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 3.98

```

Tc(MIN.) = 9.93  
 SUBAREA AREA(ACRES) = 3.90 SUBAREA RUNOFF(CFS) = 8.08  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.340  
 TOTAL AREA(ACRES) = 4.10 PEAK FLOW RATE(CFS) = 8.51

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 6.05  
 LONGEST FLOWPATH FROM NODE 7093.00 TO NODE 7095.00 = 1290.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7095.00 TO NODE 7095.60 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 318.00 DOWNSTREAM(FEET) = 290.00  
 FLOW LENGTH(FEET) = 1000.00 MANNING'S N = 0.016  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.3 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.10  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 8.51  
 PIPE TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 11.98  
 LONGEST FLOWPATH FROM NODE 7093.00 TO NODE 7095.60 = 2290.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7095.00 TO NODE 7099.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

=====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.398.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3400  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3401  
 SUBAREA AREA(ACRES) = 23.80 SUBAREA RUNOFF(CFS) = 43.68  
 TOTAL AREA(ACRES) = 27.90 TOTAL RUNOFF(CFS) = 51.21  
 TC(MIN.) = 11.98

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7095.60 TO NODE 7099.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 290.00 DOWNSTREAM(FEET) = 277.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 110.00 CHANNEL SLOPE = 0.1182  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 CHANNEL FLOW THRU SUBAREA(CFS) = 51.21  
 FLOW VELOCITY(FEET/SEC.) = 7.29 FLOW DEPTH(FEET) = 0.48  
 TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 12.23  
 LONGEST FLOWPATH FROM NODE 7093.00 TO NODE 7099.00 = 2400.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7099.00 TO NODE 7099.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

```

=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 12.23
RAINFALL INTENSITY(INCH/HR) = 5.33
TOTAL STREAM AREA(ACRES) = 27.90
PEAK FLOW RATE(CFS) AT CONFLUENCE = 51.21

*****
FLOW PROCESS FROM NODE 7104.00 TO NODE 7106.00 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 80.00
UPSTREAM ELEVATION(FEET) = 326.00
DOWNSTREAM ELEVATION(FEET) = 320.00
ELEVATION DIFFERENCE(FEET) = 6.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 5.347
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.084
SUBAREA RUNOFF(CFS) = 0.82
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.82

*****
FLOW PROCESS FROM NODE 7106.00 TO NODE 7099.00 IS CODE = 51
-----
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 320.00 DOWNSTREAM(FEET) = 280.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 1000.00 CHANNEL SLOPE = 0.0400
CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 1.000
MANNING'S FACTOR = 0.016 MAXIMUM DEPTH(FEET) = 2.00
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.739
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .4500
S.C.S. CURVE NUMBER (AMC II) = 0
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 19.92
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 11.05
AVERAGE FLOW DEPTH(FEET) = 0.67 TRAVEL TIME(MIN.) = 1.51
Tc(MIN.) = 6.85
SUBAREA AREA(ACRES) = 10.90 SUBAREA RUNOFF(CFS) = 37.96
AREA-AVERAGE RUNOFF COEFFICIENT = 0.450
TOTAL AREA(ACRES) = 11.10 PEAK FLOW RATE(CFS) = 38.65

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.97 FLOW VELOCITY(FEET/SEC.) = 13.35
LONGEST FLOWPATH FROM NODE 7104.00 TO NODE 7099.00 = 1080.00 FEET.

*****
FLOW PROCESS FROM NODE 7099.00 TO NODE 7099.00 IS CODE = 1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
=====

```

TOTAL NUMBER OF STREAMS = 3  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.85  
 RAINFALL INTENSITY(INCH/HR) = 7.74  
 TOTAL STREAM AREA(ACRES) = 11.10  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 38.65

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	20.49	12.78	5.179	5.80
2	51.21	12.23	5.326	27.90
3	38.65	6.85	7.739	11.10

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	78.34	6.85	7.739
2	97.43	12.23	5.326
3	96.16	12.78	5.179

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 97.43 Tc(MIN.) = 12.23  
 TOTAL AREA(ACRES) = 44.80  
 LONGEST FLOWPATH FROM NODE 7093.00 TO NODE 7099.00 = 2400.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7099.00 TO NODE 7100.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 275.00 DOWNSTREAM(FEET) = 265.00  
 FLOW LENGTH(FEET) = 340.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 26.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 17.37  
 ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 97.43  
 PIPE TRAVEL TIME(MIN.) = 0.33 Tc(MIN.) = 12.56  
 LONGEST FLOWPATH FROM NODE 7093.00 TO NODE 7100.00 = 2740.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 7100.00 TO NODE 7100.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 12.56  
 RAINFALL INTENSITY(INCH/HR) = 5.24  
 TOTAL STREAM AREA(ACRES) = 44.80  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 97.43

\*\*\*\*\*

FLOW PROCESS FROM NODE 7082.00 TO NODE 7100.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00

UPSTREAM ELEVATION(FEET) = 281.00

DOWNSTREAM ELEVATION(FEET) = 280.50

ELEVATION DIFFERENCE(FEET) = 0.50

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.364

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.118

SUBAREA RUNOFF(CFS) = 2.44

TOTAL AREA(ACRES) = 0.50 TOTAL RUNOFF(CFS) = 2.44

\*\*\*\*\*

FLOW PROCESS FROM NODE 7100.00 TO NODE 7100.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 6.36

RAINFALL INTENSITY(INCH/HR) = 8.12

TOTAL STREAM AREA(ACRES) = 0.50

PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.44

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	97.43	12.56	5.236	44.80
2	2.44	6.36	8.118	0.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	65.28	6.36	8.118
2	99.00	12.56	5.236

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 99.00 Tc(MIN.) = 12.56

TOTAL AREA(ACRES) = 45.30

LONGEST FLOWPATH FROM NODE 7093.00 TO NODE 7100.00 = 2740.00 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 45.30 TC(MIN.) = 12.56

PEAK FLOW RATE(CFS) = 99.00

=====

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 8000A & 8000B**

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Post-project (on-site) \*  
\* Drainage Basin 8000A (Undetained) \*  
\*\*\*\*\*

FILE NAME: MW81K100.DAT  
TIME/DATE OF STUDY: 08:00 07/14/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
NO.	(FT)	(FT)						
1	18.0	13.0	0.020/0.020/0.020	0.50	1.50	0.0100	0.125	0.0180

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8100.00 TO NODE 8101.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 865.00  
 DOWNSTREAM ELEVATION(FEET) = 810.00  
 ELEVATION DIFFERENCE(FEET) = 55.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.200  
 SUBAREA RUNOFF(CFS) = 0.86  
 TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.86

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8101.00 TO NODE 8102.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 810.00 DOWNSTREAM(FEET) = 280.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 955.00 CHANNEL SLOPE = 0.5550  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.953  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 15.88  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 8.72  
 AVERAGE FLOW DEPTH(FEET) = 0.16 TRAVEL TIME(MIN.) = 1.82  
 Tc(MIN.) = 8.09  
 SUBAREA AREA(ACRES) = 13.00 SUBAREA RUNOFF(CFS) = 29.83  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.330  
 TOTAL AREA(ACRES) = 13.30 PEAK FLOW RATE(CFS) = 30.56

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.23 FLOW VELOCITY(FEET/SEC.) = 10.60  
 LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8102.00 = 1055.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8102.00 TO NODE 8116.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 273.50 DOWNSTREAM(FEET) = 272.50  
 FLOW LENGTH(FEET) = 120.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 30.0 INCH PIPE IS 21.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.14  
 ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 30.56  
 PIPE TRAVEL TIME(MIN.) = 0.25 Tc(MIN.) = 8.34  
 LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8116.00 = 1175.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8116.00 TO NODE 8116.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2



CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 8.34  
RAINFALL INTENSITY(INCH/HR) = 6.82  
TOTAL STREAM AREA(ACRES) = 13.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.56

\*\*\*\*\*

FLOW PROCESS FROM NODE 8114.00 TO NODE 8115.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00  
UPSTREAM ELEVATION(FEET) = 280.60  
DOWNSTREAM ELEVATION(FEET) = 280.00  
ELEVATION DIFFERENCE(FEET) = 0.60  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.789  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON  $T_c$  = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.71  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 8115.00 TO NODE 8116.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 275.50  
STREET LENGTH(FEET) = 445.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.94  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.40  
HALFSTREET FLOOD WIDTH(FEET) = 14.98  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.35  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.95  
STREET FLOW TRAVEL TIME(MIN.) = 3.16  $T_c$ (MIN.) = 5.95  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.481

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
SUBAREA AREA(ACRES) = 2.40 SUBAREA RUNOFF(CFS) = 18.32  
TOTAL AREA(ACRES) = 2.60 PEAK FLOW RATE(CFS) = 19.85

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.48 HALFSTREET FLOOD WIDTH(FEET) = 18.00

FLOW VELOCITY(FEET/SEC.) = 2.77 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.33

LONGEST FLOWPATH FROM NODE 8114.00 TO NODE 8116.00 = 505.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8116.00 TO NODE 8116.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 5.95

RAINFALL INTENSITY(INCH/HR) = 8.48

TOTAL STREAM AREA(ACRES) = 2.60

PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.85

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	30.56	8.34	6.820	13.30
2	19.85	5.95	8.481	2.60

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	41.64	5.95	8.481
2	46.52	8.34	6.820

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 46.52 Tc(MIN.) = 8.34

TOTAL AREA(ACRES) = 15.90

LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8116.00 = 1175.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8116.00 TO NODE 8121.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 272.50 DOWNSTREAM(FEET) = 270.00

FLOW LENGTH(FEET) = 385.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 36.0 INCH PIPE IS 27.0 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 8.18

ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 46.52

PIPE TRAVEL TIME(MIN.) = 0.78 Tc(MIN.) = 9.12

LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8121.00 = 1560.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8121.00 TO NODE 8121.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 9.12  
RAINFALL INTENSITY(INCH/HR) = 6.44  
TOTAL STREAM AREA(ACRES) = 15.90  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 46.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 8118.00 TO NODE 8119.00 IS CODE = 21

-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00  
UPSTREAM ELEVATION(FEET) = 284.10  
DOWNSTREAM ELEVATION(FEET) = 283.80  
ELEVATION DIFFERENCE(FEET) = 0.30  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.018  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.71  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.71

\*\*\*\*\*

FLOW PROCESS FROM NODE 8119.00 TO NODE 8120.00 IS CODE = 62

-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>(STREET TABLE SECTION # 1 USED)<<<<

=====

UPSTREAM ELEVATION(FEET) = 283.80 DOWNSTREAM ELEVATION(FEET) = 280.30  
STREET LENGTH(FEET) = 320.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 6.53  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 11.98  
AVERAGE FLOW VELOCITY(FT/SEC.) = 2.14  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.74  
STREET FLOW TRAVEL TIME(MIN.) = 2.49 Tc(MIN.) = 5.50  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.915  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 9.63  
 TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 11.23

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 14.88  
 FLOW VELOCITY(FEET/SEC.) = 2.44 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.98  
 LONGEST FLOWPATH FROM NODE 8118.00 TO NODE 8120.00 = 370.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8120.00 TO NODE 8121.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 270.70 DOWNSTREAM(FEET) = 270.00  
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 13.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.85  
 ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 11.23  
 PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 5.67  
 LONGEST FLOWPATH FROM NODE 8118.00 TO NODE 8121.00 = 440.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8121.00 TO NODE 8121.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.67  
 RAINFALL INTENSITY(INCH/HR) = 8.74  
 TOTAL STREAM AREA(ACRES) = 1.40  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.23

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	46.52	9.12	6.436	15.90
2	11.23	5.67	8.741	1.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	45.48	5.67	8.741
2	54.79	9.12	6.436

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 54.79 Tc(MIN.) = 9.12  
 TOTAL AREA(ACRES) = 17.30  
 LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8121.00 = 1560.00 FEET.

```

*****
FLOW PROCESS FROM NODE      8121.00 TO NODE      8126.00 IS CODE =  31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =   270.00  DOWNSTREAM(FEET) =   264.50
FLOW LENGTH(FEET) =   270.00  MANNING'S N =   0.013
DEPTH OF FLOW IN  30.0 INCH PIPE IS  24.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) =   12.90
ESTIMATED PIPE DIAMETER(INCH) =   30.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =          54.79
PIPE TRAVEL TIME(MIN.) =    0.35  Tc(MIN.) =    9.47
LONGEST FLOWPATH FROM NODE      8100.00 TO NODE      8126.00 =  1830.00 FEET.

*****
FLOW PROCESS FROM NODE      8126.00 TO NODE      8126.00 IS CODE =   1
-----
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
=====
TOTAL NUMBER OF STREAMS =  2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM  1 ARE:
TIME OF CONCENTRATION(MIN.) =   9.47
RAINFALL INTENSITY(INCH/HR) =   6.28
TOTAL STREAM AREA(ACRES) =   17.30
PEAK FLOW RATE(CFS) AT CONFLUENCE =          54.79

*****
FLOW PROCESS FROM NODE      8123.00 TO NODE      8124.00 IS CODE =  21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7800
S.C.S. CURVE NUMBER (AMC II) =    0
INITIAL SUBAREA FLOW-LENGTH(FEET) =   65.00
UPSTREAM ELEVATION(FEET) =   286.20
DOWNSTREAM ELEVATION(FEET) =   285.50
ELEVATION DIFFERENCE(FEET) =    0.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.531
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) =          1.48
TOTAL AREA(ACRES) =    0.20  TOTAL RUNOFF(CFS) =          1.48

*****
FLOW PROCESS FROM NODE      8124.00 TO NODE      8125.00 IS CODE =  62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #  1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =   285.50  DOWNSTREAM ELEVATION(FEET) =   276.00
STREET LENGTH(FEET) =   355.00  CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =   18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =   13.00
INSIDE STREET CROSSFALL(DECIMAL) =    0.020

```

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.53

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.28

HALFSTREET FLOOD WIDTH(FEET) = 8.58

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.75

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.76

STREET FLOW TRAVEL TIME(MIN.) = 2.15 Tc(MIN.) = 6.68

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.869

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.772

SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 6.06

TOTAL AREA(ACRES) = 1.20 PEAK FLOW RATE(CFS) = 7.29

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.31 HALFSTREET FLOOD WIDTH(FEET) = 10.46

FLOW VELOCITY(FEET/SEC.) = 3.09 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.97

LONGEST FLOWPATH FROM NODE 8123.00 TO NODE 8125.00 = 420.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8125.00 TO NODE 8126.00 IS CODE = 31

-----  
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 266.00 DOWNSTREAM(FEET) = 264.50

FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013

ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000

DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.4 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.85

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 7.29

PIPE TRAVEL TIME(MIN.) = 0.17 Tc(MIN.) = 6.85

LONGEST FLOWPATH FROM NODE 8123.00 TO NODE 8126.00 = 500.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8126.00 TO NODE 8126.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 6.85

RAINFALL INTENSITY(INCH/HR) = 7.74

TOTAL STREAM AREA(ACRES) = 1.20

PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.29

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	54.79	9.47	6.282	17.30
2	7.29	6.85	7.742	1.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	51.74	6.85	7.742
2	60.70	9.47	6.282

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 60.70 Tc(MIN.) = 9.47

TOTAL AREA(ACRES) = 18.50

LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8126.00 = 1830.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8126.00 TO NODE 8147.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 264.50 DOWNSTREAM(FEET) = 264.00  
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.4 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.40  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 60.70  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 9.51  
LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8147.00 = 1860.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8147.00 TO NODE 8147.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8128.00 TO NODE 8129.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .9000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00

UPSTREAM ELEVATION(FEET) = 282.10

DOWNSTREAM ELEVATION(FEET) = 281.50

ELEVATION DIFFERENCE(FEET) = 0.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.789

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 1.71

TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.71

```

*****
FLOW PROCESS FROM NODE    8129.00 TO NODE    8130.00 IS CODE =   62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION #   1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) =  281.50  DOWNSTREAM ELEVATION(FEET) =  279.50
STREET LENGTH(FEET) =    230.00  CURB HEIGHT(INCHES) =    6.0
STREET HALFWIDTH(FEET) =    18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) =   13.00
INSIDE STREET CROSSFALL(DECIMAL) =   0.020
OUTSIDE STREET CROSSFALL(DECIMAL) =   0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF =    2
STREET PARKWAY CROSSFALL(DECIMAL) =   0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) =   0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section =   0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =           4.63
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) =   0.32
HALFSTREET FLOOD WIDTH(FEET) =   10.92
AVERAGE FLOW VELOCITY(FT/SEC.) =    1.81
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) =    0.59
STREET FLOW TRAVEL TIME(MIN.) =   2.12  Tc(MIN.) =    4.91
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =   9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) =    0
AREA-AVERAGE RUNOFF COEFFICIENT =   0.796
SUBAREA AREA(ACRES) =    0.80  SUBAREA RUNOFF(CFS) =    5.84
TOTAL AREA(ACRES) =    1.00  PEAK FLOW RATE(CFS) =    7.55

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37  HALFSTREET FLOOD WIDTH(FEET) =   13.30
FLOW VELOCITY(FT/SEC.) =  2.03  DEPTH*VELOCITY(FT*FT/SEC.) =   0.75
LONGEST FLOWPATH FROM NODE    8128.00 TO NODE    8130.00 =   290.00 FEET.

*****
FLOW PROCESS FROM NODE    8130.00 TO NODE    8134.00 IS CODE =   31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) =  268.00  DOWNSTREAM(FEET) =  266.50
FLOW LENGTH(FEET) =   290.00  MANNING'S N =   0.013
DEPTH OF FLOW IN  21.0 INCH PIPE IS  12.9 INCHES
PIPE-FLOW VELOCITY(FT/SEC.) =    4.86
ESTIMATED PIPE DIAMETER(INCH) =  21.00  NUMBER OF PIPES =    1
PIPE-FLOW(CFS) =    7.55
PIPE TRAVEL TIME(MIN.) =    0.99  Tc(MIN.) =    5.90
LONGEST FLOWPATH FROM NODE    8128.00 TO NODE    8134.00 =   580.00 FEET.

*****

```



FLOW PROCESS FROM NODE 8134.00 TO NODE 8134.00 IS CODE = 1

=====

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.90  
RAINFALL INTENSITY(INCH/HR) = 8.52  
TOTAL STREAM AREA(ACRES) = 1.00  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 7.55

\*\*\*\*\*

FLOW PROCESS FROM NODE 8132.00 TO NODE 8133.00 IS CODE = 21

=====

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00  
UPSTREAM ELEVATION(FEET) = 279.60  
DOWNSTREAM ELEVATION(FEET) = 279.00  
ELEVATION DIFFERENCE(FEET) = 0.60  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.601  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.46  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 8133.00 TO NODE 8134.00 IS CODE = 62

=====

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 279.00 DOWNSTREAM ELEVATION(FEET) = 276.00  
STREET LENGTH(FEET) = 300.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.66  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.32  
HALFSTREET FLOOD WIDTH(FEET) = 10.66  
AVERAGE FLOW VELOCITY(FT/SEC.) = 1.90  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.61  
STREET FLOW TRAVEL TIME(MIN.) = 2.63 Tc(MIN.) = 7.23  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.479  
\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA (ACRES) = 1.10      SUBAREA RUNOFF (CFS) = 6.34  
 TOTAL AREA (ACRES) = 1.30      PEAK FLOW RATE (CFS) = 7.49

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.36    HALFSTREET FLOOD WIDTH (FEET) = 12.90  
 FLOW VELOCITY (FEET/SEC.) = 2.14    DEPTH\*VELOCITY (FT\*FT/SEC.) = 0.78  
 LONGEST FLOWPATH FROM NODE 8132.00 TO NODE 8134.00 = 360.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8134.00 TO NODE 8134.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====  
 TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION (MIN.) = 7.23  
 RAINFALL INTENSITY (INCH/HR) = 7.48  
 TOTAL STREAM AREA (ACRES) = 1.30  
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 7.49

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	7.55	5.90	8.525	1.00
2	7.49	7.23	7.479	1.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	13.66	5.90	8.525
2	14.11	7.23	7.479

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 14.11    Tc (MIN.) = 7.23  
 TOTAL AREA (ACRES) = 2.30  
 LONGEST FLOWPATH FROM NODE 8128.00 TO NODE 8134.00 = 580.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8134.00 TO NODE 8143.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====  
 ELEVATION DATA: UPSTREAM (FEET) = 266.50    DOWNSTREAM (FEET) = 265.00  
 FLOW LENGTH (FEET) = 235.00    MANNING'S N = 0.013  
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.6 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 6.09  
 ESTIMATED PIPE DIAMETER (INCH) = 24.00    NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 14.11  
 PIPE TRAVEL TIME (MIN.) = 0.64    Tc (MIN.) = 7.87

LONGEST FLOWPATH FROM NODE 8128.00 TO NODE 8143.00 = 815.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8143.00 TO NODE 8143.00 IS CODE = 1  
-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.87  
RAINFALL INTENSITY(INCH/HR) = 7.08  
TOTAL STREAM AREA(ACRES) = 2.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 14.11

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8136.00 TO NODE 8137.00 IS CODE = 21  
-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00  
UPSTREAM ELEVATION(FEET) = 279.60  
DOWNSTREAM ELEVATION(FEET) = 278.50  
ELEVATION DIFFERENCE(FEET) = 1.10  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.759  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 2.19  
TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 2.19

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8137.00 TO NODE 8138.00 IS CODE = 62  
-----  
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 278.50 DOWNSTREAM ELEVATION(FEET) = 276.00  
STREET LENGTH(FEET) = 65.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.38  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.26  
HALFSTREET FLOOD WIDTH(FEET) = 7.82  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.14  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.82

STREET FLOW TRAVEL TIME(MIN.) = 0.34 Tc(MIN.) = 4.10  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 4.38  
 TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 6.57

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 9.29  
 FLOW VELOCITY(FEET/SEC.) = 3.46 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.01  
 LONGEST FLOWPATH FROM NODE 8136.00 TO NODE 8138.00 = 125.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8138.00 TO NODE 8143.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 271.00 DOWNSTREAM(FEET) = 264.50  
 FLOW LENGTH(FEET) = 400.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.25  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 6.57  
 PIPE TRAVEL TIME(MIN.) = 0.92 Tc(MIN.) = 5.02  
 LONGEST FLOWPATH FROM NODE 8136.00 TO NODE 8143.00 = 525.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8143.00 TO NODE 8143.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.02  
 RAINFALL INTENSITY(INCH/HR) = 9.46  
 TOTAL STREAM AREA(ACRES) = 0.90  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.57

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	14.11	7.87	7.080	2.30
2	6.57	5.02	9.456	0.90

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	17.14	5.02	9.456

2        19.03        7.87        7.080

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =        19.03        T<sub>c</sub>(MIN.) =        7.87

TOTAL AREA(ACRES) =        3.20

LONGEST FLOWPATH FROM NODE    8128.00 TO NODE    8143.00 =    815.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE    8143.00 TO NODE    8147.00 IS CODE =    31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) =    265.00    DOWNSTREAM(FEET) =    264.50

FLOW LENGTH(FEET) =    70.00    MANNING'S N =    0.013

DEPTH OF FLOW IN    27.0 INCH PIPE IS    17.7 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) =    6.88

ESTIMATED PIPE DIAMETER(INCH) =    27.00    NUMBER OF PIPES =    1

PIPE-FLOW(CFS) =        19.03

PIPE TRAVEL TIME(MIN.) =    0.17        T<sub>c</sub>(MIN.) =    8.04

LONGEST FLOWPATH FROM NODE    8128.00 TO NODE    8147.00 =    885.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE    8147.00 TO NODE    8147.00 IS CODE =    1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS =    2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    1 ARE:

TIME OF CONCENTRATION(MIN.) =    8.04

RAINFALL INTENSITY(INCH/HR) =    6.98

TOTAL STREAM AREA(ACRES) =    3.20

PEAK FLOW RATE(CFS) AT CONFLUENCE =        19.03

\*\*\*\*\*

FLOW PROCESS FROM NODE.    8145.00 TO NODE    8146.00 IS CODE =    21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700

S.C.S. CURVE NUMBER (AMC II) =    0

INITIAL SUBAREA FLOW-LENGTH(FEET) =    60.00

UPSTREAM ELEVATION(FEET) =    276.10

DOWNSTREAM ELEVATION(FEET) =    275.50

ELEVATION DIFFERENCE(FEET) =    0.60

SUBAREA OVERLAND TIME OF FLOW(MIN.) =    4.601

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    9.485

NOTE: RAINFALL INTENSITY IS BASED ON T<sub>c</sub> = 5-MINUTE.

SUBAREA RUNOFF(CFS) =        1.46

TOTAL AREA(ACRES) =        0.20    TOTAL RUNOFF(CFS) =        1.46

\*\*\*\*\*

FLOW PROCESS FROM NODE    8146.00 TO NODE    8147.00 IS CODE =    62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STREET TABLE SECTION #    1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 275.50 DOWNSTREAM ELEVATION(FEET) = 273.30  
STREET LENGTH(FEET) = 230.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.69  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.38  
HALFSTREET FLOOD WIDTH(FEET) = 13.81  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.18  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.83  
STREET FLOW TRAVEL TIME(MIN.) = 1.76 Tc(MIN.) = 6.36  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.122  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
SUBAREA AREA(ACRES) = 2.30 SUBAREA RUNOFF(CFS) = 14.38  
TOTAL AREA(ACRES) = 2.50 PEAK FLOW RATE(CFS) = 15.63

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.45 HALFSTREET FLOOD WIDTH(FEET) = 17.37  
FLOW VELOCITY(FEET/SEC.) = 2.52 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.14  
LONGEST FLOWPATH FROM NODE 8145.00 TO NODE 8147.00 = 290.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8147.00 TO NODE 8147.00 IS CODE = 1

-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 6.36  
RAINFALL INTENSITY(INCH/HR) = 8.12  
TOTAL STREAM AREA(ACRES) = 2.50  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 15.63

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	19.03	8.04	6.983	3.20
2	15.63	6.36	8.122	2.50

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	32.00	6.36	8.122
2	32.47	8.04	6.983

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 32.47 Tc(MIN.) = 8.04

TOTAL AREA(ACRES) = 5.70

LONGEST FLOWPATH FROM NODE 8128.00 TO NODE 8147.00 = 885.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8147.00 TO NODE 8147.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	32.47	8.04	6.983	5.70

LONGEST FLOWPATH FROM NODE 8128.00 TO NODE 8147.00 = 885.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	60.70	9.51	6.265	18.50

LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8147.00 = 1860.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	83.78	8.04	6.983
2	89.84	9.51	6.265

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 89.84 Tc(MIN.) = 9.51

TOTAL AREA(ACRES) = 24.20

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8147.00 TO NODE 8147.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8147.00 TO NODE 8149.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 264.00 DOWNSTREAM(FEET) = 263.20  
 FLOW LENGTH(FEET) = 150.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.6 INCHES  
 PIPE-FLOW VELOCITY( FEET/SEC.) = 8.98  
 ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 89.84  
 PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 9.79

LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8149.00 = 2010.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8149.00 TO NODE 8149.00 IS CODE = 1

-----  
>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION(MIN.) =	9.79
RAINFALL INTENSITY(INCH/HR) =	6.15
TOTAL STREAM AREA(ACRES) =	24.20
PEAK FLOW RATE(CFS) AT CONFLUENCE =	89.84

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8148.20 TO NODE 8148.40 IS CODE = 21

-----  
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2500
S.C.S. CURVE NUMBER (AMC II) =	0
INITIAL SUBAREA FLOW-LENGTH(FEET) =	70.00
UPSTREAM ELEVATION(FEET) =	278.00
DOWNSTREAM ELEVATION(FEET) =	277.00
ELEVATION DIFFERENCE(FEET) =	1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) =	11.366
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	5.585
SUBAREA RUNOFF(CFS) =	0.28
TOTAL AREA(ACRES) =	0.20
TOTAL RUNOFF(CFS) =	0.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8148.40 TO NODE 8148.60 IS CODE = 51

-----  
>>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
>>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	277.00	DOWNSTREAM(FEET) =	273.00
CHANNEL LENGTH THRU SUBAREA(FEET) =	430.00	CHANNEL SLOPE =	0.0093
CHANNEL BASE(FEET) =	0.00	"Z" FACTOR =	10.000
MANNING'S FACTOR = 0.035	MAXIMUM DEPTH(FEET) =	1.00	
100 YEAR RAINFALL INTENSITY(INCH/HOUR) =	3.988		

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT =	.2500		
S.C.S. CURVE NUMBER (AMC II) =	0		
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) =	0.38		
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) =	0.92		
AVERAGE FLOW DEPTH(FEET) =	0.20	TRAVEL TIME(MIN.) =	7.79
Tc(MIN.) =	19.16		
SUBAREA AREA(ACRES) =	0.20	SUBAREA RUNOFF(CFS) =	0.20
AREA-AVERAGE RUNOFF COEFFICIENT =	0.250		
TOTAL AREA(ACRES) =	0.40	PEAK FLOW RATE(CFS) =	0.40

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH(FEET) =	0.21	FLOW VELOCITY(FEET/SEC.) =	0.91
LONGEST FLOWPATH FROM NODE 8148.20 TO NODE 8148.60 =	500.00 FEET.		



\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8148.60 TO NODE 8149.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	270.00	DOWNSTREAM(FEET) =	263.20
FLOW LENGTH(FEET) =	50.00	MANNING'S N =	0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000			
DEPTH OF FLOW IN 18.0 INCH PIPE IS 1.3 INCHES			
PIPE-FLOW VELOCITY(FEET/SEC.) =	6.85		
ESTIMATED PIPE DIAMETER(INCH) =	18.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	0.40		
PIPE TRAVEL TIME(MIN.) =	0.12	Tc(MIN.) =	19.28
LONGEST FLOWPATH FROM NODE 8148.20 TO NODE 8149.00 = 550.00 FEET.			

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8149.00 TO NODE 8149.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:	
TIME OF CONCENTRATION(MIN.) =	19.28
RAINFALL INTENSITY(INCH/HR) =	3.97
TOTAL STREAM AREA(ACRES) =	0.40
PEAK FLOW RATE(CFS) AT CONFLUENCE =	0.40

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	89.84	9.79	6.149	24.20
2	0.40	19.28	3.972	0.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	90.04	9.79	6.149
2	58.43	19.28	3.972

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =	90.04	Tc(MIN.) =	9.79
TOTAL AREA(ACRES) =	24.60		
LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8149.00 = 2010.00 FEET.			

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8149.00 TO NODE 8152.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	263.20	DOWNSTREAM(FEET) =	262.50
FLOW LENGTH(FEET) =	180.00	MANNING'S N =	0.013

DEPTH OF FLOW IN 51.0 INCH PIPE IS 37.8 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.99  
 ESTIMATED PIPE DIAMETER(INCH) = 51.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 90.04  
 PIPE TRAVEL TIME(MIN.) = 0.38 Tc(MIN.) = 10.17  
 LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8152.00 = 2190.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8152.00 TO NODE 8152.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 10.17  
 RAINFALL INTENSITY(INCH/HR) = 6.00  
 TOTAL STREAM AREA(ACRES) = 24.60  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 90.04

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8150.00 TO NODE 8151.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .9000  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 70.00  
 UPSTREAM ELEVATION(FEET) = 279.20  
 DOWNSTREAM ELEVATION(FEET) = 278.50  
 ELEVATION DIFFERENCE(FEET) = 0.70  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.902  
 WARNING: INITIAL SUBAREA FLOW PATH LENGTH IS GREATER THAN  
           THE MAXIMUM OVERLAND FLOW LENGTH = 65.00  
           (Reference: Table 3-1B of Hydrology Manual)  
           THE MAXIMUM OVERLAND FLOW LENGTH IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 2.56  
 TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 2.56

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8151.00 TO NODE 8152.00 IS CODE = 62

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 278.50 DOWNSTREAM ELEVATION(FEET) = 269.00  
 STREET LENGTH(FEET) = 455.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.33  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.34  
HALFSTREET FLOOD WIDTH(FEET) = 11.63  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.89  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.98  
STREET FLOW TRAVEL TIME(MIN.) = 2.62 Tc(MIN.) = 5.52  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.897  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .6700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.701  
SUBAREA AREA(ACRES) = 1.90 SUBAREA RUNOFF(CFS) = 11.33  
TOTAL AREA(ACRES) = 2.20 PEAK FLOW RATE(CFS) = 13.73

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.39 HALFSTREET FLOOD WIDTH(FEET) = 14.17  
FLOW VELOCITY(FEET/SEC.) = 3.28 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.27  
LONGEST FLOWPATH FROM NODE 8150.00 TO NODE 8152.00 = 525.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8152.00 TO NODE 8152.00 IS CODE = 1  
-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<  
=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.52  
RAINFALL INTENSITY(INCH/HR) = 8.90  
TOTAL STREAM AREA(ACRES) = 2.20  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 13.73

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	90.04	10.17	6.002	24.60
2	13.73	5.52	8.897	2.20

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	74.47	5.52	8.897
2	99.30	10.17	6.002

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:  
PEAK FLOW RATE(CFS) = 99.30 Tc(MIN.) = 10.17  
TOTAL AREA(ACRES) = 26.80  
LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8152.00 = 2190.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8152.00 TO NODE 8153.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 262.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 45.0 INCH PIPE IS 32.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 11.69  
ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 99.30  
PIPE TRAVEL TIME(MIN.) = 0.07 Tc(MIN.) = 10.24  
LONGEST FLOWPATH FROM NODE 8100.00 TO NODE 8153.00 = 2240.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 26.80 TC(MIN.) = 10.24  
PEAK FLOW RATE(CFS) = 99.30

END OF RATIONAL METHOD ANALYSIS

\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

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San Diego, California 92110  
619-291-0707 Fax 619-291-4165

\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 July 2009 \*  
\* 100-yr Post-project (on-site) \*  
\* Drainage Basin 8000B (Undetained) \*  
\*\*\*\*\*

FILE NAME: MW82K100.DAT  
TIME/DATE OF STUDY: 11:48 07/14/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT (YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE (INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.90  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

NO.	HALF- WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	18.0	13.0	0.020/0.020/0.020	0.50	1.50	0.0100	0.125	0.0180

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*

FLOW PROCESS FROM NODE 8200.00 TO NODE 8201.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
=====

\*USER SPECIFIED (SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 760.00  
 DOWNSTREAM ELEVATION(FEET) = 690.00  
 ELEVATION DIFFERENCE(FEET) = 70.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.200  
 SUBAREA RUNOFF(CFS) = 0.86  
 TOTAL AREA(ACRES) = 0.30 TOTAL RUNOFF(CFS) = 0.86

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8201.00 TO NODE 8202.00 IS CODE = 51  
 -----

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 690.00 DOWNSTREAM(FEET) = 310.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 620.00 CHANNEL SLOPE = 0.6129  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 10.000  
 MANNING'S FACTOR = 0.035 MAXIMUM DEPTH(FEET) = 10.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.419  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3400  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 1.53  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.57  
 AVERAGE FLOW DEPTH(FEET) = 0.04 TRAVEL TIME(MIN.) = 2.89  
 Tc(MIN.) = 9.16  
 SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 1.31  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.343  
 TOTAL AREA(ACRES) = 0.90 PEAK FLOW RATE(CFS) = 1.98

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.05 FLOW VELOCITY(FEET/SEC.) = 3.89  
 LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8202.00 = 720.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8202.00 TO NODE 8203.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 310.00 DOWNSTREAM(FEET) = 277.00  
 FLOW LENGTH(FEET) = 900.00 MANNING'S N = 0.016  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 4.4 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.02  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 1.98  
 PIPE TRAVEL TIME(MIN.) = 2.49 Tc(MIN.) = 11.65  
 LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8203.00 = 1620.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8202.00 TO NODE 8203.00 IS CODE = 81  
 -----

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<  
 =====

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.496  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3300  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.3309  
 SUBAREA AREA(ACRES) = 11.80 SUBAREA RUNOFF(CFS) = 21.40  
 TOTAL AREA(ACRES) = 12.70 TOTAL RUNOFF(CFS) = 23.10  
 TC(MIN.) = 11.65

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8203.00 TO NODE 8203.00 IS CODE = 10  
 -----

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8216.00 TO NODE 8217.00 IS CODE = 21  
 -----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<  
 =====

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
 UPSTREAM ELEVATION(FEET) = 286.20  
 DOWNSTREAM ELEVATION(FEET) = 285.50  
 ELEVATION DIFFERENCE(FEET) = 0.70  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.672  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.46  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.46

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8217.00 TO NODE 8218.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<  
 =====

UPSTREAM ELEVATION(FEET) = 285.50 DOWNSTREAM ELEVATION(FEET) = 284.00  
 STREET LENGTH(FEET) = 180.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.00  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.29  
 HALFSTREET FLOOD WIDTH(FEET) = 9.19  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 1.61

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.47  
 STREET FLOW TRAVEL TIME(MIN.) = 1.86 Tc(MIN.) = 6.53  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.982  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA(ACRES) = 0.50 SUBAREA RUNOFF(CFS) = 3.07  
 TOTAL AREA(ACRES) = 0.70 PEAK FLOW RATE(CFS) = 4.30

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.32 HALFSTREET FLOOD WIDTH(FEET) = 10.71  
 FLOW VELOCITY(FEET/SEC.) = 1.74 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.56  
 LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8218.00 = 245.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8218.00 TO NODE 8223.00 IS CODE = 62

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====  
 UPSTREAM ELEVATION(FEET) = 283.00 DOWNSTREAM ELEVATION(FEET) = 280.50  
 STREET LENGTH(FEET) = 180.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curb-to-curb) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.78  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.32  
 HALFSTREET FLOOD WIDTH(FEET) = 10.87  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.28  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.73  
 STREET FLOW TRAVEL TIME(MIN.) = 1.32 Tc(MIN.) = 7.85  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.091

\*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4600  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.596  
 SUBAREA AREA(ACRES) = 0.90 SUBAREA RUNOFF(CFS) = 2.94  
 TOTAL AREA(ACRES) = 1.60 PEAK FLOW RATE(CFS) = 6.76

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.34 HALFSTREET FLOOD WIDTH(FEET) = 11.58  
 FLOW VELOCITY(FEET/SEC.) = 2.37 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.80  
 LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8223.00 = 425.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8223.00 TO NODE 8224.00 IS CODE = 31



>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 270.50 DOWNSTREAM(FEET) = 268.50  
FLOW LENGTH(FEET) = 30.00 MANNING'S N = 0.013  
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 6.3 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 12.28  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 6.76  
PIPE TRAVEL TIME(MIN.) = 0.04 Tc(MIN.) = 7.89  
LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8224.00 = 455.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8224.00 TO NODE 8224.00 IS CODE = 1

-----

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
TIME OF CONCENTRATION(MIN.) = 7.89  
RAINFALL INTENSITY(INCH/HR) = 7.07  
TOTAL STREAM AREA(ACRES) = 1.60  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.76

\*\*\*\*\*

FLOW PROCESS FROM NODE 8220.00 TO NODE 8221.00 IS CODE = 21

-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 75.00  
UPSTREAM ELEVATION(FEET) = 281.50  
DOWNSTREAM ELEVATION(FEET) = 280.50  
ELEVATION DIFFERENCE(FEET) = 1.00  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.674  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.46  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.46

\*\*\*\*\*

FLOW PROCESS FROM NODE 8221.00 TO NODE 8222.00 IS CODE = 62

-----

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<  
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 280.00 DOWNSTREAM ELEVATION(FEET) = 276.50  
STREET LENGTH(FEET) = 110.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.56  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.25  
 HALFSTREET FLOOD WIDTH(FEET) = 7.41  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.80  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.71  
 STREET FLOW TRAVEL TIME(MIN.) = 0.65 Tc(MIN.) = 5.33  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.104  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 4.21  
 TOTAL AREA(ACRES) = 0.80 PEAK FLOW RATE(CFS) = 5.61

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.29 HALFSTREET FLOOD WIDTH(FEET) = 9.04  
 FLOW VELOCITY(FEET/SEC.) = 3.11 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.89  
 LONGEST FLOWPATH FROM NODE 8220.00 TO NODE 8222.00 = 185.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8222.00 TO NODE 8224.00 IS CODE = 31  
 -----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 270.50 DOWNSTREAM(FEET) = 268.50  
 FLOW LENGTH(FEET) = 225.00 MANNING'S N = 0.013  
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000  
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.0 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 5.56  
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 5.61  
 PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 6.00  
 LONGEST FLOWPATH FROM NODE 8220.00 TO NODE 8224.00 = 410.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8224.00 TO NODE 8224.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.00  
 RAINFALL INTENSITY(INCH/HR) = 8.43  
 TOTAL STREAM AREA(ACRES) = 0.80  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.61

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	4.21	5.33	9.104	0.60
2	5.61	6.00	8.43	0.80

1	6.76	7.89	7.068	1.60
2	5.61	6.00	8.430	0.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	10.75	6.00	8.430
2	11.46	7.89	7.068

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 11.46 Tc(MIN.) = 7.89

TOTAL AREA(ACRES) = 2.40

LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8224.00 = 455.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8224.00 TO NODE 8228.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 268.50 DOWNSTREAM(FEET) = 266.50

FLOW LENGTH(FEET) = 340.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 21.0 INCH PIPE IS 17.1 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 5.46

ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 11.46

PIPE TRAVEL TIME(MIN.) = 1.04 Tc(MIN.) = 8.93

LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8228.00 = 795.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8228.00 TO NODE 8228.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 8.93

RAINFALL INTENSITY(INCH/HR) = 6.53

TOTAL STREAM AREA(ACRES) = 2.40

PEAK FLOW RATE(CFS) AT CONFLUENCE = 11.46

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8226.00 TO NODE 8227.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00

UPSTREAM ELEVATION(FEET) = 282.70

DOWNSTREAM ELEVATION(FEET) = 282.00

ELEVATION DIFFERENCE(FEET) = 0.70

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.672

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.  
 SUBAREA RUNOFF(CFS) = 1.46  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.46

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8227.00 TO NODE 8228.00 IS CODE = 62  
 -----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>(STREET TABLE SECTION # 1 USED)<<<<  
 =====

UPSTREAM ELEVATION(FEET) = 282.00 DOWNSTREAM ELEVATION(FEET) = 279.00  
 STREET LENGTH(FEET) = 275.00 CURB HEIGHT(INCHES) = 6.0  
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.03  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH(FEET) = 0.32  
 HALFSTREET FLOOD WIDTH(FEET) = 10.81  
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.00  
 PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.64  
 STREET FLOW TRAVEL TIME(MIN.) = 2.29 Tc(MIN.) = 6.96  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.662  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA(ACRES) = 1.20 SUBAREA RUNOFF(CFS) = 7.08  
 TOTAL AREA(ACRES) = 1.40 PEAK FLOW RATE(CFS) = 8.26

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 13.20  
 FLOW VELOCITY(FEET/SEC.) = 2.26 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.83  
 LONGEST FLOWPATH FROM NODE 8226.00 TO NODE 8228.00 = 340.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8228.00 TO NODE 8228.00 IS CODE = 1  
 -----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 6.96  
 RAINFALL INTENSITY(INCH/HR) = 7.66  
 TOTAL STREAM AREA(ACRES) = 1.40  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.26

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	11.46	8.93	6.526	2.40
2	8.26	6.96	7.662	1.40

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	18.02	6.96	7.662
2	18.50	8.93	6.526

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 18.50 Tc(MIN.) = 8.93

TOTAL AREA(ACRES) = 3.80

LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8228.00 = 795.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8228.00 TO NODE 8233.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM( FEET) = 266.50 DOWNSTREAM( FEET) = 266.00

FLOW LENGTH( FEET) = 100.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 27.0 INCH PIPE IS 19.8 INCHES

PIPE-FLOW VELOCITY( FEET/SEC.) = 5.91

ESTIMATED PIPE DIAMETER( INCH) = 27.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 18.50

PIPE TRAVEL TIME( MIN.) = 0.28 Tc( MIN.) = 9.21

LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8233.00 = 895.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 8233.00 TO NODE 8233.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION( MIN.) = 9.21

RAINFALL INTENSITY( INCH/HR) = 6.40

TOTAL STREAM AREA( ACRES) = 3.80

PEAK FLOW RATE( CFS) AT CONFLUENCE = 18.50

\*\*\*\*\*

FLOW PROCESS FROM NODE 8235.00 TO NODE 8236.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

\*USER SPECIFIED( SUBAREA) :

USER-SPECIFIED RUNOFF COEFFICIENT = .7700

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH( FEET) = 65.00

UPSTREAM ELEVATION( FEET) = 285.70

DOWNSTREAM ELEVATION (FEET) = 285.00  
 ELEVATION DIFFERENCE (FEET) = 0.70  
 SUBAREA OVERLAND TIME OF FLOW (MIN.) = 4.672  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.485  
 NOTE: RAINFALL INTENSITY IS BASED ON  $T_c = 5$ -MINUTE.  
 SUBAREA RUNOFF (CFS) = 1.46  
 TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 1.46

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8236.00 TO NODE 8233.00 IS CODE = 62  
 -----

>>>> COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA <<<<  
 >>>> (STREET TABLE SECTION # 1 USED) <<<<

=====  
 UPSTREAM ELEVATION (FEET) = 285.00 DOWNSTREAM ELEVATION (FEET) = 279.50  
 STREET LENGTH (FEET) = 675.00 CURB HEIGHT (INCHES) = 6.0  
 STREET HALFWIDTH (FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK (FEET) = 13.00  
 INSIDE STREET CROSSFALL (DECIMAL) = 0.020  
 OUTSIDE STREET CROSSFALL (DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
 STREET PARKWAY CROSSFALL (DECIMAL) = 0.020  
 Manning's FRICTION FACTOR for Streetflow Section (curb-to-curb) = 0.0180  
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 12.85  
 STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
 STREET FLOW DEPTH (FEET) = 0.44  
 HALFSTREET FLOOD WIDTH (FEET) = 16.60  
 AVERAGE FLOW VELOCITY (FEET/SEC.) = 2.26  
 PRODUCT OF DEPTH&VELOCITY (FT\*FT/SEC.) = 0.99  
 STREET FLOW TRAVEL TIME (MIN.) = 4.98  $T_c$  (MIN.) = 9.65  
 100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 6.206  
 \*USER SPECIFIED (SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.770  
 SUBAREA AREA (ACRES) = 4.60 SUBAREA RUNOFF (CFS) = 21.98  
 TOTAL AREA (ACRES) = 4.80 PEAK FLOW RATE (CFS) = 22.94

END OF SUBAREA STREET FLOW HYDRAULICS:  
 DEPTH (FEET) = 0.51 HALFSTREET FLOOD WIDTH (FEET) = 18.60  
 FLOW VELOCITY (FEET/SEC.) = 2.75 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.41  
 \*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,  
 AND  $L = 675.0$  FT WITH ELEVATION-DROP = 5.5 FT, IS 33.5 CFS,  
 WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 8233.00  
 LONGEST FLOWPATH FROM NODE 8235.00 TO NODE 8233.00 = 740.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8233.00 TO NODE 8233.00 IS CODE = 1  
 -----

>>>> DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE <<<<  
 >>>> AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES <<<<

=====  
 TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.65  
 RAINFALL INTENSITY(INCH/HR) = 6.21  
 TOTAL STREAM AREA(ACRES) = 4.80  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 22.94

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	18.50	9.21	6.397	3.80
2	22.94	9.65	6.206	4.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	40.38	9.21	6.397
2	40.88	9.65	6.206

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 40.88 Tc(MIN.) = 9.65  
 TOTAL AREA(ACRES) = 8.60  
 LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8233.00 = 895.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8233.00 TO NODE 8237.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 266.00 DOWNSTREAM(FEET) = 265.00  
 FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 22.6 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 9.42  
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 40.88  
 PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 9.83  
 LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8237.00 = 995.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8237.00 TO NODE 8237.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:  
 TIME OF CONCENTRATION(MIN.) = 9.83  
 RAINFALL INTENSITY(INCH/HR) = 6.13  
 TOTAL STREAM AREA(ACRES) = 8.60  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 40.88

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8230.00 TO NODE 8231.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

```

=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .8700
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00
UPSTREAM ELEVATION(FEET) = 282.70
DOWNSTREAM ELEVATION(FEET) = 282.00
ELEVATION DIFFERENCE(FEET) = 0.70
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.256
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.65
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.65

*****
FLOW PROCESS FROM NODE 8231.00 TO NODE 8232.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 282.00 DOWNSTREAM ELEVATION(FEET) = 278.50
STREET LENGTH(FEET) = 270.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.54
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.32
HALFSTREET FLOOD WIDTH(FEET) = 10.87
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.19
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 0.71
STREET FLOW TRAVEL TIME(MIN.) = 2.06 Tc(MIN.) = 5.31
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.121
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .7700
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.785
SUBAREA AREA(ACRES) = 1.10 SUBAREA RUNOFF(CFS) = 7.73
TOTAL AREA(ACRES) = 1.30 PEAK FLOW RATE(CFS) = 9.31

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.37 HALFSTREET FLOOD WIDTH(FEET) = 13.35
FLOW VELOCITY(FEET/SEC.) = 2.49 DEPTH*VELOCITY(FT*FT/SEC.) = 0.93
LONGEST FLOWPATH FROM NODE 8230.00 TO NODE 8232.00 = 335.00 FEET.

*****
FLOW PROCESS FROM NODE 8232.00 TO NODE 8237.00 IS CODE = 31
-----
>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

```



>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 265.50 DOWNSTREAM(FEET) = 265.00  
FLOW LENGTH(FEET) = 50.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.8 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 6.42  
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 9.31  
PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 5.44  
LONGEST FLOWPATH FROM NODE 8230.00 TO NODE 8237.00 = 385.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8237.00 TO NODE 8237.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

-----  
TOTAL NUMBER OF STREAMS = 2  
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
TIME OF CONCENTRATION(MIN.) = 5.44  
RAINFALL INTENSITY(INCH/HR) = 8.98  
TOTAL STREAM AREA(ACRES) = 1.30  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 9.31

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	40.88	9.83	6.134	8.60
2	9.31	5.44	8.980	1.30

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	37.24	5.44	8.980
2	47.24	9.83	6.134

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 47.24 Tc(MIN.) = 9.83  
TOTAL AREA(ACRES) = 9.90  
LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8237.00 = 995.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8237.00 TO NODE 8242.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

-----  
ELEVATION DATA: UPSTREAM(FEET) = 265.00 DOWNSTREAM(FEET) = 264.00  
FLOW LENGTH(FEET) = 110.00 MANNING'S N = 0.013  
DEPTH OF FLOW IN 33.0 INCH PIPE IS 26.7 INCHES  
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.18  
ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1  
PIPE-FLOW(CFS) = 47.24  
PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 10.03

```

LONGEST FLOWPATH FROM NODE    8216.00 TO NODE    8242.00 = 1105.00 FEET.

*****
FLOW PROCESS FROM NODE    8242.00 TO NODE    8242.00 IS CODE = 10
-----
>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<
=====

*****
FLOW PROCESS FROM NODE    8204.10 TO NODE    8204.20 IS CODE = 21
-----
>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 60.00
UPSTREAM ELEVATION(FEET) = 284.00
DOWNSTREAM ELEVATION(FEET) = 283.00
ELEVATION DIFFERENCE(FEET) = 1.00
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 2.352
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
SUBAREA RUNOFF(CFS) = 1.71
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.71

*****
FLOW PROCESS FROM NODE    8204.20 TO NODE    8204.00 IS CODE = 62
-----
>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>>(STREET TABLE SECTION # 1 USED)<<<<<
=====
UPSTREAM ELEVATION(FEET) = 283.00 DOWNSTREAM ELEVATION(FEET) = 280.00
STREET LENGTH(FEET) = 23.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 4.27
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.22
HALFSTREET FLOOD WIDTH(FEET) = 5.79
AVERAGE FLOW VELOCITY(FEET/SEC.) = 5.07
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.12
STREET FLOW TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 2.43
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485
NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .9000
S.C.S. CURVE NUMBER (AMC II) = 0

```

AREA-AVERAGE RUNOFF COEFFICIENT = 0.900  
 SUBAREA AREA (ACRES) = 0.60 SUBAREA RUNOFF (CFS) = 5.12  
 TOTAL AREA (ACRES) = 0.80 PEAK FLOW RATE (CFS) = 6.83

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH (FEET) = 0.25 HALFSTREET FLOOD WIDTH (FEET) = 7.26  
 FLOW VELOCITY (FEET/SEC.) = 5.57 DEPTH\*VELOCITY (FT\*FT/SEC.) = 1.39  
 LONGEST FLOWPATH FROM NODE 8204.10 TO NODE 8204.00 = 83.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8204.00 TO NODE 8204.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	6.83	2.43	9.485	0.80

LONGEST FLOWPATH FROM NODE 8204.10 TO NODE 8204.00 = 83.00 FEET.

\*\* MEMORY BANK # 1 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	23.10	11.65	5.496	12.70

LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8204.00 = 1620.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	11.64	2.43	9.485
2	27.06	11.65	5.496

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 27.06 Tc (MIN.) = 11.65  
 TOTAL AREA (ACRES) = 13.50

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8204.00 TO NODE 8204.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8204.00 TO NODE 8242.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM (FEET) = 271.00 DOWNSTREAM (FEET) = 264.00  
 FLOW LENGTH (FEET) = 700.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 27.0 INCH PIPE IS 20.4 INCHES  
 PIPE-FLOW VELOCITY (FEET/SEC.) = 8.40  
 ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1  
 PIPE-FLOW (CFS) = 27.06  
 PIPE TRAVEL TIME (MIN.) = 1.39 Tc (MIN.) = 13.04  
 LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8242.00 = 2320.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8242.00 TO NODE 8242.00 IS CODE = 11

-----  
 >>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<  
 =====

\*\* MAIN STREAM CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	27.06	13.04	5.111	13.50

LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8242.00 = 2320.00 FEET.

\*\* MEMORY BANK # 2 CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	47.24	10.03	6.055	9.90

LONGEST FLOWPATH FROM NODE 8216.00 TO NODE 8242.00 = 1105.00 FEET.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	68.05	10.03	6.055
2	66.94	13.04	5.111

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 68.05 Tc(MIN.) = 10.03  
 TOTAL AREA(ACRES) = 23.40

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8242.00 TO NODE 8242.00 IS CODE = 12

-----  
 >>>>CLEAR MEMORY BANK # 2 <<<<  
 =====

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8242.00 TO NODE 8247.00 IS CODE = 31

-----  
 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<  
 =====

ELEVATION DATA: UPSTREAM(FEET) = 265.00 DOWNSTREAM(FEET) = 264.00  
 FLOW LENGTH(FEET) = 260.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 45.0 INCH PIPE IS 35.2 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 7.33  
 ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 68.05  
 PIPE TRAVEL TIME(MIN.) = 0.59 Tc(MIN.) = 10.62  
 LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8247.00 = 2580.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8247.00 TO NODE 8247.00 IS CODE = 1

-----  
 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 =====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 10.62  
RAINFALL INTENSITY(INCH/HR) = 5.84  
TOTAL STREAM AREA(ACRES) = 23.40  
PEAK FLOW RATE(CFS) AT CONFLUENCE = 68.05

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8244.00 TO NODE 8245.00 IS CODE = 21  
-----

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<  
=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .8700  
S.C.S. CURVE NUMBER (AMC II) = 0  
INITIAL SUBAREA FLOW-LENGTH(FEET) = 65.00  
UPSTREAM ELEVATION(FEET) = 284.70  
DOWNSTREAM ELEVATION(FEET) = 284.00  
ELEVATION DIFFERENCE(FEET) = 0.70  
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 3.256  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485  
NOTE: RAINFALL INTENSITY IS BASED ON  $T_c$  = 5-MINUTE.  
SUBAREA RUNOFF(CFS) = 1.65  
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.65

\*\*\*\*\*  
FLOW PROCESS FROM NODE 8245.00 TO NODE 8247.00 IS CODE = 62  
-----

>>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>(STREET TABLE SECTION # 1 USED)<<<<<  
=====

UPSTREAM ELEVATION(FEET) = 284.00 DOWNSTREAM ELEVATION(FEET) = 280.50  
STREET LENGTH(FEET) = 350.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 2  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 10.05  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.40  
HALFSTREET FLOOD WIDTH(FEET) = 14.52  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.29  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.90  
STREET FLOW TRAVEL TIME(MIN.) = 2.55  $T_c$ (MIN.) = 5.81  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.614

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.777  
SUBAREA AREA(ACRES) = 2.50 SUBAREA RUNOFF(CFS) = 16.58  
TOTAL AREA(ACRES) = 2.70 PEAK FLOW RATE(CFS) = 18.08

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.47 HALFSTREET FLOOD WIDTH(FEET) = 18.00  
 FLOW VELOCITY(FEET/SEC.) = 2.66 DEPTH\*VELOCITY(FT\*FT/SEC.) = 1.25  
 LONGEST FLOWPATH FROM NODE 8244.00 TO NODE 8247.00 = 415.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8247.00 TO NODE 8247.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2  
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:  
 TIME OF CONCENTRATION(MIN.) = 5.81  
 RAINFALL INTENSITY(INCH/HR) = 8.61  
 TOTAL STREAM AREA(ACRES) = 2.70  
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 18.08

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	68.05	10.62	5.835	23.40
2	18.08	5.81	8.614	2.70

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	55.29	5.81	8.614
2	80.30	10.62	5.835

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 80.30 Tc(MIN.) = 10.62  
 TOTAL AREA(ACRES) = 26.10  
 LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8247.00 = 2580.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 8247.00 TO NODE 8248.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<  
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 262.50 DOWNSTREAM(FEET) = 262.00  
 FLOW LENGTH(FEET) = 100.00 MANNING'S N = 0.013  
 DEPTH OF FLOW IN 45.0 INCH PIPE IS 36.5 INCHES  
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.37  
 ESTIMATED PIPE DIAMETER(INCH) = 45.00 NUMBER OF PIPES = 1  
 PIPE-FLOW(CFS) = 80.30  
 PIPE TRAVEL TIME(MIN.) = 0.20 Tc(MIN.) = 10.82  
 LONGEST FLOWPATH FROM NODE 8200.00 TO NODE 8248.00 = 2680.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 26.10 TC(MIN.) = 10.82  
 PEAK FLOW RATE(CFS) = 80.30

---

END OF RATIONAL METHOD ANALYSIS

## **Drainage Basin 9000**



\*\*\*\*\*

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE  
Reference: SAN DIEGO COUNTY FLOOD CONTROL DISTRICT  
2003,1985,1981 HYDROLOGY MANUAL  
(c) Copyright 1982-2003 Advanced Engineering Software (aes)  
Ver. 1.5A Release Date: 01/01/2003 License ID 1261

Analysis prepared by:

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\*\*\*\*\* DESCRIPTION OF STUDY \*\*\*\*\*  
\* MEADOWOOD J-15956 05/13/2009 \*  
\* 100-yr Post-Project \*  
\* Drainage Basin 9000 \*  
\*\*\*\*\*

FILE NAME: B9000.DAT  
TIME/DATE OF STUDY: 09:39 05/15/2009

-----  
USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:  
-----

2003 SAN DIEGO MANUAL CRITERIA

USER SPECIFIED STORM EVENT(YEAR) = 100.00  
6-HOUR DURATION PRECIPITATION (INCHES) = 3.600  
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00  
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.95  
SAN DIEGO HYDROLOGY MANUAL "C"-VALUES USED FOR RATIONAL METHOD  
NOTE: USE MODIFIED RATIONAL METHOD PROCEDURES FOR CONFLUENCE ANALYSIS

\*USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL\*

	HALF- WIDTH	CROWN TO CROSSFALL	STREET-CROSSFALL: IN- / OUT- / PARK- SIDE / SIDE / WAY	CURB HEIGHT	GUTTER-GEOMETRIES: WIDTH	LIP	HIKE	MANNING FACTOR
NO.	(FT)	(FT)		(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.00 FEET  
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)\*(Velocity) Constraint = 6.0 (FT\*FT/S)

\*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN  
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.\*

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9001.00 TO NODE 9005.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .3500  
S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00  
 UPSTREAM ELEVATION(FEET) = 710.00  
 DOWNSTREAM ELEVATION(FEET) = 640.00  
 ELEVATION DIFFERENCE(FEET) = 70.00  
 SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.267  
 WARNING: THE MAXIMUM OVERLAND FLOW SLOPE, 10.%, IS USED IN Tc CALCULATION!  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.200  
 SUBAREA RUNOFF(CFS) = 0.57  
 TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 0.57

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 9005.00 TO NODE 9010.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 640.00 DOWNSTREAM(FEET) = 275.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 980.00 CHANNEL SLOPE = 0.3724  
 CHANNEL BASE(FEET) = 10.00 "Z" FACTOR = 99.000  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 1.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.164  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .3400  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 7.56  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.69  
 AVERAGE FLOW DEPTH(FEET) = 0.09 TRAVEL TIME(MIN.) = 3.49  
 Tc(MIN.) = 9.75  
 SUBAREA AREA(ACRES) = 6.60 SUBAREA RUNOFF(CFS) = 13.83  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.340  
 TOTAL AREA(ACRES) = 6.80 PEAK FLOW RATE(CFS) = 14.26

END OF SUBAREA CHANNEL FLOW HYDRAULICS:  
 DEPTH(FEET) = 0.12 FLOW VELOCITY(FEET/SEC.) = 5.49  
 LONGEST FLOWPATH FROM NODE 9001.00 TO NODE 9010.00 = 1080.00 FEET.

\*\*\*\*\*  
 FLOW PROCESS FROM NODE 9010.00 TO NODE 9015.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<  
 >>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<<

=====  
 ELEVATION DATA: UPSTREAM(FEET) = 275.00 DOWNSTREAM(FEET) = 268.00  
 CHANNEL LENGTH THRU SUBAREA(FEET) = 650.00 CHANNEL SLOPE = 0.0108  
 CHANNEL BASE(FEET) = 2.00 "Z" FACTOR = 1.500  
 MANNING'S FACTOR = 0.030 MAXIMUM DEPTH(FEET) = 2.00  
 100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 5.321  
 \*USER SPECIFIED(SUBAREA):  
 USER-SPECIFIED RUNOFF COEFFICIENT = .4900  
 S.C.S. CURVE NUMBER (AMC II) = 0  
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 22.85  
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.34  
 AVERAGE FLOW DEPTH(FEET) = 1.32 TRAVEL TIME(MIN.) = 2.50  
 Tc(MIN.) = 12.25  
 SUBAREA AREA(ACRES) = 6.60 SUBAREA RUNOFF(CFS) = 17.21  
 AREA-AVERAGE RUNOFF COEFFICIENT = 0.414  
 TOTAL AREA(ACRES) = 13.40 PEAK FLOW RATE(CFS) = 29.52

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH (FEET) = 1.50 FLOW VELOCITY (FEET/SEC.) = 4.64

LONGEST FLOWPATH FROM NODE 9001.00 TO NODE 9015.00 = 1730.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 9015.00 TO NODE 9027.00 IS CODE = 31

-----  
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 268.00 DOWNSTREAM (FEET) = 267.90

FLOW LENGTH (FEET) = 12.50 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.8 INCHES

PIPE-FLOW VELOCITY (FEET/SEC.) = 8.14

ESTIMATED PIPE DIAMETER (INCH) = 30.00 NUMBER OF PIPES = 1

PIPE-FLOW (CFS) = 29.52

PIPE TRAVEL TIME (MIN.) = 0.03 Tc (MIN.) = 12.28

LONGEST FLOWPATH FROM NODE 9001.00 TO NODE 9027.00 = 1742.50 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 9027.00 TO NODE 9027.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION (MIN.) = 12.28

RAINFALL INTENSITY (INCH/HR) = 5.31

TOTAL STREAM AREA (ACRES) = 13.40

PEAK FLOW RATE (CFS) AT CONFLUENCE = 29.52

\*\*\*\*\*

FLOW PROCESS FROM NODE 9021.00 TO NODE 9025.00 IS CODE = 21

-----  
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

=====

\*USER SPECIFIED (SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6800

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH (FEET) = 60.00

UPSTREAM ELEVATION (FEET) = 278.10

DOWNSTREAM ELEVATION (FEET) = 277.30

ELEVATION DIFFERENCE (FEET) = 0.80

SUBAREA OVERLAND TIME OF FLOW (MIN.) = 5.320

100 YEAR RAINFALL INTENSITY (INCH/HOUR) = 9.112

SUBAREA RUNOFF (CFS) = 1.24

TOTAL AREA (ACRES) = 0.20 TOTAL RUNOFF (CFS) = 1.24

\*\*\*\*\*

FLOW PROCESS FROM NODE 9025.00 TO NODE 9027.00 IS CODE = 61

-----  
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>(STANDARD CURB SECTION USED)<<<<

=====

UPSTREAM ELEVATION (FEET) = 277.30 DOWNSTREAM ELEVATION (FEET) = 275.00

STREET LENGTH (FEET) = 216.00 CURB HEIGHT (INCHES) = 6.0

STREET HALFWIDTH(FEET) = 32.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 16.00

INSIDE STREET CROSSFALL(DECIMAL) = 0.020

OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1

STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180

Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.00

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.36

HALFSTREET FLOOD WIDTH(FEET) = 11.50

AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.08

PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.74

STREET FLOW TRAVEL TIME(MIN.) = 1.73 Tc(MIN.) = 7.05

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.599

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .7700

S.C.S. CURVE NUMBER (AMC II) = 0

AREA-AVERAGE RUNOFF COEFFICIENT = 0.748

SUBAREA AREA(ACRES) = 0.60 SUBAREA RUNOFF(CFS) = 3.51

TOTAL AREA(ACRES) = 0.80 PEAK FLOW RATE(CFS) = 4.54

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.65

FLOW VELOCITY(FEET/SEC.) = 2.29 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.92

LONGEST FLOWPATH FROM NODE 9021.00 TO NODE 9027.00 = 276.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 9027.00 TO NODE 9027.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:

TIME OF CONCENTRATION(MIN.) = 7.05

RAINFALL INTENSITY(INCH/HR) = 7.60

TOTAL STREAM AREA(ACRES) = 0.80

PEAK FLOW RATE(CFS) AT CONFLUENCE = 4.54

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	29.52	12.28	5.314	13.40
2	4.54	7.05	7.599	0.80

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	21.50	7.05	7.599

2            32.70        12.28            5.314

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) =        32.70        Tc(MIN.) =        12.28

TOTAL AREA(ACRES) =        14.20

LONGEST FLOWPATH FROM NODE    9001.00 TO NODE    9027.00 =    1742.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE    9027.00 TO NODE    9037.00 IS CODE =    31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =    267.90    DOWNSTREAM(FEET) =    267.00

FLOW LENGTH(FEET) =        90.00        MANNING'S N =    0.013

DEPTH OF FLOW IN    30.0 INCH PIPE IS    20.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) =    9.08

ESTIMATED PIPE DIAMETER(INCH) =    30.00        NUMBER OF PIPES =    1

PIPE-FLOW(CFS) =        32.70

PIPE TRAVEL TIME(MIN.) =    0.17        Tc(MIN.) =    12.44

LONGEST FLOWPATH FROM NODE    9001.00 TO NODE    9037.00 =    1832.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE    9037.00 TO NODE    9037.00 IS CODE =    1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =    2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM    1 ARE:

TIME OF CONCENTRATION(MIN.) =    12.44

RAINFALL INTENSITY(INCH/HR) =    5.27

TOTAL STREAM AREA(ACRES) =    14.20

PEAK FLOW RATE(CFS) AT CONFLUENCE =        32.70

\*\*\*\*\*  
FLOW PROCESS FROM NODE    9031.00 TO NODE    9035.00 IS CODE =    21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA) :

USER-SPECIFIED RUNOFF COEFFICIENT = .5900

S.C.S. CURVE NUMBER (AMC II) =    0

INITIAL SUBAREA FLOW-LENGTH(FEET) =        70.00

UPSTREAM ELEVATION(FEET) =        278.70

DOWNSTREAM ELEVATION(FEET) =        277.50

ELEVATION DIFFERENCE(FEET) =        1.20

SUBAREA OVERLAND TIME OF FLOW(MIN.) =        6.418

100 YEAR RAINFALL INTENSITY(INCH/HOUR) =    8.075

SUBAREA RUNOFF(CFS) =        0.95

TOTAL AREA(ACRES) =        0.20        TOTAL RUNOFF(CFS) =        0.95

\*\*\*\*\*  
FLOW PROCESS FROM NODE    9035.00 TO NODE    9037.00 IS CODE =    61  
-----

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>(STANDARD CURB SECTION USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 277.50 DOWNSTREAM ELEVATION(FEET) = 275.00  
STREET LENGTH(FEET) = 246.00 CURB HEIGHT(INCHES) = 6.0  
STREET HALFWIDTH(FEET) = 44.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 22.00  
INSIDE STREET CROSSFALL(DECIMAL) = 0.020  
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1  
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020  
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0180  
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

\*\*TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.87  
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:  
STREET FLOW DEPTH(FEET) = 0.35  
HALFSTREET FLOOD WIDTH(FEET) = 11.39  
AVERAGE FLOW VELOCITY(FEET/SEC.) = 2.03  
PRODUCT OF DEPTH&VELOCITY(FT\*FT/SEC.) = 0.72  
STREET FLOW TRAVEL TIME(MIN.) = 2.02 Tc(MIN.) = 8.44  
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 6.768  
\*USER SPECIFIED(SUBAREA):  
USER-SPECIFIED RUNOFF COEFFICIENT = .7100  
S.C.S. CURVE NUMBER (AMC II) = 0  
AREA-AVERAGE RUNOFF COEFFICIENT = 0.686  
SUBAREA AREA(ACRES) = 0.80 SUBAREA RUNOFF(CFS) = 3.84  
TOTAL AREA(ACRES) = 1.00 PEAK FLOW RATE(CFS) = 4.64

END OF SUBAREA STREET FLOW HYDRAULICS:  
DEPTH(FEET) = 0.40 HALFSTREET FLOOD WIDTH(FEET) = 13.87  
FLOW VELOCITY(FEET/SEC.) = 2.27 DEPTH\*VELOCITY(FT\*FT/SEC.) = 0.92  
LONGEST FLOWPATH FROM NODE 9031.00 TO NODE 9037.00 = 316.00 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9037.00 TO NODE 9037.00 IS CODE = 1

-----  
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<  
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

=====

TOTAL NUMBER OF STREAMS	=	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM	2 ARE:	
TIME OF CONCENTRATION(MIN.)	=	8.44
RAINFALL INTENSITY(INCH/HR)	=	6.77
TOTAL STREAM AREA(ACRES)	=	1.00
PEAK FLOW RATE(CFS) AT CONFLUENCE	=	4.64

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	32.70	12.44	5.268	14.20
2	4.64	8.44	6.768	1.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO  
CONFLUENCE FORMULA USED FOR 2 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM	RUNOFF	Tc	INTENSITY
--------	--------	----	-----------

NUMBER	(CFS)	(MIN.)	(INCH/HOUR)
1	30.10	8.44	6.768
2	36.31	12.44	5.268

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 36.31 Tc(MIN.) = 12.44

TOTAL AREA(ACRES) = 15.20

LONGEST FLOWPATH FROM NODE 9001.00 TO NODE 9037.00 = 1832.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9037.00 TO NODE 9077.00 IS CODE = 31  
-----

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 267.00 DOWNSTREAM(FEET) = 262.74

FLOW LENGTH(FEET) = 788.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.9 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 7.27

ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 36.31

PIPE TRAVEL TIME(MIN.) = 1.81 Tc(MIN.) = 14.25

LONGEST FLOWPATH FROM NODE 9001.00 TO NODE 9077.00 = 2620.50 FEET.

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9077.00 TO NODE 9077.00 IS CODE = 1  
-----

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 14.25

RAINFALL INTENSITY(INCH/HR) = 4.83

TOTAL STREAM AREA(ACRES) = 15.20

PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.31

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9041.00 TO NODE 9047.00 IS CODE = 21  
-----

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<

=====

\*USER SPECIFIED(SUBAREA):

USER-SPECIFIED RUNOFF COEFFICIENT = .6000

S.C.S. CURVE NUMBER (AMC II) = 0

INITIAL SUBAREA FLOW-LENGTH(FEET) = 100.00

UPSTREAM ELEVATION(FEET) = 284.10

DOWNSTREAM ELEVATION(FEET) = 277.00

ELEVATION DIFFERENCE(FEET) = 7.10

SUBAREA OVERLAND TIME OF FLOW(MIN.) = 4.683

100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 9.485

NOTE: RAINFALL INTENSITY IS BASED ON Tc = 5-MINUTE.

SUBAREA RUNOFF(CFS) = 2.28

TOTAL AREA(ACRES) = 0.40 TOTAL RUNOFF(CFS) = 2.28

\*\*\*\*\*  
FLOW PROCESS FROM NODE 9047.00 TO NODE 9077.00 IS CODE = 31  
-----

```

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 271.50 DOWNSTREAM(FEET) = 262.74
FLOW LENGTH(FEET) = 867.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 5.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.68
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 2.28
PIPE TRAVEL TIME(MIN.) = 3.09 Tc(MIN.) = 7.77
LONGEST FLOWPATH FROM NODE 9041.00 TO NODE 9077.00 = 967.00 FEET.

*****
FLOW PROCESS FROM NODE 9051.00 TO NODE 9077.00 IS CODE = 81
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 7.136
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6600
S.C.S. CURVE NUMBER (AMC II) = 0
AREA-AVERAGE RUNOFF COEFFICIENT = 0.6429
SUBAREA AREA(ACRES) = 1.00 SUBAREA RUNOFF(CFS) = 4.71
TOTAL AREA(ACRES) = 1.40 TOTAL RUNOFF(CFS) = 6.42
TC(MIN.) = 7.77

*****
FLOW PROCESS FROM NODE 9077.00 TO NODE 9077.00 IS CODE = .1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 3
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 7.77
RAINFALL INTENSITY(INCH/HR) = 7.14
TOTAL STREAM AREA(ACRES) = 1.40
PEAK FLOW RATE(CFS) AT CONFLUENCE = 6.42

*****
FLOW PROCESS FROM NODE 9061.00 TO NODE 9065.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
=====
*USER SPECIFIED(SUBAREA):
USER-SPECIFIED RUNOFF COEFFICIENT = .6800
S.C.S. CURVE NUMBER (AMC II) = .0
INITIAL SUBAREA FLOW-LENGTH(FEET) = 50.00
UPSTREAM ELEVATION(FEET) = 275.60
DOWNSTREAM ELEVATION(FEET) = 275.30
ELEVATION DIFFERENCE(FEET) = 0.30
SUBAREA OVERLAND TIME OF FLOW(MIN.) = 6.338
100 YEAR RAINFALL INTENSITY(INCH/HOUR) = 8.140
SUBAREA RUNOFF(CFS) = 1.11
TOTAL AREA(ACRES) = 0.20 TOTAL RUNOFF(CFS) = 1.11

*****

```



FLOW PROCESS FROM NODE 9065.00 TO NODE 9077.00 IS CODE = 51

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<

>>>>TRAVELTIME THRU SUBAREA (EXISTING ELEMENT)<<<<

ELEVATION DATA: UPSTREAM( FEET ) = 275.30 DOWNSTREAM( FEET ) = 272.00  
CHANNEL LENGTH THRU SUBAREA( FEET ) = 645.00 CHANNEL SLOPE = 0.0051  
CHANNEL BASE( FEET ) = 1.00 "Z" FACTOR = 4.000  
MANNING'S FACTOR = 0.030 MAXIMUM DEPTH( FEET ) = 1.00  
100 YEAR RAINFALL INTENSITY( INCH/HOUR ) = 5.257

\*USER SPECIFIED( SUBAREA ) :

USER-SPECIFIED RUNOFF COEFFICIENT = .6400

S.C.S. CURVE NUMBER (AMC II) = 0

TRAVEL TIME COMPUTED USING ESTIMATED FLOW( CFS ) = 3.70

TRAVEL TIME THRU SUBAREA BASED ON VELOCITY( FEET/SEC. ) = 1.75

AVERAGE FLOW DEPTH( FEET ) = 0.61 TRAVEL TIME( MIN. ) = 6.15

Tc( MIN. ) = 12.48

SUBAREA AREA( ACRES ) = 1.50 SUBAREA RUNOFF( CFS ) = 5.05

AREA-AVERAGE RUNOFF COEFFICIENT = 0.645

TOTAL AREA( ACRES ) = 1.70 PEAK FLOW RATE( CFS ) = 5.76

END OF SUBAREA CHANNEL FLOW HYDRAULICS:

DEPTH( FEET ) = 0.74 FLOW VELOCITY( FEET/SEC. ) = 1.95

LONGEST FLOWPATH FROM NODE 9061.00 TO NODE 9077.00 = 695.00 FEET.

\*\*\*\*\*

FLOW PROCESS FROM NODE 9077.00 TO NODE 9077.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 3

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 3 ARE:

TIME OF CONCENTRATION( MIN. ) = 12.48

RAINFALL INTENSITY( INCH/HR ) = 5.26

TOTAL STREAM AREA( ACRES ) = 1.70

PEAK FLOW RATE( CFS ) AT CONFLUENCE = 5.76

\*\* CONFLUENCE DATA \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)	AREA (ACRE)
1	36.31	14.25	4.827	15.20
2	6.42	7.77	7.136	1.40
3	5.76	12.48	5.257	1.70

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO

CONFLUENCE FORMULA USED FOR 3 STREAMS.

\*\* PEAK FLOW RATE TABLE \*\*

STREAM NUMBER	RUNOFF (CFS)	Tc (MIN.)	INTENSITY (INCH/HOUR)
1	34.57	7.77	7.136
2	43.84	12.48	5.257
3	45.95	14.25	4.827

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE( CFS ) = 45.95 Tc( MIN. ) = 14.25

TOTAL AREA(ACRES) = 18.30  
LONGEST FLOWPATH FROM NODE 9001.00 TO NODE 9077.00 = 2620.50 FEET.

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 18.30 TC(MIN.) = 14.25  
PEAK FLOW RATE(CFS) = 45.95

=====

END OF RATIONAL METHOD ANALYSIS

## **Appendix D**

### **Detention Backup Information**

Rating curve information was obtained from continuous simulation hydrologic modeling for the August 19, 2009 report titled Hydromodification Management Study for Meadowood Vesting Tentative Map

Drainage Basin 2000 Detention Basin (DB2)

		Crest of Riser Notch	Top of Riser	10-year flow
Volume (acre-feet)	0	0.21	0.36	0.53
Flow (cfs)	0	3.65	5.95	36.41
Assumed Elevation (feet)	100	101.95	103	104.01

Drainage Basin 3000 Detention Basin (DB3)

		Crest of Riser Notch	Top of Riser	10-year flow
Volume (acre-feet)	0	2.05	2.62	3.29
Flow (cfs)	0	4.18	10.06	33.13
Assumed Elevation (feet)	100	102.4	103	103.69

Drainage Basin 4000 Detention Basin (DB4)

		Crest of Riser Notch	Top of Riser	10-year flow
Volume (acre-feet)	0	0.72	0.94	1.05
Flow (cfs)	0	0.67	2.76	5.51
Assumed Elevation (feet)	100	102.4	103	103.32

Drainage Basin 7000A Detention Basin (DB7A)

		Crest of Riser Notch	Top of Riser	10-year flow
Volume (acre-feet)	0	9.24	11.95	14.77
Flow (cfs)	0	13.08	31.51	96.4
Assumed Elevation (feet)	100	103.17	104	104.87

Drainage Basin 7000B Detention Basin (DB7B)

		Crest of Riser Notch	Top of Riser	10-year flow
Volume (acre-feet)	0	2.54	3.30	3.69
Flow (cfs)	0	2.64	11.50	21.90
Assumed Elevation (feet)	100	103.17	104	104.41

Drainage Basin 8000A Detention Basin (DB8A)

		Crest of Riser Notch	Top of Riser	10-year flow
Volume (acre-feet)	0	0.65	0.86	1.11
Flow (cfs)	0	1.54	3.90	13.18
Assumed Elevation (feet)	100	102.37	103	103.72

Drainage Basin 8000B Detention Basin (DB8B)

		Crest of Riser Notch	Top of Riser	10-year flow
Volume (acre-feet)	0	1.27	1.63	1.97
Flow (cfs)	0	1.05	3.2	9.4
Assumed Elevation (feet)	100	102.34	103	103.54

## Weighted Runoff Calculations

## Basin 2000A

Node	Area (AC)	RC	AreaxRC
200-2001	0.20	0.30	0.06
2001-2004	10.90	0.30	3.27
2002-2003	0.20	0.30	0.06
2003-2004	6.90	0.30	2.07
2004-2009	4.30	0.29	1.25
2005-2006	0.30	0.30	0.09
2006-2007	2.30	0.30	0.69
2007-2008	13.40	0.30	4.02
2008-2011	6.20	0.28	1.74
2013-2014	0.20	0.90	0.18
2014-2012	2.70	0.61	1.65
2016-2017	0.20	0.61	0.12
2017-2018	0.60	0.61	0.37
2020-2021	0.30	0.90	0.27
2021-2019	0.20	0.90	0.18
2023-2024	0.30	0.61	0.18
2024-2022.5	1.80	0.63	1.13
	51.00		17.33
Weighted Runoff Coefficient			0.34

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Weighted Runoff Calculations

Basin 2000B

Node	Area (AC)	RC	AreaxRC
2030-2031	0.20	0.30	0.06
2031-2032	2.60	0.30	0.78
2032-2033	5.70	0.30	1.71
	8.50		2.55
Weighted Runoff Coefficient			0.30

## Weighted Runoff Calculations

## Basin 3000

Node	Area (AC)	RC	Area x RC
3000-3001	0.20	0.30	0.06
3001-3002	10.60	0.30	3.18
3002-3006	2.60	0.28	0.73
3008-3009	0.20	0.30	0.06
3009-3010	6.70	0.30	2.01
3010-3011	4.60	0.30	1.38
3013-3014	0.20	0.61	0.12
3014-3012	2.10	0.62	1.30
3016-3017	0.30	0.61	0.18
3017-3018	2.20	0.61	1.34
3020-3021	0.20	0.30	0.06
3021-3022	1.30	0.30	0.39
3024-3025	0.40	0.61	0.24
3025-3026	2.70	0.61	1.65
3003-3004	0.20	0.30	0.06
3004-3005	8.60	0.30	2.58
3005-3028	9.70	0.30	2.91
3032-3035	0.30	0.61	0.18
3035-3033	2.00	0.61	1.22
3037-3038	0.20	0.62	0.12
3038-3036	0.80	0.62	0.50
3040-3041	0.30	0.61	0.18
3041-3042	2.30	0.61	1.40
1008-1009	0.20	0.90	0.18
1009-1010	1.20	0.90	1.08
2026-2027	0.20	0.90	0.18
2027-2028	0.60	0.90	0.54
3043.5-3043.7	0.70	0.61	0.43
	61.60		24.27

Weighted Runoff Coefficient                      0.39



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Weighted Runoff Calculations

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**Basin 4000**

**Node 4002.1**

<b>Node</b>	<b>Area (AC)</b>	<b>RC</b>	<b>AreaxRC</b>
4000-4001	0.20	0.30	0.06
4001-4002	3.00	0.30	0.90

Weighted Runoff Coefficient                      0.30

**Node 4003.0**

<b>Node</b>	<b>Area (AC)</b>	<b>RC</b>	<b>AreaxRC</b>
4004-4005	0.30	0.62	0.19
4005-4003	6.60	0.62	4.09

Weighted Runoff Coefficient                      0.62

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Weighted Runoff Calculations

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Basin 7000A			
Node	Area (AC)	RC	AreaxRC
5000	0.5	0.9	0.45
5000.1	0.4	0.3	0.12
5000.2	2.4	0.3	0.72
5000.3	3	0.3	0.90
5001	1	0.9	0.90
5001.1	0.4	0.3	0.12
5001.2	0.7	0.3	0.21
5002	1	0.9	0.90
5002.1	0.6	0.3	0.18
5002.2	1.3	0.3	0.39
5002.3	2.2	0.3	0.66
5004	0.2	0.9	0.18
5005	1.8	0.63	1.13
5008	0.2	0.3	0.06
5009	0.4	0.78	0.31
5012	0.2	0.3	0.06
5013	5.8	0.3	1.74
5017	0.6	0.9	0.54
5021	0.2	0.3	0.06
5022	14	0.3	4.20
5026	0.2	0.63	0.13
5027	1.8	0.63	1.13
5030	0.2	0.3	0.06
5031	3.8	0.3	1.14
5034	0.3	0.63	0.19
5035	5.1	0.63	3.21
5039	0.2	0.62	0.12
5040	2.7	0.62	1.67
5043	0.2	0.3	0.06
5044	2.7	0.32	0.86
5047	0.3	0.63	0.19
5048	3.5	0.63	2.21
5052	0.2	0.63	0.13
5053	4.2	0.63	2.65
5057	0.2	0.61	0.12
5058	2.3	0.64	1.47
5061	0.2	0.63	0.13
5062	3.1	0.63	1.95
5065	0.2	0.63	0.13
5066	3.1	0.63	1.95
5068	5.7	0.3	1.71
5070	0.2	0.64	0.13
5071	1.6	0.64	1.02
5075	0.2	0.27	0.05
5076	0.8	0.31	0.25
5079	0.2	0.25	0.05
5080	2	0.28	0.56
5084	0.3	0.77	0.23
5085	1.3	0.77	1.00
5088	0.6	0.77	0.46
5089	2	0.77	1.54
6000	0.2	0.28	0.06
6001	0.4	0.3	0.12
6004	0.2	0.29	0.06
6005	0.2	0.3	0.06
6012	0.2	0.63	0.13
6013	1.9	0.63	1.20
6008	0.2	0.61	0.12
6009	0.7	0.62	0.43
6014	0.3	0.35	0.11
6014.2	2	0.29	0.58
6017	0.2	0.61	0.12
6018	2.1	0.29	0.61
6021	0.3	0.3	0.09
6022	0.6	0.78	0.47
6024	0.2	0.77	0.15
6025	1.7	0.68	1.16
6032	0.2	0.3	0.06
6033	0.5	0.77	0.39
6036	0.2	0.77	0.15
6037	1.1	0.77	0.85
6038	0.2	0.67	0.13
6039	1.1	0.77	0.85

Meadowood  
J-15956  
Weighted Runoff Calculations

7/29/2009

6040	0.2	0.25	0.05
6041	0.7	0.67	0.47
6042	0.3	0.67	0.20
6043	0.7	0.67	0.47
6047	0.2	0.67	0.13
6048	1.6	0.77	1.23
6049	0.6	0.67	0.40
6052	0.6	0.77	0.46
6056	0.5	0.77	0.39
6059	0.3	0.77	0.23
6060	1.7	0.77	1.31
6061	0.2	0.77	0.15
6062	1.2	0.77	0.92
6063	0.5	0.67	0.34
6087	0.2	0.77	0.15
6088	1.2	0.77	0.92
6066	1	0.77	0.77
6082	0.5	0.77	0.39
6068	0.2	0.25	0.05
6069	0.6	0.29	0.17
6070	1.5	0.77	1.16
6077	0.5	0.67	0.34
6078	2.3	0.77	1.77
7000	0.7	0.45	0.32
700.1	1.4	0.45	0.63
7001	0.2	0.3	0.06
7001.1	0.7	0.3	0.21
7001.2	1.9	0.3	0.57
7004	0.2	0.3	0.06
7005	3.1	0.3	0.93
7006	1.3	0.63	0.82
7007	0.2	0.3	0.06
7008	2.3	0.3	0.69
7017	0.2	0.3	0.06
7018	0.9	0.3	0.27
7020	0.2	0.63	0.13
7021	0.8	0.63	0.50
7024	0.3	0.3	0.09
7025	3.4	0.3	1.02
7040	0.3	0.63	0.19
7041	1.9	0.63	1.20
7028	0.2	0.63	0.13
7029	2.7	0.63	1.70
7042	1.4	0.3	0.42
7032	0.3	0.63	0.19
7033	1.8	0.63	1.13
7036	0.2	0.63	0.13
7037	3.8	0.63	2.39
7045	0.4	0.61	0.24
7046	3.5	0.62	2.17
7049	0.2	0.61	0.12
7050	0.9	0.39	0.35
7053	0.2	0.65	0.13
7054	0.6	0.65	0.39
7058	0.2	0.63	0.13
7059	0.9	0.9	0.81
7061	0.2	0.61	0.12
7062	0.6	0.61	0.37
7066	0.2	0.51	0.10
7067	1	0.69	0.69
5102	0.3	0.9	0.27
5103	1.7	0.9	1.53
7070	0.2	0.8	0.16
7071	3.8	0.8	3.04
7079	6.1	0.45	2.75
7074.1	0.3	0.35	0.11
7074.2	13.3	0.32	4.26
7075.1	0.2	0.35	0.07
7075.2	11	0.35	3.85

194.50 96.24

Weighted Runoff Coefficient 0.49

## Weighted Runoff Calculations

**Basin 7000B****Weighted Runoff Coefficient Tributary to DB 7B**

<b>Node</b>	<b>Area (AC)</b>	<b>RC</b>	<b>AreaxRC</b>
7079-7080	0.20	0.90	0.18
7080-7081	5.60	0.67	3.75
7093-7094	0.20	0.35	0.07
7094-7095	3.90	0.34	1.33
7095-7099	23.80	0.34	8.09
7104-7106	0.20	0.45	0.09
7106-7099	10.90	0.45	4.91
	44.80		18.42

Weighted Runoff Coefficient                      0.41

**Weighted Runoff Coefficient Downstream of DB 7B**

7082-7081	0.50	0.25	0.13
-----------	------	------	------

Weighted Runoff Coefficient                      0.25

## Weighted Runoff Calculations

## Basin 8000A

Node	Area (AC)	RC	AreaxRC
8100-8101	0.3	0.35	0.11
8101-8102	13	0.33	4.29
8114-8115	0.2	0.9	0.18
8115-8116	2.4	0.9	2.16
8118-8119	0.2	0.9	0.18
8119-8120	1.2	0.9	1.08
8123-8124	0.2	0.78	0.16
8124-8125	1	0.77	0.77
8128-8129	0.20	0.90	0.18
8129-8130	0.80	0.77	0.62
8132-8133	0.20	0.77	0.15
8133-8134	1.10	0.77	0.85
8136-8137	0.30	0.77	0.23
8137-8138	0.60	0.77	0.46
8145-8146	0.20	0.77	0.15
8146-8147	2.30	0.77	1.77
8148.2-8148.4	0.20	0.25	0.05
8148.4-8148.6	0.20	0.25	0.05

24.60

13.44

Weighted Runoff Coefficient

0.55

## Node 8152

Node	Area (AC)	RC	AreaxRC
8150-8151	0.3	0.9	0.27
8146-8147	1.9	0.67	1.27
	2.2		1.543

Weighted Runoff Coefficient

0.701

## Weighted Runoff Calculations

## Basin 8000B

Node	Area (AC)	RC	AreaxRC
8200-8201	0.3	0.35	0.11
8201-8202	0.6	0.34	0.20
8202-8203	11.8	0.33	3.89
8216-8217	0.2	0.77	0.15
8217-8218	0.5	0.77	0.39
8218-8223	0.9	0.46	0.41
8220-8221	0.2	0.77	0.15
8221-8222	0.6	0.77	0.46
8226-8227	0.20	0.77	0.15
8227-8228	1.20	0.77	0.92
8235-8236	0.20	0.77	0.15
8236-8237	4.60	0.77	3.54
8230-8231	0.20	0.87	0.17
8231-8232	1.10	0.77	0.85
9010-9011	0.20	0.90	0.18
9011-8204	0.60	0.90	0.54
8244-8245	0.20	0.87	0.17
8245-8246	2.50	0.77	1.93
	26.10		14.39

Weighted Runoff Coefficient 0.55

**Appendix E**  
**100-Year Detention Analyses**

## **Drainage Basin 2000**



```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
* JUN 1998
*
* VERSION 4.1
*
*
* RUN DATE 12JAN09 TIME 16:10:10
*
*****

```

```

*****
*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*
*****

```

```

X      X XXXXXXXX XXXXX      X
X      X X      X      X      XX
X      X X      X      X      X
XXXXXXX XXXX      X      XXXXX X
X      X X      X      X      X
X      X X      X      X      X
X      X XXXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

\*\*\* FREE \*\*\*

\*DIAGRAM

```

1      ID  MEADOWOOD J-15956  01/12/09 FILE: MW2000D.HC1
2      ID  DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)
3      ID  R/O=.34, PRECIP=3.6IN, TC 12.23MIN
4      IT   2 01JAN90   1200   200
5      IO    0     2

6      KK   2000A
7      KM   DRIANAGE BASIN 2000A
8      KO    0     0     0     0     21
9      BA  0.0797
10     IN   12 01JAN90   1154
11     QI    0     3.7   3.8     4     4.1   4.3   4.5   4.7   4.9   5.2
12     QI    5.4     5.9   6.2     6.9   7.3   8.4   9.1  11.1  12.6  18.5
13     QI   25.2  94.41  14.9     9.9   7.8   6.5   5.7   5.1   4.6   4.2
14     QI    3.9     0     0     0     0     0     0     0     0     0
15     QI    0     0

16     KK  DETAIN
17     KM  100-YEAR DETENTION
18     KO    0     0     0     0     21
19     RS    1  STOR    -1
20     SV    0   0.21   0.36   0.53   0.85
21     SQ    0   3.65   5.95  36.41  70.6
22     SE   100 101.95  103 104.01  105

23     KK MW2000B
24     KM  RUN DATE   1/12/2009
25     KM  RATIONAL METHOD HYDROGRAPH PROGRAM
26     KM  COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
27     KM  6HR RAINFALL IS  3.6  INCHES
28     KM  RATIONAL METHOD RUNOFF COEFFICIENT IS  0.3
29     KM  RATIONAL METHOD TIME OF CONCENTRATION IS  11  MIN.
30     KM  FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
31     KM  IT 2 01JAN90 1200 200
32     KO    0     0     0     0     21
33     BA  0.0133
34     IN   11 01JAN90   1153
35     QI    0     0.5   0.6     0.6   0.6   0.6   0.6   0.7   0.7   0.7
36     QI    0.8   0.8   0.8     0.9   1     1.1   1.1   1.3   1.4   1.7
37     QI    2     2.9   3.8  14.78   2.3   1.5   1.2   1     0.9   0.8
38     QI    0.7   0.7   0.6     0.6   0     0     0     0     0     0
39     QI    0     0     0     0     0

40     KK COMBINE
41     KO    0     0     0     0     21
42     HC    2
43     ZZ

```

# SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT

LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
6	2000A	
	V	
	V	
16	DETAIN	
	.	
	.	
23	.	MW2000B
	.	
	.	
40	COMBINE.....	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 12JAN09 TIME 16:10:10
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
```

MEADOWOOD J-15956 01/12/09 FILE: MW2000D.HC1  
 DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)  
 R/0=.34, PRECIP=3.6IN, TC 12.23MIN

5 IO OUTPUT CONTROL VARIABLES

IPRNT 0 PRINT CONTROL  
 IPLOT 2 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 2 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1JAN90 STARTING DATE  
 ITIME 1200 STARTING TIME  
 NQ 200 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 1JAN90 ENDING DATE  
 NDTIME 1838 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .03 HOURS  
 TOTAL TIME BASE 6.63 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

\*\*\*\*\*

6 KK

```
*****
*
* 2000A
*
*****
```

DRAINAGE BASIN 2000A

8 KO OUTPUT CONTROL VARIABLES

IPRNT 0 PRINT CONTROL  
 IPLOT 2 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 200 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT .033 TIME INTERVAL IN HOURS

10 IN TIME DATA FOR INPUT TIME SERIES  
 JXMIN 12 TIME INTERVAL IN MINUTES  
 JXDATE 1JAN90 STARTING DATE  
 JXTIME 1154 STARTING TIME

SUBBASIN RUNOFF DATA

9 BA SUBBASIN CHARACTERISTICS  
 TAREA .08 SUBBASIN AREA

\*\*\*

HYDROGRAPH AT STATION 2000A

DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*
1	JAN	1200	1	2.	*	1	JAN	1340	51	5.	*	1	JAN	1520	101	11.	*	1	JAN	1700	151	6.	*
1	JAN	1202	2	2.	*	1	JAN	1342	52	5.	*	1	JAN	1522	102	12.	*	1	JAN	1702	152	6.	*
1	JAN	1204	3	3.	*	1	JAN	1344	53	5.	*	1	JAN	1524	103	12.	*	1	JAN	1704	153	6.	*
1	JAN	1206	4	4.	*	1	JAN	1346	54	5.	*	1	JAN	1526	104	12.	*	1	JAN	1706	154	6.	*
1	JAN	1208	5	4.	*	1	JAN	1348	55	5.	*	1	JAN	1528	105	12.	*	1	JAN	1708	155	6.	*
1	JAN	1210	6	4.	*	1	JAN	1350	56	5.	*	1	JAN	1530	106	13.	*	1	JAN	1710	156	6.	*
1	JAN	1212	7	4.	*	1	JAN	1352	57	5.	*	1	JAN	1532	107	14.	*	1	JAN	1712	157	5.	*
1	JAN	1214	8	4.	*	1	JAN	1354	58	5.	*	1	JAN	1534	108	15.	*	1	JAN	1714	158	5.	*
1	JAN	1216	9	4.	*	1	JAN	1356	59	5.	*	1	JAN	1536	109	16.	*	1	JAN	1716	159	5.	*
1	JAN	1218	10	4.	*	1	JAN	1358	60	6.	*	1	JAN	1538	110	17.	*	1	JAN	1718	160	5.	*
1	JAN	1220	11	4.	*	1	JAN	1400	61	6.	*	1	JAN	1540	111	18.	*	1	JAN	1720	161	5.	*
1	JAN	1222	12	4.	*	1	JAN	1402	62	6.	*	1	JAN	1542	112	19.	*	1	JAN	1722	162	5.	*
1	JAN	1224	13	4.	*	1	JAN	1404	63	6.	*	1	JAN	1544	113	20.	*	1	JAN	1724	163	5.	*
1	JAN	1226	14	4.	*	1	JAN	1406	64	6.	*	1	JAN	1546	114	21.	*	1	JAN	1726	164	5.	*
1	JAN	1228	15	4.	*	1	JAN	1408	65	6.	*	1	JAN	1548	115	22.	*	1	JAN	1728	165	5.	*
1	JAN	1230	16	4.	*	1	JAN	1410	66	6.	*	1	JAN	1550	116	23.	*	1	JAN	1730	166	5.	*
1	JAN	1232	17	4.	*	1	JAN	1412	67	6.	*	1	JAN	1552	117	24.	*	1	JAN	1732	167	5.	*
1	JAN	1234	18	4.	*	1	JAN	1414	68	6.	*	1	JAN	1554	118	25.	*	1	JAN	1734	168	4.	*
1	JAN	1236	19	4.	*	1	JAN	1416	69	6.	*	1	JAN	1556	119	37.	*	1	JAN	1736	169	4.	*
1	JAN	1238	20	4.	*	1	JAN	1418	70	6.	*	1	JAN	1558	120	48.	*	1	JAN	1738	170	4.	*
1	JAN	1240	21	4.	*	1	JAN	1420	71	6.	*	1	JAN	1600	121	60.	*	1	JAN	1740	171	4.	*
1	JAN	1242	22	4.	*	1	JAN	1422	72	6.	*	1	JAN	1602	122	71.	*	1	JAN	1742	172	4.	*
1	JAN	1244	23	4.	*	1	JAN	1424	73	7.	*	1	JAN	1604	123	83.	*	1	JAN	1744	173	4.	*
1	JAN	1246	24	4.	*	1	JAN	1426	74	7.	*	1	JAN	1606	124	94.	*	1	JAN	1746	174	4.	*
1	JAN	1248	25	4.	*	1	JAN	1428	75	7.	*	1	JAN	1608	125	81.	*	1	JAN	1748	175	4.	*
1	JAN	1250	26	4.	*	1	JAN	1430	76	7.	*	1	JAN	1610	126	68.	*	1	JAN	1750	176	4.	*
1	JAN	1252	27	4.	*	1	JAN	1432	77	7.	*	1	JAN	1612	127	55.	*	1	JAN	1752	177	4.	*
1	JAN	1254	28	4.	*	1	JAN	1434	78	7.	*	1	JAN	1614	128	41.	*	1	JAN	1754	178	4.	*
1	JAN	1256	29	4.	*	1	JAN	1436	79	7.	*	1	JAN	1616	129	28.	*	1	JAN	1756	179	3.	*
1	JAN	1258	30	4.	*	1	JAN	1438	80	7.	*	1	JAN	1618	130	15.	*	1	JAN	1758	180	3.	*
1	JAN	1300	31	4.	*	1	JAN	1440	81	7.	*	1	JAN	1620	131	14.	*	1	JAN	1800	181	2.	*
1	JAN	1302	32	4.	*	1	JAN	1442	82	7.	*	1	JAN	1622	132	13.	*	1	JAN	1802	182	1.	*
1	JAN	1304	33	4.	*	1	JAN	1444	83	7.	*	1	JAN	1624	133	12.	*	1	JAN	1804	183	1.	*

1 JAN 1306	34	5.	*	1 JAN 1446	84	8.	*	1 JAN 1626	134	12.	*	1 JAN 1806	184	0.
1 JAN 1308	35	5.	*	1 JAN 1448	85	8.	*	1 JAN 1628	135	11.	*	1 JAN 1808	185	0.
1 JAN 1310	36	5.	*	1 JAN 1450	86	8.	*	1 JAN 1630	136	10.	*	1 JAN 1810	186	0.
1 JAN 1312	37	5.	*	1 JAN 1452	87	8.	*	1 JAN 1632	137	10.	*	1 JAN 1812	187	0.
1 JAN 1314	38	5.	*	1 JAN 1454	88	8.	*	1 JAN 1634	138	9.	*	1 JAN 1814	188	0.
1 JAN 1316	39	5.	*	1 JAN 1456	89	9.	*	1 JAN 1636	139	9.	*	1 JAN 1816	189	0.
1 JAN 1318	40	5.	*	1 JAN 1458	90	9.	*	1 JAN 1638	140	9.	*	1 JAN 1818	190	0.
1 JAN 1320	41	5.	*	1 JAN 1500	91	9.	*	1 JAN 1640	141	8.	*	1 JAN 1820	191	0.
1 JAN 1322	42	5.	*	1 JAN 1502	92	9.	*	1 JAN 1642	142	8.	*	1 JAN 1822	192	0.
1 JAN 1324	43	5.	*	1 JAN 1504	93	9.	*	1 JAN 1644	143	8.	*	1 JAN 1824	193	0.
1 JAN 1326	44	5.	*	1 JAN 1506	94	9.	*	1 JAN 1646	144	7.	*	1 JAN 1826	194	0.
1 JAN 1328	45	5.	*	1 JAN 1508	95	9.	*	1 JAN 1648	145	7.	*	1 JAN 1828	195	0.
1 JAN 1330	46	5.	*	1 JAN 1510	96	10.	*	1 JAN 1650	146	7.	*	1 JAN 1830	196	0.
1 JAN 1332	47	5.	*	1 JAN 1512	97	10.	*	1 JAN 1652	147	7.	*	1 JAN 1832	197	0.
1 JAN 1334	48	5.	*	1 JAN 1514	98	10.	*	1 JAN 1654	148	7.	*	1 JAN 1834	198	0.
1 JAN 1336	49	5.	*	1 JAN 1516	99	11.	*	1 JAN 1656	149	6.	*	1 JAN 1836	199	0.
1 JAN 1338	50	5.	*	1 JAN 1518	100	11.	*	1 JAN 1658	150	6.	*	1 JAN 1838	200	0.

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PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	6.63-HR
94.	4.10	(CFS) 10.	9.	9.	9.
		(INCHES) 1.213	1.215	1.215	1.215
		(AC-FT) 5.	5.	5.	5.

CUMULATIVE AREA = .08 SQ MI

## 2000A

(O) OUTFLOW

DAHRMN PER

[illegible]



[illegible]

11750	176.	O	.	.	.	.	.	.	.	.
11752	177.	O	.	.	.	.	.	.	.	.
11754	178.	O	.	.	.	.	.	.	.	.
11756	179.	O	.	.	.	.	.	.	.	.
11758	180.	O	.	.	.	.	.	.	.	.
11800	181.	O	.	.	.	.	.	.	.	.
11802	182.O		.	.	.	.	.	.	.	.
11804	183.O		.	.	.	.	.	.	.	.
11806	184O		.	.	.	.	.	.	.	.
11808	185O		.	.	.	.	.	.	.	.
11810	186O		.	.	.	.	.	.	.	.
11812	187O		.	.	.	.	.	.	.	.
11814	188O		.	.	.	.	.	.	.	.
11816	189O		.	.	.	.	.	.	.	.
11818	190O		.	.	.	.	.	.	.	.
11820	191O		.	.	.	.	.	.	.	.
11822	192O		.	.	.	.	.	.	.	.
11824	193O		.	.	.	.	.	.	.	.
11826	194O		.	.	.	.	.	.	.	.
11828	195O		.	.	.	.	.	.	.	.
11830	196O		.	.	.	.	.	.	.	.
11832	197O		.	.	.	.	.	.	.	.
11834	198O		.	.	.	.	.	.	.	.
11836	199O		.	.	.	.	.	.	.	.
11838	200O		.	.	.	.	.	.	.	.

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16 KK      \*      DETAIN      \*  
\*      \*  
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100-YEAR DETENTION

18 KO      OUTPUT CONTROL VARIABLES

IPRNT      0      PRINT CONTROL  
IPLOT      2      PLOT CONTROL  
QSCAL      0.      HYDROGRAPH PLOT SCALE  
IPNCH      0      PUNCH COMPUTED HYDROGRAPH  
IOUT      21      SAVE HYDROGRAPH ON THIS UNIT  
ISAV1      1      FIRST ORDINATE PUNCHED OR SAVED  
ISAV2      200      LAST ORDINATE PUNCHED OR SAVED  
TIMINT      .033      TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

19 RS      STORAGE ROUTING

NSTPS      1      NUMBER OF SUBREACHES  
ITYP      STOR      TYPE OF INITIAL CONDITION  
RSVRIC      -1.00      INITIAL CONDITION  
X      .00      WORKING R AND D COEFFICIENT

20 SV	STORAGE	.0	.2	.4	.5	.9
21 SQ	DISCHARGE	0.	4.	6.	36.	71.
22 SE	ELEVATION	100.00	101.95	103.00	104.01	105.00

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WARNING --- ROUTED OUTFLOW ( 71.) IS GREATER THAN MAXIMUM OUTFLOW ( 71.) IN STORAGE-OUTFLOW TABLE

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HYDROGRAPH AT STATION      DETAIN

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DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
1	JAN	1200	1	2.	.1	101.0	*	1	JAN	1414	68	5.	.3	102.5	*	1	JAN	1628	135	16.	.4	103.3
1	JAN	1202	2	2.	.1	101.0	*	1	JAN	1416	69	5.	.3	102.6	*	1	JAN	1630	136	14.	.4	103.3
1	JAN	1204	3	2.	.1	101.0	*	1	JAN	1418	70	5.	.3	102.6	*	1	JAN	1632	137	12.	.4	103.2
1	JAN	1206	4	2.	.1	101.1	*	1	JAN	1420	71	5.	.3	102.6	*	1	JAN	1634	138	11.	.4	103.2
1	JAN	1208	5	2.	.1	101.1	*	1	JAN	1422	72	5.	.3	102.6	*	1	JAN	1636	139	10.	.4	103.1
1	JAN	1210	6	2.	.1	101.1	*	1	JAN	1424	73	5.	.3	102.7	*	1	JAN	1638	140	10.	.4	103.1
1	JAN	1212	7	2.	.1	101.2	*	1	JAN	1426	74	5.	.3	102.7	*	1	JAN	1640	141	9.	.4	103.1
1	JAN	1214	8	2.	.1	101.2	*	1	JAN	1428	75	5.	.3	102.7	*	1	JAN	1642	142	9.	.4	103.1
1	JAN	1216	9	2.	.1	101.3	*	1	JAN	1430	76	5.	.3	102.7	*	1	JAN	1644	143	8.	.4	103.1

1 JAN 1218 10	2.	.1	101.3 *	1 JAN 1432 77	5.	.3	102.8 *	1 JAN 1646 144	8.	.4	103.1
1 JAN 1220 11	2.	.1	101.3 *	1 JAN 1434 78	6.	.3	102.8 *	1 JAN 1648 145	8.	.4	103.1
1 JAN 1222 12	3.	.1	101.4 *	1 JAN 1436 79	6.	.3	102.8 *	1 JAN 1650 146	7.	.4	103.0
1 JAN 1224 13	3.	.2	101.4 *	1 JAN 1438 80	6.	.3	102.9 *	1 JAN 1652 147	7.	.4	103.0
1 JAN 1226 14	3.	.2	101.4 *	1 JAN 1440 81	6.	.3	102.9 *	1 JAN 1654 148	7.	.4	103.0
1 JAN 1228 15	3.	.2	101.5 *	1 JAN 1442 82	6.	.3	102.9 *	1 JAN 1656 149	7.	.4	103.0
1 JAN 1230 16	3.	.2	101.5 *	1 JAN 1444 83	6.	.4	103.0 *	1 JAN 1658 150	7.	.4	103.0
1 JAN 1232 17	3.	.2	101.5 *	1 JAN 1446 84	6.	.4	103.0 *	1 JAN 1700 151	6.	.4	103.0
1 JAN 1234 18	3.	.2	101.6 *	1 JAN 1448 85	6.	.4	103.0 *	1 JAN 1702 152	6.	.4	103.0
1 JAN 1236 19	3.	.2	101.6 *	1 JAN 1450 86	7.	.4	103.0 *	1 JAN 1704 153	6.	.4	103.0
1 JAN 1238 20	3.	.2	101.6 *	1 JAN 1452 87	7.	.4	103.0 *	1 JAN 1706 154	6.	.4	103.0
1 JAN 1240 21	3.	.2	101.6 *	1 JAN 1454 88	8.	.4	103.1 *	1 JAN 1708 155	6.	.4	103.0
1 JAN 1242 22	3.	.2	101.7 *	1 JAN 1456 89	8.	.4	103.1 *	1 JAN 1710 156	6.	.4	103.0
1 JAN 1244 23	3.	.2	101.7 *	1 JAN 1458 90	8.	.4	103.1 *	1 JAN 1712 157	6.	.4	103.0
1 JAN 1246 24	3.	.2	101.7 *	1 JAN 1500 91	8.	.4	103.1 *	1 JAN 1714 158	6.	.4	103.0
1 JAN 1248 25	3.	.2	101.7 *	1 JAN 1502 92	9.	.4	103.1 *	1 JAN 1716 159	6.	.4	103.0
1 JAN 1250 26	3.	.2	101.8 *	1 JAN 1504 93	9.	.4	103.1 *	1 JAN 1718 160	6.	.4	102.9
1 JAN 1252 27	3.	.2	101.8 *	1 JAN 1506 94	9.	.4	103.1 *	1 JAN 1720 161	6.	.3	102.9
1 JAN 1254 28	3.	.2	101.8 *	1 JAN 1508 95	9.	.4	103.1 *	1 JAN 1722 162	6.	.3	102.9
1 JAN 1256 29	3.	.2	101.8 *	1 JAN 1510 96	9.	.4	103.1 *	1 JAN 1724 163	6.	.3	102.9
1 JAN 1258 30	3.	.2	101.9 *	1 JAN 1512 97	10.	.4	103.1 *	1 JAN 1726 164	6.	.3	102.9
1 JAN 1300 31	4.	.2	101.9 *	1 JAN 1514 98	10.	.4	103.1 *	1 JAN 1728 165	6.	.3	102.9
1 JAN 1302 32	4.	.2	101.9 *	1 JAN 1516 99	10.	.4	103.1 *	1 JAN 1730 166	6.	.3	102.8
1 JAN 1304 33	4.	.2	101.9 *	1 JAN 1518 100	10.	.4	103.1 *	1 JAN 1732 167	6.	.3	102.8
1 JAN 1306 34	4.	.2	101.9 *	1 JAN 1520 101	11.	.4	103.2 *	1 JAN 1734 168	6.	.3	102.8
1 JAN 1308 35	4.	.2	102.0 *	1 JAN 1522 102	11.	.4	103.2 *	1 JAN 1736 169	5.	.3	102.8
1 JAN 1310 36	4.	.2	102.0 *	1 JAN 1524 103	11.	.4	103.2 *	1 JAN 1738 170	5.	.3	102.8
1 JAN 1312 37	4.	.2	102.0 *	1 JAN 1526 104	12.	.4	103.2 *	1 JAN 1740 171	5.	.3	102.7
1 JAN 1314 38	4.	.2	102.0 *	1 JAN 1528 105	12.	.4	103.2 *	1 JAN 1742 172	5.	.3	102.7
1 JAN 1316 39	4.	.2	102.0 *	1 JAN 1530 106	12.	.4	103.2 *	1 JAN 1744 173	5.	.3	102.7
1 JAN 1318 40	4.	.2	102.0 *	1 JAN 1532 107	12.	.4	103.2 *	1 JAN 1746 174	5.	.3	102.7
1 JAN 1320 41	4.	.2	102.1 *	1 JAN 1534 108	13.	.4	103.2 *	1 JAN 1748 175	5.	.3	102.7
1 JAN 1322 42	4.	.2	102.1 *	1 JAN 1536 109	14.	.4	103.3 *	1 JAN 1750 176	5.	.3	102.6
1 JAN 1324 43	4.	.2	102.1 *	1 JAN 1538 110	15.	.4	103.3 *	1 JAN 1752 177	5.	.3	102.6
1 JAN 1326 44	4.	.2	102.1 *	1 JAN 1540 111	16.	.4	103.3 *	1 JAN 1754 178	5.	.3	102.6
1 JAN 1328 45	4.	.2	102.1 *	1 JAN 1542 112	17.	.4	103.4 *	1 JAN 1756 179	5.	.3	102.6
1 JAN 1330 46	4.	.2	102.1 *	1 JAN 1544 113	18.	.4	103.4 *	1 JAN 1758 180	5.	.3	102.5
1 JAN 1332 47	4.	.2	102.2 *	1 JAN 1546 114	19.	.4	103.4 *	1 JAN 1800 181	5.	.3	102.5
1 JAN 1334 48	4.	.2	102.2 *	1 JAN 1548 115	20.	.4	103.5 *	1 JAN 1802 182	5.	.3	102.4
1 JAN 1336 49	4.	.2	102.2 *	1 JAN 1550 116	21.	.4	103.5 *	1 JAN 1804 183	5.	.3	102.3
1 JAN 1338 50	4.	.2	102.2 *	1 JAN 1552 117	22.	.4	103.5 *	1 JAN 1806 184	4.	.3	102.3
1 JAN 1340 51	4.	.2	102.2 *	1 JAN 1554 118	23.	.5	103.6 *	1 JAN 1808 185	4.	.2	102.2
1 JAN 1342 52	4.	.3	102.2 *	1 JAN 1556 119	26.	.5	103.7 *	1 JAN 1810 186	4.	.2	102.1
1 JAN 1344 53	4.	.3	102.3 *	1 JAN 1558 120	33.	.5	103.9 *	1 JAN 1812 187	4.	.2	102.0
1 JAN 1346 54	4.	.3	102.3 *	1 JAN 1600 121	39.	.6	104.1 *	1 JAN 1814 188	4.	.2	102.0
1 JAN 1348 55	4.	.3	102.3 *	1 JAN 1602 122	46.	.6	104.3 *	1 JAN 1816 189	3.	.2	101.9
1 JAN 1350 56	4.	.3	102.3 *	1 JAN 1604 123	54.	.7	104.5 *	1 JAN 1818 190	3.	.2	101.8
1 JAN 1352 57	4.	.3	102.3 *	1 JAN 1606 124	63.	.8	104.8 *	1 JAN 1820 191	3.	.2	101.7
1 JAN 1354 58	5.	.3	102.3 *	1 JAN 1608 125	69.	.8	105.0 *	1 JAN 1822 192	3.	.2	101.6
1 JAN 1356 59	5.	.3	102.4 *	1 JAN 1610 126	71.	.9	105.0 *	1 JAN 1824 193	3.	.2	101.5
1 JAN 1358 60	5.	.3	102.4 *	1 JAN 1612 127	68.	.8	104.9 *	1 JAN 1826 194	3.	.2	101.5
1 JAN 1400 61	5.	.3	102.4 *	1 JAN 1614 128	63.	.8	104.8 *	1 JAN 1828 195	3.	.2	101.4
1 JAN 1402 62	5.	.3	102.4 *	1 JAN 1616 129	56.	.7	104.6 *	1 JAN 1830 196	2.	.1	101.3
1 JAN 1404 63	5.	.3	102.4 *	1 JAN 1618 130	47.	.6	104.3 *	1 JAN 1832 197	2.	.1	101.3
1 JAN 1406 64	5.	.3	102.5 *	1 JAN 1620 131	39.	.6	104.1 *	1 JAN 1834 198	2.	.1	101.2
1 JAN 1408 65	5.	.3	102.5 *	1 JAN 1622 132	30.	.5	103.8 *	1 JAN 1836 199	2.	.1	101.2
1 JAN 1410 66	5.	.3	102.5 *	1 JAN 1624 133	23.	.5	103.6 *	1 JAN 1838 200	2.	.1	101.1
1 JAN 1412 67	5.	.3	102.5 *	1 JAN 1626 134	19.	.4	103.4 *				

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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	6.63-HR
71.	4.17	(CFS)	10.	9.	9.	9.
		(INCHES)	1.184	1.212	1.212	1.212
		(AC-FT)	5.	5.	5.	5.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	6.63-HR
1.	4.17		0.	0.	0.	0.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	6.63-HR
105.00	4.17		102.75	102.60	102.60	102.60

CUMULATIVE AREA = .08 SQ MI

## STATION DETAIN

(I) INFLOW, (O) OUTFLOW

0.	20.	40.	60.	80.	100.	0.	0.	0.	0.	0.	0.	0
						(S) STORAGE						
.0	.0	.0	.0	.0	.0	.0	.2	.4	.6	.8	1.0	.

DAHRMN PER

11200	1. I	S										
11202	2. I	S										
11204	3. OI	S										
11206	4. OI	S										
11208	5. OI	S										
11210	6. OI	S										
11212	7. OI	S										
11214	8. OI	S										
11216	9. OI	S										
11218	10. OI	S										
11220	11. OI	S										
11222	12. OI	S										
11224	13. OI	S										
11226	14. OI	S										
11228	15. OI	S										
11230	16. OI	S										
11232	17. OI	S										
11234	18. OI	S										
11236	19. OI	S										
11238	20. I	S										
11240	21. I	S										
11242	22. I	S										
11244	23. I	S										
11246	24. I	S										
11248	25. I	S										
11250	26. I	S										
11252	27. I	S										
11254	28. I	S										
11256	29. I	S										
11258	30. I	S										
11300	31. I	S										
11302	32. I	S										
11304	33. I	S										
11306	34. I	S										
11308	35. I	S										
11310	36. I	S										
11312	37. I	S										
11314	38. I	S										
11316	39. I	S										
11318	40. I	S										
11320	41. I	S										
11322	42. I	S										
11324	43. I	S										
11326	44. I	S										
11328	45. I	S										
11330	46. I	S										
11332	47. I	S										
11334	48. OI	S										
11336	49. OI	S										
11338	50. OI	S										
11340	51. OI	S										
11342	52. OI	S										
11344	53. OI	S										

11346	54.	OI	.	.	.	.	.	S	.	.	.
11348	55.	OI	.	.	.	.	.	S	.	.	.
11350	56.	OI	.	.	.	.	.	S	.	.	.
11352	57.	OI	.	.	.	.	.	S	.	.	.
11354	58.	OI	.	.	.	.	.	S	.	.	.
11356	59.	OI	.	.	.	.	.	S	.	.	.
11358	60.	OI	.	.	.	.	.	S	.	.	.
11400	61.	OI	.	.	.	.	.	S	.	.	.
11402	62.	OI	.	.	.	.	.	S	.	.	.
11404	63.	OI	.	.	.	.	.	S	.	.	.
11406	64.	OI	.	.	.	.	.	S	.	.	.
11408	65.	OI	.	.	.	.	.	S	.	.	.
11410	66.	OI	.	.	.	.	.	S	.	.	.
11412	67.	OI	.	.	.	.	.	S	.	.	.
11414	68.	OI	.	.	.	.	.	S	.	.	.
11416	69.	I	.	.	.	.	.	S	.	.	.
11418	70.	I	.	.	.	.	.	S	.	.	.
11420	71.	I	.	.	.	.	.	S	.	.	.
11422	72.	I	.	.	.	.	.	S	.	.	.
11424	73.	I	.	.	.	.	.	S	.	.	.
11426	74.	I	.	.	.	.	.	S	.	.	.
11428	75.	I	.	.	.	.	.	S	.	.	.
11430	76.	I	.	.	.	.	.	S	.	.	.
11432	77.	I	.	.	.	.	.	S	.	.	.
11434	78.	OI	.	.	.	.	.	S	.	.	.
11436	79.	OI	.	.	.	.	.	S	.	.	.
11438	80.	OI	.	.	.	.	.	S	.	.	.
11440	81.	OI	.	.	.	.	.	S	.	.	.
11442	82.	OI	.	.	.	.	.	S	.	.	.
11444	83.	OI	.	.	.	.	.	S	.	.	.
11446	84.	OI	.	.	.	.	.	S	.	.	.
11448	85.	OI	.	.	.	.	.	S	.	.	.
11450	86.	OI	.	.	.	.	.	S	.	.	.
11452	87.	I	.	.	.	.	.	S	.	.	.
11454	88.	I	.	.	.	.	.	S	.	.	.
11456	89.	I	.	.	.	.	.	S	.	.	.
11458	90.	I	.	.	.	.	.	S	.	.	.
11500	91.	I	.	.	.	.	.	S	.	.	.
11502	92.	I	.	.	.	.	.	S	.	.	.
11504	93.	I	.	.	.	.	.	S	.	.	.
11506	94.	OI	.	.	.	.	.	S	.	.	.
11508	95.	I	.	.	.	.	.	S	.	.	.
11510	96.	I	.	.	.	.	.	S	.	.	.
11512	97.	I	.	.	.	.	.	S	.	.	.
11514	98.	I	.	.	.	.	.	S	.	.	.
11516	99.	I	.	.	.	.	.	S	.	.	.
11518	100.	OI	.	.	.	.	.	S	.	.	.
11520	101.	OI	.	.	.	.	.	S	.	.	.
11522	102.	I	.	.	.	.	.	S	.	.	.
11524	103.	I	.	.	.	.	.	S	.	.	.
11526	104.	I	.	.	.	.	.	S	.	.	.
11528	105.	I	.	.	.	.	.	S	.	.	.
11530	106.	I	.	.	.	.	.	S	.	.	.
11532	107.	OI	.	.	.	.	.	S	.	.	.
11534	108.	I	.	.	.	.	.	S	.	.	.
11536	109.	OI	.	.	.	.	.	S	.	.	.
11538	110.	OI	.	.	.	.	.	S	.	.	.
11540	111.	OI	.	.	.	.	.	S	.	.	.
11542	112.	OI	.	.	.	.	.	S	.	.	.
11544	113.	OI	.	.	.	.	.	S	.	.	.

11546	114.	OI	.	.	.	.	.	S	.	.
11548	115.	OI	.	.	.	.	.	S	.	.
11550	116.	OI	.	.	.	.	.	S	.	.
11552	117.	.OI	.	.	.	.	.	S	.	.
11554	118.	.O I	.	.	.	.	.	S	.	.
11556	119.	. O I .	.	.	.	.	.	S	.	.
11558	120.	. O . I .	.	.	.	.	.	S	.	.
11600	121.	. . . . . O . I .	.	.	.	.	.	S	.	.
11602	122.	. . . . . O . I .	.	.	.	.	.	S	.	.
11604	123.	. . . . . O . . I .	.	.	.	.	.	S	.	.
11606	124.	. . . . . O . . I .	.	.	.	.	.	S	.	.
11608	125.	. . . . . O . I .	.	.	.	.	.	S	.	.
11610	126.	. . . . . IO .	.	.	.	.	.	S	.	.
11612	127.	. . . . . I . O .	.	.	.	.	.	S	.	.
11614	128.	. . . . . I . O .	.	.	.	.	.	S	.	.
11616	129.	. . . . . I . O .	.	.	.	.	.	S	.	.
11618	130.	I . . . . O .	.	.	.	.	.	S	.	.
11620	131.	. . . . . I . . O .	.	.	.	.	.	S	.	.
11622	132.	I . . . . O .	.	.	.	.	.	S	.	.
11624	133.	I . . . . O .	.	.	.	.	.	S	.	.
11626	134.	I O . . . . .	.	.	.	.	.	S	.	.
11628	135.	I O . . . . .	.	.	.	.	.	S	.	.
11630	136.	I O . . . . .	.	.	.	.	.	S	.	.
11632	137.	IO . . . . .	.	.	.	.	.	S	.	.
11634	138.	I . . . . .	.	.	.	.	.	S	.	.
11636	139.	IO . . . . .	.	.	.	.	.	S	.	.
11638	140.	IO . . . . .	.	.	.	.	.	S	.	.
11640	141.	IO . . . . .	.	.	.	.	.	S	.	.
11642	142.	I . . . . .	.	.	.	.	.	S	.	.
11644	143.	I . . . . .	.	.	.	.	.	S	.	.
11646	144.	I . . . . .	.	.	.	.	.	S	.	.
11648	145.	I . . . . .	.	.	.	.	.	S	.	.
11650	146.	IO . . . . .	.	.	.	.	.	S	.	.
11652	147.	IO . . . . .	.	.	.	.	.	S	.	.
11654	148.	I . . . . .	.	.	.	.	.	S	.	.
11656	149.	I . . . . .	.	.	.	.	.	S	.	.
11658	150.	I . . . . .	.	.	.	.	.	S	.	.
11700	151.	.I . . . . .	.	.	.	.	.	S	.	.
11702	152.	I . . . . .	.	.	.	.	.	S	.	.
11704	153.	I . . . . .	.	.	.	.	.	S	.	.
11706	154.	I . . . . .	.	.	.	.	.	S	.	.
11708	155.	I . . . . .	.	.	.	.	.	S	.	.
11710	156.	I . . . . .	.	.	.	.	.	S	.	.
11712	157.	I . . . . .	.	.	.	.	.	S	.	.
11714	158.	I . . . . .	.	.	.	.	.	S	.	.
11716	159.	I . . . . .	.	.	.	.	.	S	.	.
11718	160.	I . . . . .	.	.	.	.	.	S	.	.
11720	161.	.I . . . . .	.	.	.	.	.	S	.	.
11722	162.	IO . . . . .	.	.	.	.	.	S	.	.
11724	163.	IO . . . . .	.	.	.	.	.	S	.	.
11726	164.	IO . . . . .	.	.	.	.	.	S	.	.
11728	165.	IO . . . . .	.	.	.	.	.	S	.	.
11730	166.	IO . . . . .	.	.	.	.	.	S	.	.
11732	167.	IO . . . . .	.	.	.	.	.	S	.	.
11734	168.	IO . . . . .	.	.	.	.	.	S	.	.
11736	169.	IO . . . . .	.	.	.	.	.	S	.	.
11738	170.	IO . . . . .	.	.	.	.	.	S	.	.
11740	171.	IO . . . . .	.	.	.	.	.	S	.	.
11742	172.	IO . . . . .	.	.	.	.	.	S	.	.
11744	173.	IO . . . . .	.	.	.	.	.	S	.	.



11746	174.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11748	175.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11750	176.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11752	177.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11754	178.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11756	179.	I	.	.	.	.	.	.	.	S	.	.	.	.
11758	180.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11800	181.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11802	182.	IO	.	.	.	.	.	.	.	S	.	.	.	.
11804	183I	O	.	.	.	.	.	.	.	S	.	.	.	.
11806	184I	O	.	.	.	.	.	.	.	S	.	.	.	.
11808	185I	O	.	.	.	.	.	.	.	S	.	.	.	.
11810	186I	O	.	.	.	.	.	.	.	S	.	.	.	.
11812	187I	O	.	.	.	.	.	.	.	S	.	.	.	.
11814	188I	O	.	.	.	.	.	.	.	S	.	.	.	.
11816	189I	O	.	.	.	.	.	.	.	S	.	.	.	.
11818	190I	O	.	.	.	.	.	.	.	S	.	.	.	.
11820	191I	O	.	.	.	.	.	.	.	S	.	.	.	.
11822	192I	O	.	.	.	.	.	.	.	S	.	.	.	.
11824	193IO		.	.	.	.	.	.	.	S	.	.	.	.
11826	194IO		.	.	.	.	.	.	.	S	.	.	.	.
11828	195IO		.	.	.	.	.	.	.	S	.	.	.	.
11830	196IO		.	.	.	.	.	.	.	S	.	.	.	.
11832	197IO		.	.	.	.	.	.	.	S	.	.	.	.
11834	198IO		.	.	.	.	.	.	.	S	.	.	.	.
11836	199IO		.	.	.	.	.	.	.	S	.	.	.	.
11838	200IO		.	.	.	.	.	.	.	S	.	.	.	.

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23 KK \* MW2000B \*

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RUN DATE 1/12/2009

RATIONAL METHOD HYDROGRAPH PROGRAM

COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY

6HR RAINFALL IS 3.6 INCHES

RATIONAL METHOD RUNOFF COEFFICIENT IS 0.3

RATIONAL METHOD TIME OF CONCENTRATION IS 11 MIN.

FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1

IT 2 01JAN90 1200 200

32 KO OUTPUT CONTROL VARIABLES

IPRNT 0 PRINT CONTROL  
IPLOT 2 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 200 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .033 TIME INTERVAL IN HOURS

34 IN TIME DATA FOR INPUT TIME SERIES

JXMIN 11 TIME INTERVAL IN MINUTES  
JXDATE 1JAN90 STARTING DATE  
JXTIME 1153 STARTING TIME

SUBBASIN RUNOFF DATA

33 BA SUBBASIN CHARACTERISTICS

TAREA .01 SUBBASIN AREA

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HYDROGRAPH AT STATION MW2000B

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DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW
					*						*						*					
1	JAN	1200	1	0.	*	1	JAN	1340	51	1.	*	1	JAN	1520	101	2.	*	1	JAN	1700	151	1.
1	JAN	1202	2	0.	*	1	JAN	1342	52	1.	*	1	JAN	1522	102	2.	*	1	JAN	1702	152	1.
1	JAN	1204	3	1.	*	1	JAN	1344	53	1.	*	1	JAN	1524	103	2.	*	1	JAN	1704	153	1.
1	JAN	1206	4	1.	*	1	JAN	1346	54	1.	*	1	JAN	1526	104	2.	*	1	JAN	1706	154	1.
1	JAN	1208	5	1.	*	1	JAN	1348	55	1.	*	1	JAN	1528	105	2.	*	1	JAN	1708	155	1.
1	JAN	1210	6	1.	*	1	JAN	1350	56	1.	*	1	JAN	1530	106	2.	*	1	JAN	1710	156	1.
1	JAN	1212	7	1.	*	1	JAN	1352	57	1.	*	1	JAN	1532	107	2.	*	1	JAN	1712	157	1.
1	JAN	1214	8	1.	*	1	JAN	1354	58	1.	*	1	JAN	1534	108	2.	*	1	JAN	1714	158	1.

1 JAN 1216	9	1.	*	1 JAN 1356	59	1.	*	1 JAN 1536	109	2.	*	1 JAN 1716	159	1.
1 JAN 1218	10	1.	*	1 JAN 1358	60	1.	*	1 JAN 1538	110	2.	*	1 JAN 1718	160	1.
1 JAN 1220	11	1.	*	1 JAN 1400	61	1.	*	1 JAN 1540	111	3.	*	1 JAN 1720	161	1.
1 JAN 1222	12	1.	*	1 JAN 1402	62	1.	*	1 JAN 1542	112	3.	*	1 JAN 1722	162	1.
1 JAN 1224	13	1.	*	1 JAN 1404	63	1.	*	1 JAN 1544	113	3.	*	1 JAN 1724	163	1.
1 JAN 1226	14	1.	*	1 JAN 1406	64	1.	*	1 JAN 1546	114	3.	*	1 JAN 1726	164	1.
1 JAN 1228	15	1.	*	1 JAN 1408	65	1.	*	1 JAN 1548	115	3.	*	1 JAN 1728	165	1.
1 JAN 1230	16	1.	*	1 JAN 1410	66	1.	*	1 JAN 1550	116	3.	*	1 JAN 1730	166	1.
1 JAN 1232	17	1.	*	1 JAN 1412	67	1.	*	1 JAN 1552	117	4.	*	1 JAN 1732	167	1.
1 JAN 1234	18	1.	*	1 JAN 1414	68	1.	*	1 JAN 1554	118	4.	*	1 JAN 1734	168	1.
1 JAN 1236	19	1.	*	1 JAN 1416	69	1.	*	1 JAN 1556	119	5.	*	1 JAN 1736	169	1.
1 JAN 1238	20	1.	*	1 JAN 1418	70	1.	*	1 JAN 1558	120	7.	*	1 JAN 1738	170	1.
1 JAN 1240	21	1.	*	1 JAN 1420	71	1.	*	1 JAN 1600	121	9.	*	1 JAN 1740	171	1.
1 JAN 1242	22	1.	*	1 JAN 1422	72	1.	*	1 JAN 1602	122	11.	*	1 JAN 1742	172	1.
1 JAN 1244	23	1.	*	1 JAN 1424	73	1.	*	1 JAN 1604	123	13.	*	1 JAN 1744	173	1.
1 JAN 1246	24	1.	*	1 JAN 1426	74	1.	*	1 JAN 1606	124	15.	*	1 JAN 1746	174	1.
1 JAN 1248	25	1.	*	1 JAN 1428	75	1.	*	1 JAN 1608	125	13.	*	1 JAN 1748	175	1.
1 JAN 1250	26	1.	*	1 JAN 1430	76	1.	*	1 JAN 1610	126	10.	*	1 JAN 1750	176	1.
1 JAN 1252	27	1.	*	1 JAN 1432	77	1.	*	1 JAN 1612	127	8.	*	1 JAN 1752	177	1.
1 JAN 1254	28	1.	*	1 JAN 1434	78	1.	*	1 JAN 1614	128	6.	*	1 JAN 1754	178	1.
1 JAN 1256	29	1.	*	1 JAN 1436	79	1.	*	1 JAN 1616	129	3.	*	1 JAN 1756	179	1.
1 JAN 1258	30	1.	*	1 JAN 1438	80	1.	*	1 JAN 1618	130	2.	*	1 JAN 1758	180	0.
1 JAN 1300	31	1.	*	1 JAN 1440	81	1.	*	1 JAN 1620	131	2.	*	1 JAN 1800	181	0.
1 JAN 1302	32	1.	*	1 JAN 1442	82	1.	*	1 JAN 1622	132	2.	*	1 JAN 1802	182	0.
1 JAN 1304	33	1.	*	1 JAN 1444	83	1.	*	1 JAN 1624	133	2.	*	1 JAN 1804	183	0.
1 JAN 1306	34	1.	*	1 JAN 1446	84	1.	*	1 JAN 1626	134	2.	*	1 JAN 1806	184	0.
1 JAN 1308	35	1.	*	1 JAN 1448	85	1.	*	1 JAN 1628	135	2.	*	1 JAN 1808	185	0.
1 JAN 1310	36	1.	*	1 JAN 1450	86	1.	*	1 JAN 1630	136	1.	*	1 JAN 1810	186	0.
1 JAN 1312	37	1.	*	1 JAN 1452	87	1.	*	1 JAN 1632	137	1.	*	1 JAN 1812	187	0.
1 JAN 1314	38	1.	*	1 JAN 1454	88	1.	*	1 JAN 1634	138	1.	*	1 JAN 1814	188	0.
1 JAN 1316	39	1.	*	1 JAN 1456	89	1.	*	1 JAN 1636	139	1.	*	1 JAN 1816	189	0.
1 JAN 1318	40	1.	*	1 JAN 1458	90	1.	*	1 JAN 1638	140	1.	*	1 JAN 1818	190	0.
1 JAN 1320	41	1.	*	1 JAN 1500	91	1.	*	1 JAN 1640	141	1.	*	1 JAN 1820	191	0.
1 JAN 1322	42	1.	*	1 JAN 1502	92	1.	*	1 JAN 1642	142	1.	*	1 JAN 1822	192	0.
1 JAN 1324	43	1.	*	1 JAN 1504	93	1.	*	1 JAN 1644	143	1.	*	1 JAN 1824	193	0.
1 JAN 1326	44	1.	*	1 JAN 1506	94	1.	*	1 JAN 1646	144	1.	*	1 JAN 1826	194	0.
1 JAN 1328	45	1.	*	1 JAN 1508	95	1.	*	1 JAN 1648	145	1.	*	1 JAN 1828	195	0.
1 JAN 1330	46	1.	*	1 JAN 1510	96	1.	*	1 JAN 1650	146	1.	*	1 JAN 1830	196	0.
1 JAN 1332	47	1.	*	1 JAN 1512	97	1.	*	1 JAN 1652	147	1.	*	1 JAN 1832	197	0.
1 JAN 1334	48	1.	*	1 JAN 1514	98	1.	*	1 JAN 1654	148	1.	*	1 JAN 1834	198	0.
1 JAN 1336	49	1.	*	1 JAN 1516	99	2.	*	1 JAN 1656	149	1.	*	1 JAN 1836	199	0.
1 JAN 1338	50	1.	*	1 JAN 1518	100	2.	*	1 JAN 1658	150	1.	*	1 JAN 1838	200	0.

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PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	6.63-HR
15.	4.10	(CFS)	2.	1.	1.
		(INCHES)	1.071	1.074	1.074
		(AC-FT)	1.	1.	1.

CUMULATIVE AREA = .01 SQ MI

## STATION MW2000B

(O) OUTFLOW

0.	2.	4.	6.	8.	10.	12.	14.	16.	0.	0.	0.	0
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DAHRMN PER

[illegible]

[illegible]

[illegible]

[illegible]

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40 KK \* COMBINE \*  
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41 KO            OUTPUT CONTROL VARIABLES  
                 IPRNT            0   PRINT CONTROL  
                 IPLOT            2   PLOT CONTROL  
                 QSCAL            0.   HYDROGRAPH PLOT SCALE  
                 IPNCH            0   PUNCH COMPUTED HYDROGRAPH  
                 IOUT            21   SAVE HYDROGRAPH ON THIS UNIT  
                 ISAV1            1   FIRST ORDINATE PUNCHED OR SAVED  
                 ISAV2            200   LAST ORDINATE PUNCHED OR SAVED  
                 TIMINT            .033   TIME INTERVAL IN HOURS

42 HC            HYDROGRAPH COMBINATION  
                 ICOMP            2   NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION COMBINE  
SUM OF 2 HYDROGRAPHS

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DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW
					*						*						*					
1	JAN	1200	1	2.	*	1	JAN	1340	51	5.	*	1	JAN	1520	101	12.	*	1	JAN	1700	151	7.
1	JAN	1202	2	2.	*	1	JAN	1342	52	5.	*	1	JAN	1522	102	13.	*	1	JAN	1702	152	7.
1	JAN	1204	3	2.	*	1	JAN	1344	53	5.	*	1	JAN	1524	103	13.	*	1	JAN	1704	153	7.
1	JAN	1206	4	2.	*	1	JAN	1346	54	5.	*	1	JAN	1526	104	13.	*	1	JAN	1706	154	7.
1	JAN	1208	5	3.	*	1	JAN	1348	55	5.	*	1	JAN	1528	105	14.	*	1	JAN	1708	155	7.
1	JAN	1210	6	3.	*	1	JAN	1350	56	5.	*	1	JAN	1530	106	14.	*	1	JAN	1710	156	7.
1	JAN	1212	7	3.	*	1	JAN	1352	57	5.	*	1	JAN	1532	107	14.	*	1	JAN	1712	157	7.
1	JAN	1214	8	3.	*	1	JAN	1354	58	5.	*	1	JAN	1534	108	15.	*	1	JAN	1714	158	7.
1	JAN	1216	9	3.	*	1	JAN	1356	59	5.	*	1	JAN	1536	109	16.	*	1	JAN	1716	159	7.
1	JAN	1218	10	3.	*	1	JAN	1358	60	5.	*	1	JAN	1538	110	17.	*	1	JAN	1718	160	7.
1	JAN	1220	11	3.	*	1	JAN	1400	61	5.	*	1	JAN	1540	111	18.	*	1	JAN	1720	161	7.
1	JAN	1222	12	3.	*	1	JAN	1402	62	5.	*	1	JAN	1542	112	19.	*	1	JAN	1722	162	6.
1	JAN	1224	13	3.	*	1	JAN	1404	63	6.	*	1	JAN	1544	113	20.	*	1	JAN	1724	163	6.
1	JAN	1226	14	3.	*	1	JAN	1406	64	6.	*	1	JAN	1546	114	22.	*	1	JAN	1726	164	6.
1	JAN	1228	15	3.	*	1	JAN	1408	65	6.	*	1	JAN	1548	115	23.	*	1	JAN	1728	165	6.
1	JAN	1230	16	3.	*	1	JAN	1410	66	6.	*	1	JAN	1550	116	24.	*	1	JAN	1730	166	6.
1	JAN	1232	17	3.	*	1	JAN	1412	67	6.	*	1	JAN	1552	117	25.	*	1	JAN	1732	167	6.
1	JAN	1234	18	4.	*	1	JAN	1414	68	6.	*	1	JAN	1554	118	27.	*	1	JAN	1734	168	6.
1	JAN	1236	19	4.	*	1	JAN	1416	69	6.	*	1	JAN	1556	119	31.	*	1	JAN	1736	169	6.
1	JAN	1238	20	4.	*	1	JAN	1418	70	6.	*	1	JAN	1558	120	39.	*	1	JAN	1738	170	6.
1	JAN	1240	21	4.	*	1	JAN	1420	71	6.	*	1	JAN	1600	121	48.	*	1	JAN	1740	171	6.
1	JAN	1242	22	4.	*	1	JAN	1422	72	6.	*	1	JAN	1602	122	57.	*	1	JAN	1742	172	6.



1 JAN 1244	23	4.	*	1 JAN 1424	73	6.	*	1 JAN 1604	123	67.	*	1 JAN 1744	173	6.
1 JAN 1246	24	4.	*	1 JAN 1426	74	6.	*	1 JAN 1606	124	78.	*	1 JAN 1746	174	6.
1 JAN 1248	25	4.	*	1 JAN 1428	75	6.	*	1 JAN 1608	125	82.	*	1 JAN 1748	175	6.
1 JAN 1250	26	4.	*	1 JAN 1430	76	6.	*	1 JAN 1610	126	81.	*	1 JAN 1750	176	6.
1 JAN 1252	27	4.	*	1 JAN 1432	77	7.	*	1 JAN 1612	127	76.	*	1 JAN 1752	177	6.
1 JAN 1254	28	4.	*	1 JAN 1434	78	7.	*	1 JAN 1614	128	69.	*	1 JAN 1754	178	6.
1 JAN 1256	29	4.	*	1 JAN 1436	79	7.	*	1 JAN 1616	129	59.	*	1 JAN 1756	179	6.
1 JAN 1258	30	4.	*	1 JAN 1438	80	7.	*	1 JAN 1618	130	49.	*	1 JAN 1758	180	5.
1 JAN 1300	31	4.	*	1 JAN 1440	81	7.	*	1 JAN 1620	131	41.	*	1 JAN 1800	181	5.
1 JAN 1302	32	4.	*	1 JAN 1442	82	7.	*	1 JAN 1622	132	32.	*	1 JAN 1802	182	5.
1 JAN 1304	33	4.	*	1 JAN 1444	83	7.	*	1 JAN 1624	133	25.	*	1 JAN 1804	183	5.
1 JAN 1306	34	4.	*	1 JAN 1446	84	7.	*	1 JAN 1626	134	20.	*	1 JAN 1806	184	4.
1 JAN 1308	35	4.	*	1 JAN 1448	85	7.	*	1 JAN 1628	135	17.	*	1 JAN 1808	185	4.
1 JAN 1310	36	4.	*	1 JAN 1450	86	8.	*	1 JAN 1630	136	15.	*	1 JAN 1810	186	4.
1 JAN 1312	37	4.	*	1 JAN 1452	87	9.	*	1 JAN 1632	137	13.	*	1 JAN 1812	187	4.
1 JAN 1314	38	4.	*	1 JAN 1454	88	9.	*	1 JAN 1634	138	12.	*	1 JAN 1814	188	4.
1 JAN 1316	39	5.	*	1 JAN 1456	89	9.	*	1 JAN 1636	139	11.	*	1 JAN 1816	189	3.
1 JAN 1318	40	5.	*	1 JAN 1458	90	10.	*	1 JAN 1638	140	11.	*	1 JAN 1818	190	3.
1 JAN 1320	41	5.	*	1 JAN 1500	91	10.	*	1 JAN 1640	141	10.	*	1 JAN 1820	191	3.
1 JAN 1322	42	5.	*	1 JAN 1502	92	10.	*	1 JAN 1642	142	10.	*	1 JAN 1822	192	3.
1 JAN 1324	43	5.	*	1 JAN 1504	93	10.	*	1 JAN 1644	143	9.	*	1 JAN 1824	193	3.
1 JAN 1326	44	5.	*	1 JAN 1506	94	10.	*	1 JAN 1646	144	9.	*	1 JAN 1826	194	3.
1 JAN 1328	45	5.	*	1 JAN 1508	95	10.	*	1 JAN 1648	145	9.	*	1 JAN 1828	195	3.
1 JAN 1330	46	5.	*	1 JAN 1510	96	11.	*	1 JAN 1650	146	8.	*	1 JAN 1830	196	2.
1 JAN 1332	47	5.	*	1 JAN 1512	97	11.	*	1 JAN 1652	147	8.	*	1 JAN 1832	197	2.
1 JAN 1334	48	5.	*	1 JAN 1514	98	11.	*	1 JAN 1654	148	8.	*	1 JAN 1834	198	2.
1 JAN 1336	49	5.	*	1 JAN 1516	99	12.	*	1 JAN 1656	149	8.	*	1 JAN 1836	199	2.
1 JAN 1338	50	5.	*	1 JAN 1518	100	12.	*	1 JAN 1658	150	7.	*	1 JAN 1838	200	2.
		*				*				*				

\*\*\*\*\*

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	6.63-HR
82.	4.13	(CFS)	12.	11.	11.	11.
		(INCHES)	1.164	1.192	1.192	1.192
		(AC-FT)	6.	6.	6.	6.

CUMULATIVE AREA = .09 SQ MI



[illegible]

[illegible]

[illegible]



RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	2000A	94.	4.10	10.	9.	9.	.08		
ROUTED TO	DETAIN	71.	4.17	10.	9.	9.	.08	105.00	4.17
HYDROGRAPH AT	MW2000B	15.	4.10	2.	1.	1.	.01		
2 COMBINED AT	COMBINE	82.	4.13	12.	11.	11.	.09		

\*\*\* NORMAL END OF HEC-1 \*\*\*

## **Drainage Basin 3000**



```

*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*
* JUN 1998
*
* VERSION 4.1
*
* RUN DATE 29JUL09 TIME 14:12:36
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 756-1104
*
*****

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X      X XXXXXXXX XXXXX      X
X      X X      X      X      XX
X      X X      X      X      X
XXXXXXX XXXX      X      XXXXX X
X      X X      X      X      X
X      X X      X      X      X
X      X XXXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

\*\*\* FREE \*\*\*

\*DIAGRAM

```

1 ID MEADOWOOD J-15956 07/16/09 FILE: MW3000D.HC1
2 ID DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)
3 ID R/O=.39, PRECIP=3.6IN, TC 12.35MIN
4 IT 1 01JAN90 1200 700
5 IO 0 2

6 KK 3000
7 KM DRIANAGE BASIN 3000
8 KM RUN DATE 7/16/2009
9 KM RATIONAL METHOD HYDROGRAPH PROGRAM
10 KM COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
11 KM 6HR RAINFALL IS 3.6 INCHES
12 KM RATIONAL METHOD RUNOFF COEFFICIENT IS 0.39
13 KM RATIONAL METHOD TIME OF CONCENTRATION IS 14 MIN.
14 KM FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
15 KM IT 2 01JAN90 1200 200
16 BA 0.0963
17 IN 14 01JAN90 1155
18 QI 0 5.2 5.4 5.6 5.9 6.1 6.6 6.8 7.4 7.8
19 QI 8.6 9.1 10.5 11.4 13.9 15.8 23.2 18.8 131.19 18.6
20 QI 12.5 9.8 8.2 7.1 6.3 5.8 5.3 0 0 0
21 QI 0 0 0 0 0 0 0 0 0 0

22 KK DETAIN
23 KM 100-YEAR DETENTION
24 KO 0 0 0 0 21
25 RS 1 STOR -1
26 SV 0 2.05 2.62 3.29 3.933
27 SQ 0 4.18 10.06 33.13 79.1
28 SE 100 102.4 103 103.69 104
29 ZZ

```

# SCHEMATIC DIAGRAM OF STREAM NETWORK

## INPUT

LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
6	3000	
	V	
	V	
22	DETAIN	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\*\*\*\*\*  
 \*  
 \* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* JUN 1998 \*  
 \* VERSION 4.1 \*  
 \*  
 \* RUN DATE 29JUL09 TIME 14:12:36 \*  
 \*  
 \*\*\*\*\*

\*\*\*\*\*  
 \*  
 \* U.S. ARMY CORPS OF ENGINEERS  
 \* HYDROLOGIC ENGINEERING CENTER  
 \* 609 SECOND STREET  
 \* DAVIS, CALIFORNIA 95616  
 \* (916) 756-1104  
 \*  
 \*\*\*\*\*

MEADOWOOD J-15956 07/16/09 FILE: MW3000D.HC1  
 DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)  
 R/O=.39, PRECIP=3.6IN, TC 12.35MIN

S IO OUTPUT CONTROL VARIABLES  
 IPRNT 0 PRINT CONTROL  
 IPLOT 2 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA  
 NMIN 1 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1JAN90 STARTING DATE  
 ITIME 1200 STARTING TIME  
 NQ 700 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 1JAN90 ENDING DATE  
 NDTIME 2339 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .02 HOURS  
 TOTAL TIME BASE 11.65 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

\*\*\* \*\*

\*\*\*\*\*  
 \*  
 6 KK \* 3000 \*  
 \*  
 \*\*\*\*\*

DRAINAGE BASIN 3000  
 RUN DATE 7/16/2009  
 RATIONAL METHOD HYDROGRAPH PROGRAM  
 COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
 6HR RAINFALL IS 3.6 INCHES  
 RATIONAL METHOD RUNOFF COEFFICIENT IS 0.39

RATIONAL METHOD TIME OF CONCENTRATION IS 14 MIN.  
 FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
 IT 2 01JAN90 1200 200

17 IN TIME DATA FOR INPUT TIME SERIES  
 JXMIN 14 TIME INTERVAL IN MINUTES  
 JXDATE 1JAN90 STARTING DATE  
 JXTIME 1155 STARTING TIME

SUBBASIN RUNOFF DATA

16 BA SUBBASIN CHARACTERISTICS  
 TAREA .10 SUBBASIN AREA

\*\*\*

HYDROGRAPH AT STATION 3000

DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*
1	JAN	1200	1	2.	*	1	JAN	1455	176	11.	*	1	JAN	1750	351	6.	*	1	JAN	2045	526	0.	*
1	JAN	1201	2	2.	*	1	JAN	1456	177	11.	*	1	JAN	1751	352	6.	*	1	JAN	2046	527	0.	*
1	JAN	1202	3	3.	*	1	JAN	1457	178	11.	*	1	JAN	1752	353	6.	*	1	JAN	2047	528	0.	*
1	JAN	1203	4	3.	*	1	JAN	1458	179	12.	*	1	JAN	1753	354	6.	*	1	JAN	2048	529	0.	*
1	JAN	1204	5	3.	*	1	JAN	1459	180	12.	*	1	JAN	1754	355	5.	*	1	JAN	2049	530	0.	*
1	JAN	1205	6	4.	*	1	JAN	1500	181	12.	*	1	JAN	1755	356	5.	*	1	JAN	2050	531	0.	*
1	JAN	1206	7	4.	*	1	JAN	1501	182	12.	*	1	JAN	1756	357	5.	*	1	JAN	2051	532	0.	*
1	JAN	1207	8	4.	*	1	JAN	1502	183	12.	*	1	JAN	1757	358	5.	*	1	JAN	2052	533	0.	*
1	JAN	1208	9	5.	*	1	JAN	1503	184	12.	*	1	JAN	1758	359	5.	*	1	JAN	2053	534	0.	*
1	JAN	1209	10	5.	*	1	JAN	1504	185	13.	*	1	JAN	1759	360	5.	*	1	JAN	2054	535	0.	*
1	JAN	1210	11	5.	*	1	JAN	1505	186	13.	*	1	JAN	1800	361	5.	*	1	JAN	2055	536	0.	*
1	JAN	1211	12	5.	*	1	JAN	1506	187	13.	*	1	JAN	1801	362	5.	*	1	JAN	2056	537	0.	*
1	JAN	1212	13	5.	*	1	JAN	1507	188	13.	*	1	JAN	1802	363	4.	*	1	JAN	2057	538	0.	*
1	JAN	1213	14	5.	*	1	JAN	1508	189	13.	*	1	JAN	1803	364	4.	*	1	JAN	2058	539	0.	*
1	JAN	1214	15	5.	*	1	JAN	1509	190	14.	*	1	JAN	1804	365	3.	*	1	JAN	2059	540	0.	*
1	JAN	1215	16	5.	*	1	JAN	1510	191	14.	*	1	JAN	1805	366	3.	*	1	JAN	2100	541	0.	*
1	JAN	1216	17	5.	*	1	JAN	1511	192	14.	*	1	JAN	1806	367	3.	*	1	JAN	2101	542	0.	*
1	JAN	1217	18	5.	*	1	JAN	1512	193	14.	*	1	JAN	1807	368	2.	*	1	JAN	2102	543	0.	*
1	JAN	1218	19	5.	*	1	JAN	1513	194	14.	*	1	JAN	1808	369	2.	*	1	JAN	2103	544	0.	*
1	JAN	1219	20	5.	*	1	JAN	1514	195	14.	*	1	JAN	1809	370	2.	*	1	JAN	2104	545	0.	*
1	JAN	1220	21	5.	*	1	JAN	1515	196	14.	*	1	JAN	1810	371	1.	*	1	JAN	2105	546	0.	*
1	JAN	1221	22	5.	*	1	JAN	1516	197	15.	*	1	JAN	1811	372	1.	*	1	JAN	2106	547	0.	*
1	JAN	1222	23	5.	*	1	JAN	1517	198	15.	*	1	JAN	1812	373	0.	*	1	JAN	2107	548	0.	*
1	JAN	1223	24	5.	*	1	JAN	1518	199	15.	*	1	JAN	1813	374	0.	*	1	JAN	2108	549	0.	*
1	JAN	1224	25	5.	*	1	JAN	1519	200	15.	*	1	JAN	1814	375	0.	*	1	JAN	2109	550	0.	*
1	JAN	1225	26	5.	*	1	JAN	1520	201	15.	*	1	JAN	1815	376	0.	*	1	JAN	2110	551	0.	*
1	JAN	1226	27	5.	*	1	JAN	1521	202	15.	*	1	JAN	1816	377	0.	*	1	JAN	2111	552	0.	*
1	JAN	1227	28	5.	*	1	JAN	1522	203	15.	*	1	JAN	1817	378	0.	*	1	JAN	2112	553	0.	*
1	JAN	1228	29	5.	*	1	JAN	1523	204	16.	*	1	JAN	1818	379	0.	*	1	JAN	2113	554	0.	*
1	JAN	1229	30	5.	*	1	JAN	1524	205	16.	*	1	JAN	1819	380	0.	*	1	JAN	2114	555	0.	*
1	JAN	1230	31	6.	*	1	JAN	1525	206	16.	*	1	JAN	1820	381	0.	*	1	JAN	2115	556	0.	*
1	JAN	1231	32	6.	*	1	JAN	1526	207	16.	*	1	JAN	1821	382	0.	*	1	JAN	2116	557	0.	*
1	JAN	1232	33	6.	*	1	JAN	1527	208	17.	*	1	JAN	1822	383	0.	*	1	JAN	2117	558	0.	*
1	JAN	1233	34	6.	*	1	JAN	1528	209	17.	*	1	JAN	1823	384	0.	*	1	JAN	2118	559	0.	*
1	JAN	1234	35	6.	*	1	JAN	1529	210	18.	*	1	JAN	1824	385	0.	*	1	JAN	2119	560	0.	*
1	JAN	1235	36	6.	*	1	JAN	1530	211	18.	*	1	JAN	1825	386	0.	*	1	JAN	2120	561	0.	*

1 JAN 1236	37	6.	*	1 JAN 1531	212	19.	*	1 JAN 1826	387	0.	*	1 JAN 2121	562	0.
1 JAN 1237	38	6.	*	1 JAN 1532	213	20.	*	1 JAN 1827	388	0.	*	1 JAN 2122	563	0.
1 JAN 1238	39	6.	*	1 JAN 1533	214	20.	*	1 JAN 1828	389	0.	*	1 JAN 2123	564	0.
1 JAN 1239	40	6.	*	1 JAN 1534	215	21.	*	1 JAN 1829	390	0.	*	1 JAN 2124	565	0.
1 JAN 1240	41	6.	*	1 JAN 1535	216	21.	*	1 JAN 1830	391	0.	*	1 JAN 2125	566	0.
1 JAN 1241	42	6.	*	1 JAN 1536	217	22.	*	1 JAN 1831	392	0.	*	1 JAN 2126	567	0.
1 JAN 1242	43	6.	*	1 JAN 1537	218	22.	*	1 JAN 1832	393	0.	*	1 JAN 2127	568	0.
1 JAN 1243	44	6.	*	1 JAN 1538	219	23.	*	1 JAN 1833	394	0.	*	1 JAN 2128	569	0.
1 JAN 1244	45	6.	*	1 JAN 1539	220	23.	*	1 JAN 1834	395	0.	*	1 JAN 2129	570	0.
1 JAN 1245	46	6.	*	1 JAN 1540	221	23.	*	1 JAN 1835	396	0.	*	1 JAN 2130	571	0.
1 JAN 1246	47	6.	*	1 JAN 1541	222	23.	*	1 JAN 1836	397	0.	*	1 JAN 2131	572	0.
1 JAN 1247	48	6.	*	1 JAN 1542	223	22.	*	1 JAN 1837	398	0.	*	1 JAN 2132	573	0.
1 JAN 1248	49	6.	*	1 JAN 1543	224	22.	*	1 JAN 1838	399	0.	*	1 JAN 2133	574	0.
1 JAN 1249	50	6.	*	1 JAN 1544	225	22.	*	1 JAN 1839	400	0.	*	1 JAN 2134	575	0.
1 JAN 1250	51	6.	*	1 JAN 1545	226	21.	*	1 JAN 1840	401	0.	*	1 JAN 2135	576	0.
1 JAN 1251	52	6.	*	1 JAN 1546	227	21.	*	1 JAN 1841	402	0.	*	1 JAN 2136	577	0.
1 JAN 1252	53	6.	*	1 JAN 1547	228	21.	*	1 JAN 1842	403	0.	*	1 JAN 2137	578	0.
1 JAN 1253	54	6.	*	1 JAN 1548	229	20.	*	1 JAN 1843	404	0.	*	1 JAN 2138	579	0.
1 JAN 1254	55	6.	*	1 JAN 1549	230	20.	*	1 JAN 1844	405	0.	*	1 JAN 2139	580	0.
1 JAN 1255	56	6.	*	1 JAN 1550	231	20.	*	1 JAN 1845	406	0.	*	1 JAN 2140	581	0.
1 JAN 1256	57	6.	*	1 JAN 1551	232	19.	*	1 JAN 1846	407	0.	*	1 JAN 2141	582	0.
1 JAN 1257	58	6.	*	1 JAN 1552	233	19.	*	1 JAN 1847	408	0.	*	1 JAN 2142	583	0.
1 JAN 1258	59	6.	*	1 JAN 1553	234	19.	*	1 JAN 1848	409	0.	*	1 JAN 2143	584	0.
1 JAN 1259	60	6.	*	1 JAN 1554	235	27.	*	1 JAN 1849	410	0.	*	1 JAN 2144	585	0.
1 JAN 1300	61	6.	*	1 JAN 1555	236	35.	*	1 JAN 1850	411	0.	*	1 JAN 2145	586	0.
1 JAN 1301	62	6.	*	1 JAN 1556	237	43.	*	1 JAN 1851	412	0.	*	1 JAN 2146	587	0.
1 JAN 1302	63	6.	*	1 JAN 1557	238	51.	*	1 JAN 1852	413	0.	*	1 JAN 2147	588	0.
1 JAN 1303	64	6.	*	1 JAN 1558	239	59.	*	1 JAN 1853	414	0.	*	1 JAN 2148	589	0.
1 JAN 1304	65	6.	*	1 JAN 1559	240	67.	*	1 JAN 1854	415	0.	*	1 JAN 2149	590	0.
1 JAN 1305	66	6.	*	1 JAN 1600	241	75.	*	1 JAN 1855	416	0.	*	1 JAN 2150	591	0.
1 JAN 1306	67	6.	*	1 JAN 1601	242	83.	*	1 JAN 1856	417	0.	*	1 JAN 2151	592	0.
1 JAN 1307	68	6.	*	1 JAN 1602	243	91.	*	1 JAN 1857	418	0.	*	1 JAN 2152	593	0.
1 JAN 1308	69	6.	*	1 JAN 1603	244	99.	*	1 JAN 1858	419	0.	*	1 JAN 2153	594	0.
1 JAN 1309	70	6.	*	1 JAN 1604	245	107.	*	1 JAN 1859	420	0.	*	1 JAN 2154	595	0.
1 JAN 1310	71	6.	*	1 JAN 1605	246	115.	*	1 JAN 1900	421	0.	*	1 JAN 2155	596	0.
1 JAN 1311	72	6.	*	1 JAN 1606	247	123.	*	1 JAN 1901	422	0.	*	1 JAN 2156	597	0.
1 JAN 1312	73	6.	*	1 JAN 1607	248	131.	*	1 JAN 1902	423	0.	*	1 JAN 2157	598	0.
1 JAN 1313	74	6.	*	1 JAN 1608	249	123.	*	1 JAN 1903	424	0.	*	1 JAN 2158	599	0.
1 JAN 1314	75	6.	*	1 JAN 1609	250	115.	*	1 JAN 1904	425	0.	*	1 JAN 2159	600	0.
1 JAN 1315	76	6.	*	1 JAN 1610	251	107.	*	1 JAN 1905	426	0.	*	1 JAN 2200	601	0.
1 JAN 1316	77	6.	*	1 JAN 1611	252	99.	*	1 JAN 1906	427	0.	*	1 JAN 2201	602	0.
1 JAN 1317	78	7.	*	1 JAN 1612	253	91.	*	1 JAN 1907	428	0.	*	1 JAN 2202	603	0.
1 JAN 1318	79	7.	*	1 JAN 1613	254	83.	*	1 JAN 1908	429	0.	*	1 JAN 2203	604	0.
1 JAN 1319	80	7.	*	1 JAN 1614	255	75.	*	1 JAN 1909	430	0.	*	1 JAN 2204	605	0.
1 JAN 1320	81	7.	*	1 JAN 1615	256	67.	*	1 JAN 1910	431	0.	*	1 JAN 2205	606	0.
1 JAN 1321	82	7.	*	1 JAN 1616	257	59.	*	1 JAN 1911	432	0.	*	1 JAN 2206	607	0.
1 JAN 1322	83	7.	*	1 JAN 1617	258	51.	*	1 JAN 1912	433	0.	*	1 JAN 2207	608	0.
1 JAN 1323	84	7.	*	1 JAN 1618	259	43.	*	1 JAN 1913	434	0.	*	1 JAN 2208	609	0.
1 JAN 1324	85	7.	*	1 JAN 1619	260	35.	*	1 JAN 1914	435	0.	*	1 JAN 2209	610	0.
1 JAN 1325	86	7.	*	1 JAN 1620	261	27.	*	1 JAN 1915	436	0.	*	1 JAN 2210	611	0.
1 JAN 1326	87	7.	*	1 JAN 1621	262	19.	*	1 JAN 1916	437	0.	*	1 JAN 2211	612	0.
1 JAN 1327	88	7.	*	1 JAN 1622	263	18.	*	1 JAN 1917	438	0.	*	1 JAN 2212	613	0.
1 JAN 1328	89	7.	*	1 JAN 1623	264	18.	*	1 JAN 1918	439	0.	*	1 JAN 2213	614	0.
1 JAN 1329	90	7.	*	1 JAN 1624	265	17.	*	1 JAN 1919	440	0.	*	1 JAN 2214	615	0.
1 JAN 1330	91	7.	*	1 JAN 1625	266	17.	*	1 JAN 1920	441	0.	*	1 JAN 2215	616	0.
1 JAN 1331	92	7.	*	1 JAN 1626	267	16.	*	1 JAN 1921	442	0.	*	1 JAN 2216	617	0.
1 JAN 1332	93	7.	*	1 JAN 1627	268	16.	*	1 JAN 1922	443	0.	*	1 JAN 2217	618	0.
1 JAN 1333	94	7.	*	1 JAN 1628	269	16.	*	1 JAN 1923	444	0.	*	1 JAN 2218	619	0.
1 JAN 1334	95	7.	*	1 JAN 1629	270	15.	*	1 JAN 1924	445	0.	*	1 JAN 2219	620	0.
1 JAN 1335	96	7.	*	1 JAN 1630	271	15.	*	1 JAN 1925	446	0.	*	1 JAN 2220	621	0.

1 JAN 1336 97	7. *	1 JAN 1631 272	14. *	1 JAN 1926 447	0. *	1 JAN 2221 622	0.
1 JAN 1337 98	7. *	1 JAN 1632 273	14. *	1 JAN 1927 448	0. *	1 JAN 2222 623	0.
1 JAN 1338 99	7. *	1 JAN 1633 274	13. *	1 JAN 1928 449	0. *	1 JAN 2223 624	0.
1 JAN 1339 100	7. *	1 JAN 1634 275	13. *	1 JAN 1929 450	0. *	1 JAN 2224 625	0.
1 JAN 1340 101	7. *	1 JAN 1635 276	13. *	1 JAN 1930 451	0. *	1 JAN 2225 626	0.
1 JAN 1341 102	7. *	1 JAN 1636 277	12. *	1 JAN 1931 452	0. *	1 JAN 2226 627	0.
1 JAN 1342 103	7. *	1 JAN 1637 278	12. *	1 JAN 1932 453	0. *	1 JAN 2227 628	0.
1 JAN 1343 104	7. *	1 JAN 1638 279	12. *	1 JAN 1933 454	0. *	1 JAN 2228 629	0.
1 JAN 1344 105	7. *	1 JAN 1639 280	12. *	1 JAN 1934 455	0. *	1 JAN 2229 630	0.
1 JAN 1345 106	7. *	1 JAN 1640 281	12. *	1 JAN 1935 456	0. *	1 JAN 2230 631	0.
1 JAN 1346 107	7. *	1 JAN 1641 282	11. *	1 JAN 1936 457	0. *	1 JAN 2231 632	0.
1 JAN 1347 108	7. *	1 JAN 1642 283	11. *	1 JAN 1937 458	0. *	1 JAN 2232 633	0.
1 JAN 1348 109	7. *	1 JAN 1643 284	11. *	1 JAN 1938 459	0. *	1 JAN 2233 634	0.
1 JAN 1349 110	7. *	1 JAN 1644 285	11. *	1 JAN 1939 460	0. *	1 JAN 2234 635	0.
1 JAN 1350 111	7. *	1 JAN 1645 286	11. *	1 JAN 1940 461	0. *	1 JAN 2235 636	0.
1 JAN 1351 112	8. *	1 JAN 1646 287	10. *	1 JAN 1941 462	0. *	1 JAN 2236 637	0.
1 JAN 1352 113	8. *	1 JAN 1647 288	10. *	1 JAN 1942 463	0. *	1 JAN 2237 638	0.
1 JAN 1353 114	8. *	1 JAN 1648 289	10. *	1 JAN 1943 464	0. *	1 JAN 2238 639	0.
1 JAN 1354 115	8. *	1 JAN 1649 290	10. *	1 JAN 1944 465	0. *	1 JAN 2239 640	0.
1 JAN 1355 116	8. *	1 JAN 1650 291	10. *	1 JAN 1945 466	0. *	1 JAN 2240 641	0.
1 JAN 1356 117	8. *	1 JAN 1651 292	10. *	1 JAN 1946 467	0. *	1 JAN 2241 642	0.
1 JAN 1357 118	8. *	1 JAN 1652 293	9. *	1 JAN 1947 468	0. *	1 JAN 2242 643	0.
1 JAN 1358 119	8. *	1 JAN 1653 294	9. *	1 JAN 1948 469	0. *	1 JAN 2243 644	0.
1 JAN 1359 120	8. *	1 JAN 1654 295	9. *	1 JAN 1949 470	0. *	1 JAN 2244 645	0.
1 JAN 1400 121	8. *	1 JAN 1655 296	9. *	1 JAN 1950 471	0. *	1 JAN 2245 646	0.
1 JAN 1401 122	8. *	1 JAN 1656 297	9. *	1 JAN 1951 472	0. *	1 JAN 2246 647	0.
1 JAN 1402 123	8. *	1 JAN 1657 298	9. *	1 JAN 1952 473	0. *	1 JAN 2247 648	0.
1 JAN 1403 124	8. *	1 JAN 1658 299	9. *	1 JAN 1953 474	0. *	1 JAN 2248 649	0.
1 JAN 1404 125	8. *	1 JAN 1659 300	9. *	1 JAN 1954 475	0. *	1 JAN 2249 650	0.
1 JAN 1405 126	8. *	1 JAN 1700 301	9. *	1 JAN 1955 476	0. *	1 JAN 2250 651	0.
1 JAN 1406 127	8. *	1 JAN 1701 302	8. *	1 JAN 1956 477	0. *	1 JAN 2251 652	0.
1 JAN 1407 128	8. *	1 JAN 1702 303	8. *	1 JAN 1957 478	0. *	1 JAN 2252 653	0.
1 JAN 1408 129	8. *	1 JAN 1703 304	8. *	1 JAN 1958 479	0. *	1 JAN 2253 654	0.
1 JAN 1409 130	8. *	1 JAN 1704 305	8. *	1 JAN 1959 480	0. *	1 JAN 2254 655	0.
1 JAN 1410 131	8. *	1 JAN 1705 306	8. *	1 JAN 2000 481	0. *	1 JAN 2255 656	0.
1 JAN 1411 132	8. *	1 JAN 1706 307	8. *	1 JAN 2001 482	0. *	1 JAN 2256 657	0.
1 JAN 1412 133	8. *	1 JAN 1707 308	8. *	1 JAN 2002 483	0. *	1 JAN 2257 658	0.
1 JAN 1413 134	8. *	1 JAN 1708 309	8. *	1 JAN 2003 484	0. *	1 JAN 2258 659	0.
1 JAN 1414 135	9. *	1 JAN 1709 310	8. *	1 JAN 2004 485	0. *	1 JAN 2259 660	0.
1 JAN 1415 136	9. *	1 JAN 1710 311	8. *	1 JAN 2005 486	0. *	1 JAN 2300 661	0.
1 JAN 1416 137	9. *	1 JAN 1711 312	8. *	1 JAN 2006 487	0. *	1 JAN 2301 662	0.
1 JAN 1417 138	9. *	1 JAN 1712 313	7. *	1 JAN 2007 488	0. *	1 JAN 2302 663	0.
1 JAN 1418 139	9. *	1 JAN 1713 314	7. *	1 JAN 2008 489	0. *	1 JAN 2303 664	0.
1 JAN 1419 140	9. *	1 JAN 1714 315	7. *	1 JAN 2009 490	0. *	1 JAN 2304 665	0.
1 JAN 1420 141	9. *	1 JAN 1715 316	7. *	1 JAN 2010 491	0. *	1 JAN 2305 666	0.
1 JAN 1421 142	9. *	1 JAN 1716 317	7. *	1 JAN 2011 492	0. *	1 JAN 2306 667	0.
1 JAN 1422 143	9. *	1 JAN 1717 318	7. *	1 JAN 2012 493	0. *	1 JAN 2307 668	0.
1 JAN 1423 144	9. *	1 JAN 1718 319	7. *	1 JAN 2013 494	0. *	1 JAN 2308 669	0.
1 JAN 1424 145	9. *	1 JAN 1719 320	7. *	1 JAN 2014 495	0. *	1 JAN 2309 670	0.
1 JAN 1425 146	9. *	1 JAN 1720 321	7. *	1 JAN 2015 496	0. *	1 JAN 2310 671	0.
1 JAN 1426 147	9. *	1 JAN 1721 322	7. *	1 JAN 2016 497	0. *	1 JAN 2311 672	0.
1 JAN 1427 148	9. *	1 JAN 1722 323	7. *	1 JAN 2017 498	0. *	1 JAN 2312 673	0.
1 JAN 1428 149	9. *	1 JAN 1723 324	7. *	1 JAN 2018 499	0. *	1 JAN 2313 674	0.
1 JAN 1429 150	9. *	1 JAN 1724 325	7. *	1 JAN 2019 500	0. *	1 JAN 2314 675	0.
1 JAN 1430 151	9. *	1 JAN 1725 326	7. *	1 JAN 2020 501	0. *	1 JAN 2315 676	0.
1 JAN 1431 152	9. *	1 JAN 1726 327	7. *	1 JAN 2021 502	0. *	1 JAN 2316 677	0.
1 JAN 1432 153	9. *	1 JAN 1727 328	7. *	1 JAN 2022 503	0. *	1 JAN 2317 678	0.
1 JAN 1433 154	10. *	1 JAN 1728 329	6. *	1 JAN 2023 504	0. *	1 JAN 2318 679	0.
1 JAN 1434 155	10. *	1 JAN 1729 330	6. *	1 JAN 2024 505	0. *	1 JAN 2319 680	0.
1 JAN 1435 156	10. *	1 JAN 1730 331	6. *	1 JAN 2025 506	0. *	1 JAN 2320 681	0.

1 JAN 1436 157	10.	*	1 JAN 1731 332	6.	*	1 JAN 2026 507	0.	*	1 JAN 2321 682	0.
1 JAN 1437 158	10.	*	1 JAN 1732 333	6.	*	1 JAN 2027 508	0.	*	1 JAN 2322 683	0.
1 JAN 1438 159	10.	*	1 JAN 1733 334	6.	*	1 JAN 2028 509	0.	*	1 JAN 2323 684	0.
1 JAN 1439 160	10.	*	1 JAN 1734 335	6.	*	1 JAN 2029 510	0.	*	1 JAN 2324 685	0.
1 JAN 1440 161	10.	*	1 JAN 1735 336	6.	*	1 JAN 2030 511	0.	*	1 JAN 2325 686	0.
1 JAN 1441 162	10.	*	1 JAN 1736 337	6.	*	1 JAN 2031 512	0.	*	1 JAN 2326 687	0.
1 JAN 1442 163	10.	*	1 JAN 1737 338	6.	*	1 JAN 2032 513	0.	*	1 JAN 2327 688	0.
1 JAN 1443 164	11.	*	1 JAN 1738 339	6.	*	1 JAN 2033 514	0.	*	1 JAN 2328 689	0.
1 JAN 1444 165	11.	*	1 JAN 1739 340	6.	*	1 JAN 2034 515	0.	*	1 JAN 2329 690	0.
1 JAN 1445 166	11.	*	1 JAN 1740 341	6.	*	1 JAN 2035 516	0.	*	1 JAN 2330 691	0.
1 JAN 1446 167	11.	*	1 JAN 1741 342	6.	*	1 JAN 2036 517	0.	*	1 JAN 2331 692	0.
1 JAN 1447 168	11.	*	1 JAN 1742 343	6.	*	1 JAN 2037 518	0.	*	1 JAN 2332 693	0.
1 JAN 1448 169	11.	*	1 JAN 1743 344	6.	*	1 JAN 2038 519	0.	*	1 JAN 2333 694	0.
1 JAN 1449 170	11.	*	1 JAN 1744 345	6.	*	1 JAN 2039 520	0.	*	1 JAN 2334 695	0.
1 JAN 1450 171	11.	*	1 JAN 1745 346	6.	*	1 JAN 2040 521	0.	*	1 JAN 2335 696	0.
1 JAN 1451 172	11.	*	1 JAN 1746 347	6.	*	1 JAN 2041 522	0.	*	1 JAN 2336 697	0.
1 JAN 1452 173	11.	*	1 JAN 1747 348	6.	*	1 JAN 2042 523	0.	*	1 JAN 2337 698	0.
1 JAN 1453 174	11.	*	1 JAN 1748 349	6.	*	1 JAN 2043 524	0.	*	1 JAN 2338 699	0.
1 JAN 1454 175	11.	*	1 JAN 1749 350	6.	*	1 JAN 2044 525	0.	*	1 JAN 2339 700	0.
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PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	11.65-HR
131.	4.12	(CFS)	14.	7.	7.	7.
		(INCHES)	1.392	1.399	1.399	1.399
		(AC-FT)	7.	7.	7.	7.

CUMULATIVE AREA = .10 SQ MI



3000

(O) OUTFLOW

0.	20.	40.	60.	80.	100.	120.	140.	0.	0.	0.	0.	0.
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DAHRMN PER

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

[illegible]

11755	356.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11756	357.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11757	358.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11758	359.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11759	360.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11800	361.	O	. . . . .	.	.	.	.	.	.	.	.	.	.	.	.
11801	362.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11802	363.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11803	364.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11804	365.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11805	366.	O	.	.	.	.	.	.	.	.	.	.	.	.	.
11806	367.O		.	.	.	.	.	.	.	.	.	.	.	.	.
11807	368.O		.	.	.	.	.	.	.	.	.	.	.	.	.
11808	369.O		.	.	.	.	.	.	.	.	.	.	.	.	.
11809	370.O		.	.	.	.	.	.	.	.	.	.	.	.	.
11810	371.O.		. . . . .	.	.	.	.	.	.	.	.	.	.	.	.
11811	372O		.	.	.	.	.	.	.	.	.	.	.	.	.
11812	373O		.	.	.	.	.	.	.	.	.	.	.	.	.
11813	374O		.	.	.	.	.	.	.	.	.	.	.	.	.
11814	375O		.	.	.	.	.	.	.	.	.	.	.	.	.
11815	376O		.	.	.	.	.	.	.	.	.	.	.	.	.
11816	377O		.	.	.	.	.	.	.	.	.	.	.	.	.
11817	378O		.	.	.	.	.	.	.	.	.	.	.	.	.
11818	379O		.	.	.	.	.	.	.	.	.	.	.	.	.
11819	380O		.	.	.	.	.	.	.	.	.	.	.	.	.
11820	381O		. . . . .	.	.	.	.	.	.	.	.	.	.	.	.
11821	382O		.	.	.	.	.	.	.	.	.	.	.	.	.
11822	383O		.	.	.	.	.	.	.	.	.	.	.	.	.
11823	384O		.	.	.	.	.	.	.	.	.	.	.	.	.
11824	385O		.	.	.	.	.	.	.	.	.	.	.	.	.
11825	386O		.	.	.	.	.	.	.	.	.	.	.	.	.
11826	387O		.	.	.	.	.	.	.	.	.	.	.	.	.
11827	388O		.	.	.	.	.	.	.	.	.	.	.	.	.
11828	389O		.	.	.	.	.	.	.	.	.	.	.	.	.
11829	390O		.	.	.	.	.	.	.	.	.	.	.	.	.
11830	391O		. . . . .	.	.	.	.	.	.	.	.	.	.	.	.
11831	392O		.	.	.	.	.	.	.	.	.	.	.	.	.
11832	393O		.	.	.	.	.	.	.	.	.	.	.	.	.
11833	394O		.	.	.	.	.	.	.	.	.	.	.	.	.
11834	395O		.	.	.	.	.	.	.	.	.	.	.	.	.
11835	396O		.	.	.	.	.	.	.	.	.	.	.	.	.
11836	397O		.	.	.	.	.	.	.	.	.	.	.	.	.
11837	398O		.	.	.	.	.	.	.	.	.	.	.	.	.
11838	399O		.	.	.	.	.	.	.	.	.	.	.	.	.
11839	400O		.	.	.	.	.	.	.	.	.	.	.	.	.
11840	401O		. . . . .	.	.	.	.	.	.	.	.	.	.	.	.
11841	402O		.	.	.	.	.	.	.	.	.	.	.	.	.
11842	403O		.	.	.	.	.	.	.	.	.	.	.	.	.
11843	404O		.	.	.	.	.	.	.	.	.	.	.	.	.
11844	405O		.	.	.	.	.	.	.	.	.	.	.	.	.
11845	406O		.	.	.	.	.	.	.	.	.	.	.	.	.
11846	407O		.	.	.	.									

11855	4160
11856	4170
11857	4180
11858	4190
11859	4200
11900	4210
11901	4220
11902	4230
11903	4240
11904	4250
11905	4260
11906	4270
11907	4280
11908	4290
11909	4300
11910	4310
11911	4320
11912	4330
11913	4340
11914	4350
11915	4360
11916	4370
11917	4380
11918	4390
11919	4400
11920	4410
11921	4420
11922	4430
11923	4440
11924	4450
11925	4460
11926	4470
11927	4480
11928	4490
11929	4500
11930	4510
11931	4520
11932	4530
11933	4540
11934	4550
11935	4560
11936	4570
11937	4580
11938	4590
11939	4600
11940	4610
11941	4620
11942	4630
11943	4640
11944	4650
11945	4660
11946	4670
11947	4680
11948	4690
11949	4700
11950	4710
11951	4720
11952	4730
11953	4740
11954	4750



[illegible]

12055	5360
12056	5370
12057	5380
12058	5390
12059	5400
12100	5410
12101	5420
12102	5430
12103	5440
12104	5450
12105	5460
12106	5470
12107	5480
12108	5490
12109	5500
12110	5510
12111	5520
12112	5530
12113	5540
12114	5550
12115	5560
12116	5570
12117	5580
12118	5590
12119	5600
12120	5610
12121	5620
12122	5630
12123	5640
12124	5650
12125	5660
12126	5670
12127	5680
12128	5690
12129	5700
12130	5710
12131	5720
12132	5730
12133	5740
12134	5750
12135	5760
12136	5770
12137	5780
12138	5790
12139	5800
12140	5810
12141	5820
12142	5830
12143	5840
12144	5850
12145	5860
12146	5870
12147	5880
12148	5890
12149	5900
12150	5910
12151	5920
12152	5930
12153	5940
12154	5950

[illegible]

12255	6560
12256	6570
12257	6580
12258	6590
12259	6600
12300	6610
12301	6620
12302	6630
12303	6640
12304	6650
12305	6660
12306	6670
12307	6680
12308	6690
12309	6700
12310	6710
12311	6720
12312	6730
12313	6740
12314	6750
12315	6760
12316	6770
12317	6780
12318	6790
12319	6800
12320	6810
12321	6820
12322	6830
12323	6840
12324	6850
12325	6860
12326	6870
12327	6880
12328	6890
12329	6900
12330	6910
12331	6920
12332	6930
12333	6940
12334	6950
12335	6960
12336	6970
12337	6980
12338	6990
12339	7000

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22 KK \* DETAIN \*  
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100-YEAR DETENTION

24 KO OUTPUT CONTROL VARIABLES  
IPRNT 0 PRINT CONTROL  
IPLOT 2 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 700 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .017 TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

25 RS STORAGE ROUTING  
NSTPS 1 NUMBER OF SUBREACHES  
ITYP STOR TYPE OF INITIAL CONDITION  
RSVRIC -1.00 INITIAL CONDITION  
X .00 WORKING R AND D COEFFICIENT  
  
26 SV STORAGE .0 2.0 2.6 3.3 3.9  
  
27 SQ DISCHARGE 0. 4. 10. 33. 79.  
  
28 SE ELEVATION 100.00 102.40 103.00 103.69 104.00

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HYDROGRAPH AT STATION DETAIN

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DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
1	JAN	1200	1	2.	.9	101.1	*	1	JAN	1554	235	14.	2.7	103.1	*	1	JAN	1948	469	4.	1.8	102.1
1	JAN	1201	2	2.	.9	101.1	*	1	JAN	1555	236	15.	2.8	103.1	*	1	JAN	1949	470	4.	1.8	102.1
1	JAN	1202	3	2.	.9	101.1	*	1	JAN	1556	237	16.	2.8	103.2	*	1	JAN	1950	471	4.	1.7	102.0
1	JAN	1203	4	2.	.9	101.1	*	1	JAN	1557	238	17.	2.8	103.2	*	1	JAN	1951	472	4.	1.7	102.0
1	JAN	1204	5	2.	.9	101.1	*	1	JAN	1558	239	19.	2.9	103.3	*	1	JAN	1952	473	4.	1.7	102.0
1	JAN	1205	6	2.	.9	101.1	*	1	JAN	1559	240	21.	2.9	103.3	*	1	JAN	1953	474	4.	1.7	102.0
1	JAN	1206	7	2.	.9	101.1	*	1	JAN	1600	241	23.	3.0	103.4	*	1	JAN	1954	475	4.	1.7	102.0
1	JAN	1207	8	2.	.9	101.1	*	1	JAN	1601	242	26.	3.1	103.5	*	1	JAN	1955	476	4.	1.7	102.0
1	JAN	1208	9	2.	.9	101.1	*	1	JAN	1602	243	29.	3.2	103.6	*	1	JAN	1956	477	4.	1.7	102.0
1	JAN	1209	10	2.	.9	101.1	*	1	JAN	1603	244	32.	3.3	103.7	*	1	JAN	1957	478	3.	1.7	102.0
1	JAN	1210	11	2.	.9	101.1	*	1	JAN	1604	245	37.	3.3	103.7	*	1	JAN	1958	479	3.	1.7	102.0

1 JAN 1211 12	2.	.9	101.1 *	1 JAN 1605 246	44.	3.4	103.8 *	1 JAN 1959 480	3.	1.7	102.0
1 JAN 1212 13	2.	.9	101.1 *	1 JAN 1606 247	51.	3.5	103.8 *	1 JAN 2000 481	3.	1.7	102.0
1 JAN 1213 14	2.	.9	101.1 *	1 JAN 1607 248	58.	3.6	103.9 *	1 JAN 2001 482	3.	1.7	102.0
1 JAN 1214 15	2.	1.0	101.1 *	1 JAN 1608 249	65.	3.7	103.9 *	1 JAN 2002 483	3.	1.7	102.0
1 JAN 1215 16	2.	1.0	101.1 *	1 JAN 1609 250	70.	3.8	103.9 *	1 JAN 2003 484	3.	1.7	102.0
1 JAN 1216 17	2.	1.0	101.1 *	1 JAN 1610 251	74.	3.9	104.0 *	1 JAN 2004 485	3.	1.7	102.0
1 JAN 1217 18	2.	1.0	101.2 *	1 JAN 1611 252	77.	3.9	104.0 *	1 JAN 2005 486	3.	1.7	102.0
1 JAN 1218 19	2.	1.0	101.1 *	1 JAN 1612 253	78.	3.9	104.0 *	1 JAN 2006 487	3.	1.7	102.0
1 JAN 1219 20	2.	1.0	101.1 *	1 JAN 1613 254	79.	3.9	104.0 *	1 JAN 2007 488	3.	1.7	101.9
1 JAN 1220 21	2.	1.0	101.1 *	1 JAN 1614 255	79.	3.9	104.0 *	1 JAN 2008 489	3.	1.7	101.9
1 JAN 1221 22	2.	1.0	101.2 *	1 JAN 1615 256	78.	3.9	104.0 *	1 JAN 2009 490	3.	1.7	101.9
1 JAN 1222 23	2.	1.0	101.2 *	1 JAN 1616 257	77.	3.9	104.0 *	1 JAN 2010 491	3.	1.7	101.9
1 JAN 1223 24	2.	1.0	101.2 *	1 JAN 1617 258	75.	3.9	104.0 *	1 JAN 2011 492	3.	1.6	101.9
1 JAN 1224 25	2.	1.0	101.2 *	1 JAN 1618 259	72.	3.8	104.0 *	1 JAN 2012 493	3.	1.6	101.9
1 JAN 1225 26	2.	1.0	101.2 *	1 JAN 1619 260	69.	3.8	103.9 *	1 JAN 2013 494	3.	1.6	101.9
1 JAN 1226 27	2.	1.0	101.2 *	1 JAN 1620 261	65.	3.7	103.9 *	1 JAN 2014 495	3.	1.6	101.9
1 JAN 1227 28	2.	1.0	101.2 *	1 JAN 1621 262	61.	3.7	103.9 *	1 JAN 2015 496	3.	1.6	101.9
1 JAN 1228 29	2.	1.0	101.2 *	1 JAN 1622 263	57.	3.6	103.9 *	1 JAN 2016 497	3.	1.6	101.9
1 JAN 1229 30	2.	1.0	101.2 *	1 JAN 1623 264	54.	3.6	103.8 *	1 JAN 2017 498	3.	1.6	101.9
1 JAN 1230 31	2.	1.0	101.2 *	1 JAN 1624 265	50.	3.5	103.8 *	1 JAN 2018 499	3.	1.6	101.9
1 JAN 1231 32	2.	1.0	101.2 *	1 JAN 1625 266	47.	3.5	103.8 *	1 JAN 2019 500	3.	1.6	101.9
1 JAN 1232 33	2.	1.0	101.2 *	1 JAN 1626 267	44.	3.4	103.8 *	1 JAN 2020 501	3.	1.6	101.9
1 JAN 1233 34	2.	1.0	101.2 *	1 JAN 1627 268	42.	3.4	103.7 *	1 JAN 2021 502	3.	1.6	101.9
1 JAN 1234 35	2.	1.0	101.2 *	1 JAN 1628 269	39.	3.4	103.7 *	1 JAN 2022 503	3.	1.6	101.9
1 JAN 1235 36	2.	1.1	101.2 *	1 JAN 1629 270	37.	3.3	103.7 *	1 JAN 2023 504	3.	1.6	101.9
1 JAN 1236 37	2.	1.1	101.2 *	1 JAN 1630 271	35.	3.3	103.7 *	1 JAN 2024 505	3.	1.6	101.9
1 JAN 1237 38	2.	1.1	101.2 *	1 JAN 1631 272	33.	3.3	103.7 *	1 JAN 2025 506	3.	1.6	101.9
1 JAN 1238 39	2.	1.1	101.2 *	1 JAN 1632 273	32.	3.3	103.7 *	1 JAN 2026 507	3.	1.6	101.8
1 JAN 1239 40	2.	1.1	101.3 *	1 JAN 1633 274	31.	3.2	103.6 *	1 JAN 2027 508	3.	1.6	101.8
1 JAN 1240 41	2.	1.1	101.3 *	1 JAN 1634 275	30.	3.2	103.6 *	1 JAN 2028 509	3.	1.6	101.8
1 JAN 1241 42	2.	1.1	101.3 *	1 JAN 1635 276	30.	3.2	103.6 *	1 JAN 2029 510	3.	1.6	101.8
1 JAN 1242 43	2.	1.1	101.3 *	1 JAN 1636 277	29.	3.2	103.6 *	1 JAN 2030 511	3.	1.6	101.8
1 JAN 1243 44	2.	1.1	101.3 *	1 JAN 1637 278	28.	3.1	103.5 *	1 JAN 2031 512	3.	1.6	101.8
1 JAN 1244 45	2.	1.1	101.3 *	1 JAN 1638 279	27.	3.1	103.5 *	1 JAN 2032 513	3.	1.6	101.8
1 JAN 1245 46	2.	1.1	101.3 *	1 JAN 1639 280	27.	3.1	103.5 *	1 JAN 2033 514	3.	1.5	101.8
1 JAN 1246 47	2.	1.1	101.3 *	1 JAN 1640 281	26.	3.1	103.5 *	1 JAN 2034 515	3.	1.5	101.8
1 JAN 1247 48	2.	1.1	101.3 *	1 JAN 1641 282	25.	3.1	103.5 *	1 JAN 2035 516	3.	1.5	101.8
1 JAN 1248 49	2.	1.1	101.3 *	1 JAN 1642 283	25.	3.0	103.4 *	1 JAN 2036 517	3.	1.5	101.8
1 JAN 1249 50	2.	1.1	101.3 *	1 JAN 1643 284	24.	3.0	103.4 *	1 JAN 2037 518	3.	1.5	101.8
1 JAN 1250 51	2.	1.1	101.3 *	1 JAN 1644 285	23.	3.0	103.4 *	1 JAN 2038 519	3.	1.5	101.8
1 JAN 1251 52	2.	1.1	101.3 *	1 JAN 1645 286	23.	3.0	103.4 *	1 JAN 2039 520	3.	1.5	101.8
1 JAN 1252 53	2.	1.1	101.3 *	1 JAN 1646 287	22.	3.0	103.4 *	1 JAN 2040 521	3.	1.5	101.8
1 JAN 1253 54	2.	1.1	101.3 *	1 JAN 1647 288	22.	3.0	103.3 *	1 JAN 2041 522	3.	1.5	101.8
1 JAN 1254 55	2.	1.1	101.3 *	1 JAN 1648 289	21.	2.9	103.3 *	1 JAN 2042 523	3.	1.5	101.8
1 JAN 1255 56	2.	1.1	101.3 *	1 JAN 1649 290	21.	2.9	103.3 *	1 JAN 2043 524	3.	1.5	101.8
1 JAN 1256 57	2.	1.2	101.4 *	1 JAN 1650 291	20.	2.9	103.3 *	1 JAN 2044 525	3.	1.5	101.8
1 JAN 1257 58	2.	1.2	101.4 *	1 JAN 1651 292	20.	2.9	103.3 *	1 JAN 2045 526	3.	1.5	101.8
1 JAN 1258 59	2.	1.2	101.4 *	1 JAN 1652 293	19.	2.9	103.3 *	1 JAN 2046 527	3.	1.5	101.7
1 JAN 1259 60	2.	1.2	101.4 *	1 JAN 1653 294	19.	2.9	103.3 *	1 JAN 2047 528	3.	1.5	101.7
1 JAN 1300 61	2.	1.2	101.4 *	1 JAN 1654 295	18.	2.9	103.2 *	1 JAN 2048 529	3.	1.5	101.7
1 JAN 1301 62	2.	1.2	101.4 *	1 JAN 1655 296	18.	2.8	103.2 *	1 JAN 2049 530	3.	1.5	101.7
1 JAN 1302 63	2.	1.2	101.4 *	1 JAN 1656 297	17.	2.8	103.2 *	1 JAN 2050 531	3.	1.5	101.7
1 JAN 1303 64	2.	1.2	101.4 *	1 JAN 1657 298	17.	2.8	103.2 *	1 JAN 2051 532	3.	1.5	101.7
1 JAN 1304 65	2.	1.2	101.4 *	1 JAN 1658 299	17.	2.8	103.2 *	1 JAN 2052 533	3.	1.5	101.7
1 JAN 1305 66	2.	1.2	101.4 *	1 JAN 1659 300	16.	2.8	103.2 *	1 JAN 2053 534	3.	1.5	101.7
1 JAN 1306 67	2.	1.2	101.4 *	1 JAN 1700 301	16.	2.8	103.2 *	1 JAN 2054 535	3.	1.5	101.7
1 JAN 1307 68	2.	1.2	101.4 *	1 JAN 1701 302	16.	2.8	103.2 *	1 JAN 2055 536	3.	1.5	101.7
1 JAN 1308 69	2.	1.2	101.4 *	1 JAN 1702 303	15.	2.8	103.2 *	1 JAN 2056 537	3.	1.5	101.7
1 JAN 1309 70	2.	1.2	101.4 *	1 JAN 1703 304	15.	2.8	103.1 *	1 JAN 2057 538	3.	1.4	101.7
1 JAN 1310 71	2.	1.2	101.4 *	1 JAN 1704 305	15.	2.8	103.1 *	1 JAN 2058 539	3.	1.4	101.7

1 JAN 1311 72	3.	1.2	101.4 *	1 JAN 1705 306	14.	2.7	103.1 *	1 JAN 2059 540	3.	1.4	101.7
1 JAN 1312 73	3.	1.2	101.4 *	1 JAN 1706 307	14.	2.7	103.1 *	1 JAN 2100 541	3.	1.4	101.7
1 JAN 1313 74	3.	1.2	101.5 *	1 JAN 1707 308	14.	2.7	103.1 *	1 JAN 2101 542	3.	1.4	101.7
1 JAN 1314 75	3.	1.2	101.5 *	1 JAN 1708 309	13.	2.7	103.1 *	1 JAN 2102 543	3.	1.4	101.7
1 JAN 1315 76	3.	1.3	101.5 *	1 JAN 1709 310	13.	2.7	103.1 *	1 JAN 2103 544	3.	1.4	101.7
1 JAN 1316 77	3.	1.3	101.5 *	1 JAN 1710 311	13.	2.7	103.1 *	1 JAN 2104 545	3.	1.4	101.7
1 JAN 1317 78	3.	1.3	101.5 *	1 JAN 1711 312	13.	2.7	103.1 *	1 JAN 2105 546	3.	1.4	101.7
1 JAN 1318 79	3.	1.3	101.5 *	1 JAN 1712 313	12.	2.7	103.1 *	1 JAN 2106 547	3.	1.4	101.7
1 JAN 1319 80	3.	1.3	101.5 *	1 JAN 1713 314	12.	2.7	103.1 *	1 JAN 2107 548	3.	1.4	101.6
1 JAN 1320 81	3.	1.3	101.5 *	1 JAN 1714 315	12.	2.7	103.1 *	1 JAN 2108 549	3.	1.4	101.6
1 JAN 1321 82	3.	1.3	101.5 *	1 JAN 1715 316	12.	2.7	103.1 *	1 JAN 2109 550	3.	1.4	101.6
1 JAN 1322 83	3.	1.3	101.5 *	1 JAN 1716 317	12.	2.7	103.0 *	1 JAN 2110 551	3.	1.4	101.6
1 JAN 1323 84	3.	1.3	101.5 *	1 JAN 1717 318	11.	2.7	103.0 *	1 JAN 2111 552	3.	1.4	101.6
1 JAN 1324 85	3.	1.3	101.5 *	1 JAN 1718 319	11.	2.7	103.0 *	1 JAN 2112 553	3.	1.4	101.6
1 JAN 1325 86	3.	1.3	101.5 *	1 JAN 1719 320	11.	2.6	103.0 *	1 JAN 2113 554	3.	1.4	101.6
1 JAN 1326 87	3.	1.3	101.5 *	1 JAN 1720 321	11.	2.6	103.0 *	1 JAN 2114 555	3.	1.4	101.6
1 JAN 1327 88	3.	1.3	101.5 *	1 JAN 1721 322	11.	2.6	103.0 *	1 JAN 2115 556	3.	1.4	101.6
1 JAN 1328 89	3.	1.3	101.5 *	1 JAN 1722 323	10.	2.6	103.0 *	1 JAN 2116 557	3.	1.4	101.6
1 JAN 1329 90	3.	1.3	101.6 *	1 JAN 1723 324	10.	2.6	103.0 *	1 JAN 2117 558	3.	1.4	101.6
1 JAN 1330 91	3.	1.3	101.6 *	1 JAN 1724 325	10.	2.6	103.0 *	1 JAN 2118 559	3.	1.4	101.6
1 JAN 1331 92	3.	1.3	101.6 *	1 JAN 1725 326	10.	2.6	103.0 *	1 JAN 2119 560	3.	1.4	101.6
1 JAN 1332 93	3.	1.3	101.6 *	1 JAN 1726 327	10.	2.6	103.0 *	1 JAN 2120 561	3.	1.4	101.6
1 JAN 1333 94	3.	1.4	101.6 *	1 JAN 1727 328	10.	2.6	103.0 *	1 JAN 2121 562	3.	1.4	101.6
1 JAN 1334 95	3.	1.4	101.6 *	1 JAN 1728 329	10.	2.6	103.0 *	1 JAN 2122 563	3.	1.3	101.6
1 JAN 1335 96	3.	1.4	101.6 *	1 JAN 1729 330	10.	2.6	103.0 *	1 JAN 2123 564	3.	1.3	101.6
1 JAN 1336 97	3.	1.4	101.6 *	1 JAN 1730 331	10.	2.6	103.0 *	1 JAN 2124 565	3.	1.3	101.6
1 JAN 1337 98	3.	1.4	101.6 *	1 JAN 1731 332	10.	2.6	103.0 *	1 JAN 2125 566	3.	1.3	101.6
1 JAN 1338 99	3.	1.4	101.6 *	1 JAN 1732 333	10.	2.6	103.0 *	1 JAN 2126 567	3.	1.3	101.6
1 JAN 1339 100	3.	1.4	101.6 *	1 JAN 1733 334	10.	2.6	103.0 *	1 JAN 2127 568	3.	1.3	101.6
1 JAN 1340 101	3.	1.4	101.6 *	1 JAN 1734 335	10.	2.6	103.0 *	1 JAN 2128 569	3.	1.3	101.6
1 JAN 1341 102	3.	1.4	101.6 *	1 JAN 1735 336	10.	2.6	102.9 *	1 JAN 2129 570	3.	1.3	101.5
1 JAN 1342 103	3.	1.4	101.6 *	1 JAN 1736 337	9.	2.6	102.9 *	1 JAN 2130 571	3.	1.3	101.5
1 JAN 1343 104	3.	1.4	101.6 *	1 JAN 1737 338	9.	2.6	102.9 *	1 JAN 2131 572	3.	1.3	101.5
1 JAN 1344 105	3.	1.4	101.7 *	1 JAN 1738 339	9.	2.6	102.9 *	1 JAN 2132 573	3.	1.3	101.5
1 JAN 1345 106	3.	1.4	101.7 *	1 JAN 1739 340	9.	2.6	102.9 *	1 JAN 2133 574	3.	1.3	101.5
1 JAN 1346 107	3.	1.4	101.7 *	1 JAN 1740 341	9.	2.5	102.9 *	1 JAN 2134 575	3.	1.3	101.5
1 JAN 1347 108	3.	1.4	101.7 *	1 JAN 1741 342	9.	2.5	102.9 *	1 JAN 2135 576	3.	1.3	101.5
1 JAN 1348 109	3.	1.4	101.7 *	1 JAN 1742 343	9.	2.5	102.9 *	1 JAN 2136 577	3.	1.3	101.5
1 JAN 1349 110	3.	1.4	101.7 *	1 JAN 1743 344	9.	2.5	102.9 *	1 JAN 2137 578	3.	1.3	101.5
1 JAN 1350 111	3.	1.5	101.7 *	1 JAN 1744 345	9.	2.5	102.9 *	1 JAN 2138 579	3.	1.3	101.5
1 JAN 1351 112	3.	1.5	101.7 *	1 JAN 1745 346	9.	2.5	102.9 *	1 JAN 2139 580	3.	1.3	101.5
1 JAN 1352 113	3.	1.5	101.7 *	1 JAN 1746 347	9.	2.5	102.9 *	1 JAN 2140 581	3.	1.3	101.5
1 JAN 1353 114	3.	1.5	101.7 *	1 JAN 1747 348	9.	2.5	102.9 *	1 JAN 2141 582	3.	1.3	101.5
1 JAN 1354 115	3.	1.5	101.7 *	1 JAN 1748 349	9.	2.5	102.9 *	1 JAN 2142 583	3.	1.3	101.5
1 JAN 1355 116	3.	1.5	101.7 *	1 JAN 1749 350	9.	2.5	102.9 *	1 JAN 2143 584	3.	1.3	101.5
1 JAN 1356 117	3.	1.5	101.7 *	1 JAN 1750 351	9.	2.5	102.9 *	1 JAN 2144 585	3.	1.3	101.5
1 JAN 1357 118	3.	1.5	101.8 *	1 JAN 1751 352	9.	2.5	102.9 *	1 JAN 2145 586	3.	1.3	101.5
1 JAN 1358 119	3.	1.5	101.8 *	1 JAN 1752 353	9.	2.5	102.9 *	1 JAN 2146 587	3.	1.3	101.5
1 JAN 1359 120	3.	1.5	101.8 *	1 JAN 1753 354	9.	2.5	102.9 *	1 JAN 2147 588	3.	1.3	101.5
1 JAN 1400 121	3.	1.5	101.8 *	1 JAN 1754 355	9.	2.5	102.9 *	1 JAN 2148 589	3.	1.3	101.5
1 JAN 1401 122	3.	1.5	101.8 *	1 JAN 1755 356	9.	2.5	102.9 *	1 JAN 2149 590	3.	1.3	101.5
1 JAN 1402 123	3.	1.5	101.8 *	1 JAN 1756 357	9.	2.5	102.8 *	1 JAN 2150 591	3.	1.2	101.5
1 JAN 1403 124	3.	1.5	101.8 *	1 JAN 1757 358	9.	2.5	102.8 *	1 JAN 2151 592	3.	1.2	101.5
1 JAN 1404 125	3.	1.5	101.8 *	1 JAN 1758 359	8.	2.5	102.8 *	1 JAN 2152 593	3.	1.2	101.5
1 JAN 1405 126	3.	1.5	101.8 *	1 JAN 1759 360	8.	2.5	102.8 *	1 JAN 2153 594	3.	1.2	101.4
1 JAN 1406 127	3.	1.6	101.8 *	1 JAN 1800 361	8.	2.5	102.8 *	1 JAN 2154 595	3.	1.2	101.4
1 JAN 1407 128	3.	1.6	101.8 *	1 JAN 1801 362	8.	2.5	102.8 *	1 JAN 2155 596	3.	1.2	101.4
1 JAN 1408 129	3.	1.6	101.8 *	1 JAN 1802 363	8.	2.4	102.8 *	1 JAN 2156 597	2.	1.2	101.4
1 JAN 1409 130	3.	1.6	101.8 *	1 JAN 1803 364	8.	2.4	102.8 *	1 JAN 2157 598	2.	1.2	101.4
1 JAN 1410 131	3.	1.6	101.9 *	1 JAN 1804 365	8.	2.4	102.8 *	1 JAN 2158 599	2.	1.2	101.4

1 JAN 1411 132	3.	1.6	101.9 *	1 JAN 1805 366	8.	2.4	102.8 *	1 JAN 2159 600	2.	1.2	101.4
1 JAN 1412 133	3.	1.6	101.9 *	1 JAN 1806 367	8.	2.4	102.8 *	1 JAN 2200 601	2.	1.2	101.4
1 JAN 1413 134	3.	1.6	101.9 *	1 JAN 1807 368	8.	2.4	102.8 *	1 JAN 2201 602	2.	1.2	101.4
1 JAN 1414 135	3.	1.6	101.9 *	1 JAN 1808 369	8.	2.4	102.8 *	1 JAN 2202 603	2.	1.2	101.4
1 JAN 1415 136	3.	1.6	101.9 *	1 JAN 1809 370	8.	2.4	102.8 *	1 JAN 2203 604	2.	1.2	101.4
1 JAN 1416 137	3.	1.6	101.9 *	1 JAN 1810 371	8.	2.4	102.8 *	1 JAN 2204 605	2.	1.2	101.4
1 JAN 1417 138	3.	1.6	101.9 *	1 JAN 1811 372	8.	2.4	102.7 *	1 JAN 2205 606	2.	1.2	101.4
1 JAN 1418 139	3.	1.6	101.9 *	1 JAN 1812 373	7.	2.4	102.7 *	1 JAN 2206 607	2.	1.2	101.4
1 JAN 1419 140	3.	1.6	101.9 *	1 JAN 1813 374	7.	2.4	102.7 *	1 JAN 2207 608	2.	1.2	101.4
1 JAN 1420 141	3.	1.7	101.9 *	1 JAN 1814 375	7.	2.3	102.7 *	1 JAN 2208 609	2.	1.2	101.4
1 JAN 1421 142	3.	1.7	101.9 *	1 JAN 1815 376	7.	2.3	102.7 *	1 JAN 2209 610	2.	1.2	101.4
1 JAN 1422 143	3.	1.7	102.0 *	1 JAN 1816 377	7.	2.3	102.7 *	1 JAN 2210 611	2.	1.2	101.4
1 JAN 1423 144	3.	1.7	102.0 *	1 JAN 1817 378	7.	2.3	102.7 *	1 JAN 2211 612	2.	1.2	101.4
1 JAN 1424 145	3.	1.7	102.0 *	1 JAN 1818 379	7.	2.3	102.7 *	1 JAN 2212 613	2.	1.2	101.4
1 JAN 1425 146	3.	1.7	102.0 *	1 JAN 1819 380	7.	2.3	102.7 *	1 JAN 2213 614	2.	1.2	101.4
1 JAN 1426 147	3.	1.7	102.0 *	1 JAN 1820 381	7.	2.3	102.7 *	1 JAN 2214 615	2.	1.2	101.4
1 JAN 1427 148	3.	1.7	102.0 *	1 JAN 1821 382	7.	2.3	102.6 *	1 JAN 2215 616	2.	1.2	101.4
1 JAN 1428 149	3.	1.7	102.0 *	1 JAN 1822 383	6.	2.3	102.6 *	1 JAN 2216 617	2.	1.2	101.4
1 JAN 1429 150	4.	1.7	102.0 *	1 JAN 1823 384	6.	2.3	102.6 *	1 JAN 2217 618	2.	1.2	101.4
1 JAN 1430 151	4.	1.7	102.0 *	1 JAN 1824 385	6.	2.3	102.6 *	1 JAN 2218 619	2.	1.2	101.3
1 JAN 1431 152	4.	1.7	102.0 *	1 JAN 1825 386	6.	2.2	102.6 *	1 JAN 2219 620	2.	1.1	101.3
1 JAN 1432 153	4.	1.7	102.0 *	1 JAN 1826 387	6.	2.2	102.6 *	1 JAN 2220 621	2.	1.1	101.3
1 JAN 1433 154	4.	1.8	102.1 *	1 JAN 1827 388	6.	2.2	102.6 *	1 JAN 2221 622	2.	1.1	101.3
1 JAN 1434 155	4.	1.8	102.1 *	1 JAN 1828 389	6.	2.2	102.6 *	1 JAN 2222 623	2.	1.1	101.3
1 JAN 1435 156	4.	1.8	102.1 *	1 JAN 1829 390	6.	2.2	102.6 *	1 JAN 2223 624	2.	1.1	101.3
1 JAN 1436 157	4.	1.8	102.1 *	1 JAN 1830 391	6.	2.2	102.6 *	1 JAN 2224 625	2.	1.1	101.3
1 JAN 1437 158	4.	1.8	102.1 *	1 JAN 1831 392	6.	2.2	102.6 *	1 JAN 2225 626	2.	1.1	101.3
1 JAN 1438 159	4.	1.8	102.1 *	1 JAN 1832 393	6.	2.2	102.5 *	1 JAN 2226 627	2.	1.1	101.3
1 JAN 1439 160	4.	1.8	102.1 *	1 JAN 1833 394	6.	2.2	102.5 *	1 JAN 2227 628	2.	1.1	101.3
1 JAN 1440 161	4.	1.8	102.1 *	1 JAN 1834 395	5.	2.2	102.5 *	1 JAN 2228 629	2.	1.1	101.3
1 JAN 1441 162	4.	1.8	102.1 *	1 JAN 1835 396	5.	2.2	102.5 *	1 JAN 2229 630	2.	1.1	101.3
1 JAN 1442 163	4.	1.8	102.1 *	1 JAN 1836 397	5.	2.2	102.5 *	1 JAN 2230 631	2.	1.1	101.3
1 JAN 1443 164	4.	1.8	102.2 *	1 JAN 1837 398	5.	2.2	102.5 *	1 JAN 2231 632	2.	1.1	101.3



1 JAN 1511 192	5.	2.1	102.5 *	1 JAN 1905 426	4.	2.0	102.3 *	1 JAN 2259 660	2.	1.0	101.2
1 JAN 1512 193	5.	2.1	102.5 *	1 JAN 1906 427	4.	2.0	102.3 *	1 JAN 2300 661	2.	1.0	101.2
1 JAN 1513 194	5.	2.2	102.5 *	1 JAN 1907 428	4.	2.0	102.3 *	1 JAN 2301 662	2.	1.0	101.2
1 JAN 1514 195	5.	2.2	102.5 *	1 JAN 1908 429	4.	2.0	102.3 *	1 JAN 2302 663	2.	1.0	101.2
1 JAN 1515 196	6.	2.2	102.5 *	1 JAN 1909 430	4.	2.0	102.3 *	1 JAN 2303 664	2.	1.0	101.2
1 JAN 1516 197	6.	2.2	102.6 *	1 JAN 1910 431	4.	2.0	102.3 *	1 JAN 2304 665	2.	1.0	101.2
1 JAN 1517 198	6.	2.2	102.6 *	1 JAN 1911 432	4.	1.9	102.3 *	1 JAN 2305 666	2.	1.0	101.2
1 JAN 1518 199	6.	2.2	102.6 *	1 JAN 1912 433	4.	1.9	102.3 *	1 JAN 2306 667	2.	1.0	101.2
1 JAN 1519 200	6.	2.2	102.6 *	1 JAN 1913 434	4.	1.9	102.3 *	1 JAN 2307 668	2.	1.0	101.2
1 JAN 1520 201	6.	2.2	102.6 *	1 JAN 1914 435	4.	1.9	102.3 *	1 JAN 2308 669	2.	1.0	101.2
1 JAN 1521 202	6.	2.3	102.6 *	1 JAN 1915 436	4.	1.9	102.3 *	1 JAN 2309 670	2.	1.0	101.2
1 JAN 1522 203	6.	2.3	102.6 *	1 JAN 1916 437	4.	1.9	102.2 *	1 JAN 2310 671	2.	1.0	101.2
1 JAN 1523 204	7.	2.3	102.6 *	1 JAN 1917 438	4.	1.9	102.2 *	1 JAN 2311 672	2.	1.0	101.2
1 JAN 1524 205	7.	2.3	102.7 *	1 JAN 1918 439	4.	1.9	102.2 *	1 JAN 2312 673	2.	1.0	101.2
1 JAN 1525 206	7.	2.3	102.7 *	1 JAN 1919 440	4.	1.9	102.2 *	1 JAN 2313 674	2.	1.0	101.2
1 JAN 1526 207	7.	2.3	102.7 *	1 JAN 1920 441	4.	1.9	102.2 *	1 JAN 2314 675	2.	1.0	101.2
1 JAN 1527 208	7.	2.3	102.7 *	1 JAN 1921 442	4.	1.9	102.2 *	1 JAN 2315 676	2.	1.0	101.1
1 JAN 1528 209	7.	2.3	102.7 *	1 JAN 1922 443	4.	1.9	102.2 *	1 JAN 2316 677	2.	1.0	101.1
1 JAN 1529 210	7.	2.4	102.7 *	1 JAN 1923 444	4.	1.9	102.2 *	1 JAN 2317 678	2.	1.0	101.1
1 JAN 1530 211	8.	2.4	102.7 *	1 JAN 1924 445	4.	1.9	102.2 *	1 JAN 2318 679	2.	1.0	101.1
1 JAN 1531 212	8.	2.4	102.8 *	1 JAN 1925 446	4.	1.9	102.2 *	1 JAN 2319 680	2.	1.0	101.1
1 JAN 1532 213	8.	2.4	102.8 *	1 JAN 1926 447	4.	1.9	102.2 *	1 JAN 2320 681	2.	1.0	101.1
1 JAN 1533 214	8.	2.4	102.8 *	1 JAN 1927 448	4.	1.9	102.2 *	1 JAN 2321 682	2.	1.0	101.1
1 JAN 1534 215	8.	2.4	102.8 *	1 JAN 1928 449	4.	1.9	102.2 *	1 JAN 2322 683	2.	1.0	101.1
1 JAN 1535 216	8.	2.5	102.8 *	1 JAN 1929 450	4.	1.9	102.2 *	1 JAN 2323 684	2.	1.0	101.1
1 JAN 1536 217	9.	2.5	102.8 *	1 JAN 1930 451	4.	1.8	102.2 *	1 JAN 2324 685	2.	1.0	101.1
1 JAN 1537 218	9.	2.5	102.9 *	1 JAN 1931 452	4.	1.8	102.2 *	1 JAN 2325 686	2.	1.0	101.1
1 JAN 1538 219	9.	2.5	102.9 *	1 JAN 1932 453	4.	1.8	102.2 *	1 JAN 2326 687	2.	1.0	101.1
1 JAN 1539 220	9.	2.5	102.9 *	1 JAN 1933 454	4.	1.8	102.1 *	1 JAN 2327 688	2.	.9	101.1
1 JAN 1540 221	9.	2.6	102.9 *	1 JAN 1934 455	4.	1.8	102.1 *	1 JAN 2328 689	2.	.9	101.1
1 JAN 1541 222	10.	2.6	102.9 *	1 JAN 1935 456	4.	1.8	102.1 *	1 JAN 2329 690	2.	.9	101.1
1 JAN 1542 223	10.	2.6	103.0 *	1 JAN 1936 457	4.	1.8	102.1 *	1 JAN 2330 691	2.	.9	101.1
1 JAN 1543 224	10.	2.6	103.0 *	1 JAN 1937 458	4.	1.8	102.1 *	1 JAN 2331 692	2.	.9	101.1
1 JAN 1544 225	10.	2.6	103.0 *	1 JAN 1938 459	4.	1.8	102.1 *	1 JAN 2332 693	2.	.9	101.1
1 JAN 1545 226	11.	2.6	103.0 *	1 JAN 1939 460	4.	1.8	102.1 *	1 JAN 2333 694	2.	.9	101.1
1 JAN 1546 227	11.	2.6	103.0 *	1 JAN 1940 461	4.	1.8	102.1 *	1 JAN 2334 695	2.	.9	101.1
1 JAN 1547 228	12.	2.7	103.0 *	1 JAN 1941 462	4.	1.8	102.1 *	1 JAN 2335 696	2.	.9	101.1
1 JAN 1548 229	12.	2.7	103.1 *	1 JAN 1942 463	4.	1.8	102.1 *	1 JAN 2336 697	2.	.9	101.1
1 JAN 1549 230	12.	2.7	103.1 *	1 JAN 1943 464	4.	1.8	102.1 *	1 JAN 2337 698	2.	.9	101.1
1 JAN 1550 231	13.	2.7	103.1 *	1 JAN 1944 465	4.	1.8	102.1 *	1 JAN 2338 699	2.	.9	101.1
1 JAN 1551 232	13.	2.7	103.1 *	1 JAN 1945 466	4.	1.8	102.1 *	1 JAN 2339 700	2.	.9	101.1
1 JAN 1552 233	13.	2.7	103.1 *	1 JAN 1946 467	4.	1.8	102.1 *				
1 JAN 1553 234	14.	2.7	103.1 *	1 JAN 1947 468	4.	1.8	102.1 *				

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PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	11.65-HR
79.	4.22	(CFS) 12.	7.	7.	7.
		(INCHES) 1.169	1.397	1.397	1.397
		(AC-FT) 6.	7.	7.	7.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	6-HR	24-HR	72-HR	11.65-HR
4.	4.22	2.	2.	2.	2.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	11.65-HR
104.00	4.22	102.70	102.09	102.09	102.09

CUMULATIVE AREA = .10 SQ MI

## STATION DETAIN

(I) INFLOW, (O) OUTFLOW

0.	20.	40.	60.	80.	100.	120.	140.	0.	0.	0.	0.	0.
								(S) STORAGE				
0.	0.	0.	0.	0.	0.	0.	1.	2.	3.	4.	0.	0.

DAHRMN PER

11200	1.I	-----S-----										
11201	2.I	.	.	.	.	.	.	S.	.	.	.	.
11202	3.I	.	.	.	.	.	.	S.	.	.	.	.
11203	4.I	.	.	.	.	.	.	S.	.	.	.	.
11204	5.OI	.	.	.	.	.	.	S.	.	.	.	.
11205	6.OI	.	.	.	.	.	.	S.	.	.	.	.
11206	7.OI	.	.	.	.	.	.	S.	.	.	.	.
11207	8.OI	.	.	.	.	.	.	S.	.	.	.	.
11208	9.OI	.	.	.	.	.	.	S.	.	.	.	.
11209	10.O I	.	.	.	.	.	.	S.	.	.	.	.
11210	11.O.I.	.....S.....										
11211	12.O I	.	.	.	.	.	.	S.	.	.	.	.
11212	13.O I	.	.	.	.	.	.	S.	.	.	.	.
11213	14.O I	.	.	.	.	.	.	S.	.	.	.	.
11214	15.O I	.	.	.	.	.	.	S	.	.	.	.
11215	16.O I	.	.	.	.	.	.	S	.	.	.	.
11216	17.O I	.	.	.	.	.	.	S	.	.	.	.
11217	18.O I	.	.	.	.	.	.	S	.	.	.	.
11218	19.O I	.	.	.	.	.	.	S	.	.	.	.
11219	20.O I	.	.	.	.	.	.	S	.	.	.	.
11220	21.O.I.	.....S.....										
11221	22.O I	.	.	.	.	.	.	S	.	.	.	.
11222	23.O I	.	.	.	.	.	.	S	.	.	.	.
11223	24.O I	.	.	.	.	.	.	S	.	.	.	.
11224	25.O I	.	.	.	.	.	.	S	.	.	.	.
11225	26.O I	.	.	.	.	.	.	S	.	.	.	.
11226	27.O I	.	.	.	.	.	.	S	.	.	.	.
11227	28.O I	.	.	.	.	.	.	S	.	.	.	.
11228	29.O I	.	.	.	.	.	.	S	.	.	.	.
11229	30.O I	.	.	.	.	.	.	S	.	.	.	.
11230	31.O.I.	.....S.....										
11231	32.O I	.	.	.	.	.	.	S	.	.	.	.
11232	33.O I	.	.	.	.	.	.	S	.	.	.	.
11233	34.O I	.	.	.	.	.	.	S	.	.	.	.
11234	35.O I	.	.	.	.	.	.	S	.	.	.	.
11235	36.O I	.	.	.	.	.	.	.S	.	.	.	.
11236	37.O I	.	.	.	.	.	.	.S	.	.	.	.
11237	38.O I	.	.	.	.	.	.	.S	.	.	.	.
11238	39.O I	.	.	.	.	.	.	.S	.	.	.	.
11239	40.O I	.	.	.	.	.	.	.S	.	.	.	.
11240	41.O.I.	.....S.....										
11241	42.O I	.	.	.	.	.	.	.S	.	.	.	.
11242	43.O I	.	.	.	.	.	.	.S	.	.	.	.
11243	44.O I	.	.	.	.	.	.	.S	.	.	.	.
11244	45.O I	.	.	.	.	.	.	.S	.	.	.	.
11245	46.O I	.	.	.	.	.	.	.S	.	.	.	.
11246	47.O I	.	.	.	.	.	.	.S	.	.	.	.
11247	48.O I	.	.	.	.	.	.	.S	.	.	.	.
11248	49.O I	.	.	.	.	.	.	.S	.	.	.	.
11249	50.O I	.	.	.	.	.	.	.S	.	.	.	.
11250	51.O.I.	.....S.....										
11251	52.O I	.	.	.	.	.	.	.S	.	.	.	.
11252	53.O I	.	.	.	.	.	.	.S	.	.	.	.

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11353	114.	O	I	.	.	.	.	.	.	S	.	.	.	.
11354	115.	O	I	.	.	.	.	.	.	S	.	.	.	.
11355	116.	O	I	.	.	.	.	.	.	S	.	.	.	.
11356	117.	O	I	.	.	.	.	.	.	S	.	.	.	.
11357	118.	O	I	.	.	.	.	.	.	S	.	.	.	.
11358	119.	O	I	.	.	.	.	.	.	S	.	.	.	.
11359	120.	O	I	.	.	.	.	.	.	S	.	.	.	.
11400	121.	O	I	.	.	.	.	.	.	S	.	.	.	.
11401	122.	O	I	.	.	.	.	.	.	S	.	.	.	.
11402	123.	O	I	.	.	.	.	.	.	S	.	.	.	.
11403	124.	O	I	.	.	.	.	.	.	S	.	.	.	.
11404	125.	O	I	.	.	.	.	.	.	S	.	.	.	.
11405	126.	O	I	.	.	.	.	.	.	S	.	.	.	.
11406	127.	O	I	.	.	.	.	.	.	S	.	.	.	.
11407	128.	O	I	.	.	.	.	.	.	S	.	.	.	.
11408	129.	O	I	.	.	.	.	.	.	S	.	.	.	.
11409	130.	O	I	.	.	.	.	.	.	S	.	.	.	.
11410	131.	O	I	.	.	.	.	.	.	S	.	.	.	.
11411	132.	O	I	.	.	.	.	.	.	S	.	.	.	.
11412	133.	O	I	.	.	.	.	.	.	S	.	.	.	.
11413	134.	O	I	.	.	.	.	.	.	S	.	.	.	.
11414	135.	O	I	.	.	.	.	.	.	S	.	.	.	.
11415	136.	O	I	.	.	.	.	.	.	S	.	.	.	.
11416	137.	O	I	.	.	.	.	.	.	S	.	.	.	.
11417	138.	O	I	.	.	.	.	.	.	S	.	.	.	.
11418	139.	O	I	.	.	.	.	.	.	S	.	.	.	.
11419	140.	O	I	.	.	.	.	.	.	S	.	.	.	.
11420	141.	O	I	.	.	.	.	.	.	S	.	.	.	.
11421	142.	O	I	.	.	.	.	.	.	S	.	.	.	.
11422	143.	O	I	.	.	.	.	.	.	S	.	.	.	.
11423	144.	O	I	.	.	.	.	.	.	S	.	.	.	.
11424	145.	O	I	.	.	.	.	.	.	S	.	.	.	.
11425	146.	O	I	.	.	.	.	.	.	S	.	.	.	.
11426	147.	O	I	.	.	.	.	.	.	S	.	.	.	.
11427	148.	O	I	.	.	.	.	.	.	S	.	.	.	.
11428	149.	O	I	.	.	.	.	.	.	S	.	.	.	.
11429	150.	O	I	.	.	.	.	.	.	S	.	.	.	.
11430	151.	O	I	.	.	.	.	.	.	S	.	.	.	.
11431	152.	O	I	.	.	.	.	.	.	S	.	.	.	.
11432	153.	O	I	.	.	.	.	.	.	S	.	.	.	.
11433	154.	O	I	.	.	.	.	.	.	S	.	.	.	.
11434	155.	O	I	.	.	.	.	.	.	S	.	.	.	.
11435	156.	O	I	.	.	.	.	.	.	S	.	.	.	.
11436	157.	O	I	.	.	.	.	.	.	S	.	.	.	.
11437	158.	O	I	.	.	.	.	.	.	S	.	.	.	.
11438	159.	O	I	.	.	.	.	.	.	S	.	.	.	.
11439	160.	O	I	.	.	.	.	.	.	S	.	.	.	.
11440	161.	O	I	.	.	.	.	.	.	S	.	.	.	.
11441	162.	O	I	.	.	.	.	.	.	S	.	.	.	.
11442	163.	O	I	.	.	.	.	.	.	S	.	.	.	.
11443	164.	O	I	.	.	.	.	.	.	S	.	.	.	.
11444	165.	O	I	.	.	.	.	.	.	S	.	.	.	.
11445	166.	O	I	.	.	.	.	.	.	S	.	.	.	.
11446														

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11753	354.	IO	.	.	.	.	.	.	.	S	.	.	.
11754	355.	IO	.	.	.	.	.	.	.	S	.	.	.
11755	356.	IO	.	.	.	.	.	.	.	S	.	.	.
11756	357.	IO	.	.	.	.	.	.	.	S	.	.	.
11757	358.	IO	.	.	.	.	.	.	.	S	.	.	.
11758	359.	IO	.	.	.	.	.	.	.	S	.	.	.
11759	360.	IO	.	.	.	.	.	.	.	S	.	.	.
11800	361.	I O	.	.	.	.	.	.	.	S	.	.	.
11801	362.	I O	.	.	.	.	.	.	.	S	.	.	.
11802	363.	I O	.	.	.	.	.	.	.	S	.	.	.
11803	364.	I O	.	.	.	.	.	.	.	S	.	.	.
11804	365.	I O	.	.	.	.	.	.	.	S	.	.	.
11805	366.	I O	.	.	.	.	.	.	.	S	.	.	.
11806	367.	I O	.	.	.	.	.	.	.	S	.	.	.
11807	368.	I O	.	.	.	.	.	.	.	S	.	.	.
11808	369.	I O	.	.	.	.	.	.	.	S	.	.	.
11809	370.	I O	.	.	.	.	.	.	.	S	.	.	.
11810	371.	I O	.	.	.	.	.	.	.	S	.	.	.
11811	372I	O	.	.	.	.	.	.	.	S	.	.	.
11812	373I	O	.	.	.	.	.	.	.	S	.	.	.
11813	374I	O	.	.	.	.	.	.	.	S	.	.	.
11814	375I	O	.	.	.	.	.	.	.	S	.	.	.
11815	376I	O	.	.	.	.	.	.	.	S	.	.	.
11816	377I	O	.	.	.	.	.	.	.	S	.	.	.
11817	378I	O	.	.	.	.	.	.	.	S	.	.	.
11818	379I	O	.	.	.	.	.	.	.	S	.	.	.
11819	380I	O	.	.	.	.	.	.	.	S	.	.	.
11820	381I	O	.	.	.	.	.	.	.	S	.	.	.
11821	382I	O	.	.	.	.	.	.	.	S	.	.	.
11822	383I	O	.	.	.	.	.	.	.	S	.	.	.
11823	384I	O	.	.	.	.	.	.	.	S	.	.	.
11824	385I	O	.	.	.	.	.	.	.	S	.	.	.
11825	386I	O	.	.	.	.	.	.	.	S	.	.	.
11826	387I	O	.	.	.	.	.	.	.	S	.	.	.
11827	388I	O	.	.	.	.	.	.	.	S	.	.	.
11828	389I	O	.	.	.	.	.	.	.	S	.	.	.
11829	390I	O	.	.	.	.	.	.	.	S	.	.	.
11830	391I	O	.	.	.	.	.	.	.	S	.	.	.
11831	392I	O	.	.	.	.	.	.	.	S	.	.	.
11832	393I	O	.	.	.	.	.	.	.	S	.	.	.
11833	394I	O	.	.	.	.	.	.	.	S	.	.	.
11834	395I	O	.	.	.	.	.	.	.	S	.	.	.
11835	396I	O	.	.	.	.	.	.	.	S	.	.	.
11836	397I	O	.	.	.	.	.	.	.	S	.	.	.
11837	398I	O	.	.	.	.	.	.	.	S	.	.	.
11838	399I	O	.	.	.	.	.	.	.	S	.	.	.
11839	400I	O	.	.	.	.	.	.	.	S	.	.	.
11840	401I	O	.	.	.	.	.	.	.	S	.	.	.
11841	402I	O	.	.	.	.	.	.	.	S	.	.	.
11842	403I	O	.	.	.	.	.	.	.	S	.	.	.
11843	404I	O	.	.	.	.	.	.	.	S	.	.	.
11844	405I	O	.	.	.	.	.	.	.	S	.	.	.
11845	406I	O	.	.	.	.	.	.	.	S	.	.	.
11846	407I	O	.	.	.	.	.	.	.	S	.	.	.
11847	408I	O	.	.	.	.	.	.	.	S	.	.	.
11848	409												

[illegible]

[illegible]

12053	534IO	.	.	.	.	.	S	.	.	.
12054	535IO	.	.	.	.	.	S	.	.	.
12055	536IO	.	.	.	.	.	S	.	.	.
12056	537IO	.	.	.	.	.	S	.	.	.
12057	538IO	.	.	.	.	.	S	.	.	.
12058	539IO	.	.	.	.	.	S	.	.	.
12059	540IO	.	.	.	.	.	S	.	.	.
12100	541IO.	.	.	.	.	.	S	.	.	.
12101	542IO	.	.	.	.	.	S	.	.	.
12102	543IO	.	.	.	.	.	S	.	.	.
12103	544IO	.	.	.	.	.	S	.	.	.
12104	545IO	.	.	.	.	.	S	.	.	.
12105	546IO	.	.	.	.	.	S	.	.	.
12106	547IO	.	.	.	.	.	S	.	.	.
12107	548IO	.	.	.	.	.	S	.	.	.
12108	549IO	.	.	.	.	.	S	.	.	.
12109	550IO	.	.	.	.	.	S	.	.	.
12110	551IO.	.	.	.	.	.	S	.	.	.
12111	552IO	.	.	.	.	.	S	.	.	.
12112	553IO	.	.	.	.	.	S	.	.	.
12113	554IO	.	.	.	.	.	S	.	.	.
12114	555IO	.	.	.	.	.	S	.	.	.
12115	556IO	.	.	.	.	.	S	.	.	.
12116	557IO	.	.	.	.	.	S	.	.	.
12117	558IO	.	.	.	.	.	S	.	.	.
12118	559IO	.	.	.	.	.	S	.	.	.
12119	560IO	.	.	.	.	.	S	.	.	.
12120	561IO.	.	.	.	.	.	S	.	.	.
12121	562IO	.	.	.	.	.	S	.	.	.
12122	563IO	.	.	.	.	.	S	.	.	.
12123	564IO	.	.	.	.	.	S	.	.	.
12124	565IO	.	.	.	.	.	S	.	.	.
12125	566IO	.	.	.	.	.	S	.	.	.
12126	567IO	.	.	.	.	.	S	.	.	.
12127	568IO	.	.	.	.	.	S	.	.	.
12128	569IO	.	.	.	.	.	S	.	.	.
12129	570IO	.	.	.	.	.	S	.	.	.
12130	571IO.	.	.	.	.	.	S	.	.	.
12131	572IO	.	.	.	.	.	S	.	.	.
12132	573IO	.	.	.	.	.	S	.	.	.
12133	574IO	.	.	.	.	.	S	.	.	.
12134	575IO	.	.	.	.	.	S	.	.	.
12135	576IO	.	.	.	.	.	S	.	.	.
12136	577IO	.	.	.	.	.	S	.	.	.
12137	578IO	.	.	.	.	.	S	.	.	.
12138	579IO	.	.	.	.	.	S	.	.	.
12139	580IO	.	.	.	.	.	S	.	.	.
12140	581IO.	.	.	.	.	.	S	.	.	.
12141	582IO	.	.	.	.	.	S	.	.	.
12142	583IO	.	.	.	.	.	S	.	.	.
12143	584IO	.	.	.	.	.	S	.	.	.
12144	585IO	.	.	.	.	.	S	.	.	.
12145	586IO	.	.	.	.	.	S	.	.	.
12146	587IO	.	.	.	.	.	S	.	.	.
12147	588IO	.	.	.	.	.	S	.	.	.
12148	589IO	.	.	.	.	.	S	.	.	.
12149	590IO	.	.	.	.	.	S	.	.	.
12150	591IO.	.	.	.	.	.	S	.	.	.
12151	592IO	.	.	.	.	.	S	.	.	.
12152	593IO	.	.	.	.	.	S	.	.	.

[illegible]

12253	654IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12254	655IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12255	656IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12256	657IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12257	658IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12258	659IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12259	660IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12300	661IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12301	662IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12302	663IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12303	664IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12304	665IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12305	666IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12306	667IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12307	668IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12308	669IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12309	670IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12310	671IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12311	672IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12312	673IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12313	674IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12314	675IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12315	676IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12316	677IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12317	678IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12318	679IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12319	680IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12320	681IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12321	682IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12322	683IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12323	684IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12324	685IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12325	686IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12326	687IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12327	688IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12328	689IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12329	690IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12330	691IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12331	692IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12332	693IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12333	694IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12334	695IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12335	696IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12336	697IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12337	698IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12338	699IO	.	.	.	.	.	.	.	S	.	.	.	.	.
12339	700IO	.	.	.	.	.	.	.	S	.	.	.	.	.

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	3000	131.	4.12	14.	7.	7.	.10		
ROUTED TO	DETAIN	79.	4.22	12.	7.	7.	.10	104.00	4.22

\*\*\* NORMAL END OF HEC-1 \*\*\*

## **Drainage Basin 4000**



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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*      JUN 1998                      *
*      VERSION 4.1                   *
*
* RUN DATE 29JUL09 TIME 14:50:13 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
*      609 SECOND STREET
* DAVIS, CALIFORNIA 95616
*      (916) 756-1104
*
*****

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X      X XXXXXXXX XXXXX      X
X      X X      X      X      XX
X      X X      X      X      X
XXXXXXX XXXX      X      XXXXX X
X      X X      X      X      X
X      X X      X      X      X
X      X XXXXXXXX XXXXX      XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE..  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

\*\*\* FREE \*\*\*

\*DIAGRAM

```

1  ID  MEADOWOOD J-15956 01/13/09 FILE: MW4000D.HC1
2  ID  DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)
3  ID  R/O=.50, PRECIP=3.6IN, TC 6.66MIN
4  IT   1 01JAN90   1200   600
5  IO   3       1

6  KK   4003
7  KM  RUN DATE   7/16/2009
8  KM  RATIONAL METHOD HYDROGRAPH PROGRAM
9  KM  COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
10 KM  6HR RAINFALL IS  3.6  INCHES
11 KM  RATIONAL METHOD RUNOFF COEFFICIENT IS  0.62
12 KM  RATIONAL METHOD TIME OF CONCENTRATION IS  6  MIN.
13 KM  FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
14 KM  IT 2 01JAN90 1200 200
15 KO   0       0       0       0       21
16 BA  0.0108
17 IN   6 01JAN90   1157
18 QI   0       0.9     0.9     0.9     1       1       1       1       1       1.1
19 QI   1.1     1.1     1.1     1.2     1.2     1.2     1.2     1.3     1.3     1.4
20 QI   1.4     1.4     1.5     1.5     1.6     1.7     1.7     1.8     1.9     2
21 QI   2.1     2.3     2.4     2.7     2.8     3.2     3.5     4.3     4.9     7.1
22 QI  10.2    35.92    5.7     3.8     3       2.5     2.2     2       1.8     1.6
23 QI   1.5     1.4     1.3     1.3     1.2     1.1     1.1     1       1       1
24 QI   0.9     0       0       0       0       0       0       0       0       0
25 QI   0       0

26 KK  4002.1
27 KM  RUN DATE   7/16/2009
28 KM  RATIONAL METHOD HYDROGRAPH PROGRAM
29 KM  COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
30 KM  6HR RAINFALL IS  3.6  INCHES
31 KM  RATIONAL METHOD RUNOFF COEFFICIENT IS  0.3
32 KM  RATIONAL METHOD TIME OF CONCENTRATION IS  13  MIN.
33 KM  FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
34 KM  IT 2 01JAN90 1200 200
35 BA  0.005
36 IN  13 01JAN90   1147
37 QI   0       0       0.2     0.2     0.2     0.2     0.2     0.3     0.3     0.3
38 QI   0.3     0.3     0.4     0.4     0.4     0.5     0.6     0.7     1       0.9
39 QI   5.4     0.8     0.5     0.4     0.3     0.3     0.3     0.2     0.2     0
40 QI   0       0       0       0       0       0       0       0       0       0

41 KK  Combine
42 KM  Combine the two drainage areas entering the detention basin
43 HC   2

44 KK  DETAIN
45 KM  100-YEAR DETENTION
46 KO   0       0       0       0       21
47 RS   1  STOR   -1
48 SV   0  0.72   0.94   1.05   1.246
49 SQ   0  0.67   2.76   5.51   15.5

```

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
50	SE      100    102.4      103    103.32      104
51	KK      4006
52	KM    Undetained Area Trib to Node 4006
53	KM    RUN DATE    7/16/2009
54	KM    RATIONAL METHOD HYDROGRAPH PROGRAM
55	KM    COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
56	KM    6HR RAINFALL IS    3.6    INCHES
57	KM    RATIONAL METHOD RUNOFF COEFFICIENT IS    0.284
58	KM    RATIONAL METHOD TIME OF CONCENTRATION IS    16    MIN.
59	KM    FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
60	KM    IT 2 01JAN90 1200 200
61	BA    0.0017
62	IN      16 01JAN90      1152
63	QI      0      0.1      0.1      0.1      0.1      0.1      0.1      0.1      0.1
64	QI      0.1      0.1      0.2      0.2      0.3      0.4      1.38      0.2      0.1      0.1
65	QI      0.1      0.1      0.1      0.1      0      0      0      0      0      0
66	QI      0      0      0      0      0
67	KK Combine
68	KM    Combine detained outflow from DB4 and area trib to Node 4006
69	KO      0      0      0      0      21
70	HC      2
71	ZZ

# SCHEMATIC DIAGRAM OF STREAM NETWORK

## INPUT

LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
6	4003	
	.	
	.	
26	.	4002.1
	.	
	.	
41	Combine.....	
	V	
	V	
44	DETAIN	
	.	
	.	
51	.	4006
	.	
	.	
57	Combine.....	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 29JUL09 TIME 14:50:13
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
```

MEADOWOOD J-15956 01/13/09 FILE: MW4000D.HC1  
 DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)  
 R/0=.50, PRECIP=3.6IN, TC 6.66MIN

5 IO OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL  
 IPLOT 1 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA

NMIN 1 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1JAN90 STARTING DATE  
 ITIME 1200 STARTING TIME  
 NQ 600 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 1JAN90 ENDING DATE  
 NDTIME 2159 ENDING TIME  
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL .02 HOURS  
 TOTAL TIME BASE 9.98 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-Feet  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

\*\*\* \*\*

6 KK

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*****
*
* 4003
*
*****
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RUN DATE 7/16/2009  
 RATIONAL METHOD HYDROGRAPH PROGRAM  
 COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
 6HR RAINFALL IS 3.6 INCHES  
 RATIONAL METHOD RUNOFF COEFFICIENT IS 0.62  
 RATIONAL METHOD TIME OF CONCENTRATION IS 6 MIN.

FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
IT 2 01JAN90 1200 200

15 KO OUTPUT CONTROL VARIABLES  
IPRNT 3 PRINT CONTROL  
IPLOT 1 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 600 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .017 TIME INTERVAL IN HOURS

17 IN TIME DATA FOR INPUT TIME SERIES  
JXMIN 6 TIME INTERVAL IN MINUTES  
JXDATE 1JAN90 STARTING DATE  
JXTIME 1157 STARTING TIME

SUBBASIN RUNOFF DATA

16 BA SUBBASIN CHARACTERISTICS  
TAREA .01 SUBBASIN AREA

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HYDROGRAPH AT STATION 4003

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	9.98-HR
36.	4.05	(CFS)	3.	2.	2.	2.
		(INCHES)	2.210	2.211	2.211	2.211
		(AC-FT)	1.	1.	1.	1.

CUMULATIVE AREA = .01 SQ MI

\*\*\* \*\*

\*\*\*\*\*

26 KK \* 4002.1 \*

\*\*\*\*\*

RUN DATE 7/16/2009  
RATIONAL METHOD HYDROGRAPH PROGRAM  
COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
6HR RAINFALL IS 3.6 INCHES  
RATIONAL METHOD RUNOFF COEFFICIENT IS 0.3  
RATIONAL METHOD TIME OF CONCENTRATION IS 13 MIN.  
FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
IT 2 01JAN90 1200 200

36 IN TIME DATA FOR INPUT TIME SERIES  
JXMIN 13 TIME INTERVAL IN MINUTES

JXDATE 1JAN90 STARTING DATE  
JXTIME 1147 STARTING TIME

SUBBASIN RUNOFF DATA

35 BA SUBBASIN CHARACTERISTICS  
TAREA .00 SUBBASIN AREA

\*\*\*

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION 4002.1

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	9.98-HR
5.	4.12	(CFS)	1.	0.	0.	0.
		(INCHES)	1.061	1.061	1.061	1.061
		(AC-FT)	0.	0.	0.	0.
CUMULATIVE AREA =			.00 SQ MI			

\*\*\* \*\*

\*\*\*\*\*

41 KK \* Combine \*

Combine the two drainage areas entering the detention basin

43 HC HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

HYDROGRAPH AT STATION Combine

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	9.98-HR
40.	4.05	(CFS)	3.	2.	2.	2.
		(INCHES)	1.846	1.847	1.847	1.847
		(AC-FT)	2.	2.	2.	2.
CUMULATIVE AREA =			.02 SQ MI			

\*\*\* \*\*

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\* \*

44 KK \* DETAIN \*  
 \* \*  
 \*\*\*\*\*

100-YEAR DETENTION

46 KO OUTPUT CONTROL VARIABLES

IPRNT 3 PRINT CONTROL  
 IPLOT 1 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 600 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT .017 TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

47 RS STORAGE ROUTING

NSTPS 1 NUMBER OF SUBREACHES  
 ITYP STOR TYPE OF INITIAL CONDITION  
 RSVRIC -1.00 INITIAL CONDITION  
 X .00 WORKING R AND D COEFFICIENT

		.0	.7	.9	1.0	1.2
48 SV	STORAGE	.0	.7	.9	1.0	1.2
49 SQ	DISCHARGE	0.	1.	3.	6.	16.
50 SE	ELEVATION	100.00	102.40	103.00	103.32	104.00

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HYDROGRAPH AT STATION DETAIN

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	9.98-HR
15.	4.13	(CFS)	3.	2.	2.	2.
		(INCHES)	1.504	1.718	1.718	1.718
		(AC-FT)	1.	1.	1.	1.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	9.98-HR
1.	4.13		1.	1.	1.	1.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	9.98-HR
104.00	4.13		102.74	102.43	102.43	102.43

CUMULATIVE AREA = .02 SQ MI

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51 KK \* 4006 \*  
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Undetained Area Trib to Node 4006  
RUN DATE 7/16/2009  
RATIONAL METHOD HYDROGRAPH PROGRAM  
COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
6HR RAINFALL IS 3.6 INCHES  
RATIONAL METHOD RUNOFF COEFFICIENT IS 0.284  
RATIONAL METHOD TIME OF CONCENTRATION IS 16 MIN.  
FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
IT 2 01JAN90 1200 200

62 IN TIME DATA FOR INPUT TIME SERIES  
JXMIN 16 TIME INTERVAL IN MINUTES  
JXDATE 1JAN90 STARTING DATE  
JXTIME 1152 STARTING TIME

SUBBASIN RUNOFF DATA

61 BA SUBBASIN CHARACTERISTICS  
TAREA .00 SUBBASIN AREA

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HYDROGRAPH AT STATION 4006

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	9.98-HR
1.	4.13	(CFS)	0.	0.	0.	0.
		(INCHES)	1.051	1.062	1.062	1.062
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

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67 KK \* Combine \*  
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Combine detained outflow from DB4 and area trib to Node 4006

69 KO OUTPUT CONTROL VARIABLES  
IPRNT 3 PRINT CONTROL  
IPLOT 1 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 600 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .017 TIME INTERVAL IN HOURS

70 HC

HYDROGRAPH COMBINATION

ICOMP

2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION Combine

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	9.98-HR
17.	4.13	(CFS)	3.	2.	2.	2.
		(INCHES)	1.443	1.654	1.654	1.654
		(AC-FT)	1.	2.	2.	2.
		CUMULATIVE AREA =	.02 SQ MI			

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	4003	36.	4.05	3.	2.	2.	.01		
HYDROGRAPH AT	4002.1	5.	4.12	1.	0.	0.	.00		
2 COMBINED AT	Combine	40.	4.05	3.	2.	2.	.02		
ROUTED TO	DETAIN	15.	4.13	3.	2.	2.	.02	104.00	4.13
HYDROGRAPH AT	4006	1.	4.13	0.	0.	0.	.00		
2 COMBINED AT	Combine	17.	4.13	3.	2.	2.	.02		

\*\*\* NORMAL END OF HEC-1 \*\*\*

## **Drainage Basin 7000A and 7000B**

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1998 *
* VERSION 4.1 *
*
* RUN DATE 13AUG09 TIME 16:26:33 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****

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X      X XXXXXXX XXXXX      X
X      X X      X      X      XX
X      X X      X      X      X
XXXXXXX XXXX      X      XXXXX X
X      X X      X      X      X
X      X X      X      X      X
X      X XXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

\*\*\* FREE \*\*\*

\*DIAGRAM

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1  ID  MEADOWOOD J-15956 01/19/09 FILE: MW7A7B.HC1
2  ID  DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)
3  ID  FOR COMINED DRAINAGE BASINS 7000A AND 7000B
4  IT   1 01JAN90   1200   900
5  IO   3       1

6  KK   7000A
7  KM   DRAINAGE BASIN 7000A
8  KM   RUN DATE   8/8/2009
9  KM   RATIONAL METHOD HYDROGRAPH PROGRAM
10 KM   COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
11 KM   6HR RAINFALL IS  3.6  INCHES
12 KM   RATIONAL METHOD RUNOFF COEFFICIENT IS  0.49
13 KM   RATIONAL METHOD TIME OF CONCENTRATION IS  10  MIN.
14 KM   FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
15 KM   IT 2 01JAN90 1200 200
16 KO   0       0       0       0       21
17 BA  0.3039
18 IN   10 01JAN90   1155
19 QI   0    20.5   20.9   21.7   22.2   23.1   23.7   24.8   25.4   26.8
20 QI  27.5   29.3   30.2   32.4   33.7   36.6   38.3   42.5   45.1   51.6
21 QI   56   68.4    78   114.5  233.6  505.77  91.8   61.4   48.1   40.3
22 QI   35   31.3   28.4   26.1   24.2   22.6   21.3    0      0      0
23 QI   0     0     0     0     0     0     0     0     0     0

24 KK   DB7A
25 KM   100-YEAR DETENTION
26 KO   0       0       0       0       21
27 RS   1    STOR   6.75
28 SV   0   9.329  11.95  14.77  18.8
29 SQ   0  13.08  31.51  96.4   255
30 SE  100 103.167 104.0 104.87  106

31 KK   7000B
32 KM   DRIANAGE BASIN 7000B
33 KM   RUN DATE   8/8/2009
34 KM   RATIONAL METHOD HYDROGRAPH PROGRAM
35 KM   COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
36 KM   6HR RAINFALL IS  3.6  INCHES
37 KM   RATIONAL METHOD RUNOFF COEFFICIENT IS  0.41
38 KM   RATIONAL METHOD TIME OF CONCENTRATION IS  12  MIN.
39 KM   FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
40 KM   IT 2 01JAN90 1200 200
41 KO   0       0       0       0       21
42 BA  0.07
43 IN   12 01JAN90   1154
44 QI   0     4     4.1   4.2   4.4   4.6   4.7    5    5.2   5.6
45 QI   5.8   6.3   6.6   7.3   7.7   8.8   9.6  11.7  13.4  19.6
46 QI  29.3  97.43  15.7  10.5   8.2   6.9    6    5.4   4.9   4.5
47 QI   4.1    0     0     0     0     0     0     0     0     0
48 QI   0     0

```

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
49	KK DB7B
50	KM DETAIN 7000B
51	KO 0 0 0 0 21
52	RS 1 STOR 1.3
53	SV 0 2.544 3.302 3.69 4.2
54	SQ 0 2.642 11.50 21.90 45.6
55	SE 100 103.167 104.0 104.41 106
56	KK7000B_DS
57	KM DRAIANGE BASIN DOWNSTREAM OF DB7B (NOT DETAINED)
58	KM RUN DATE 8/8/2009
59	KM RATIONAL METHOD HYDROGRAPH PROGRAM
60	KM COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
61	KM 6HR RAINFALL IS 3.6 INCHES
62	KM RATIONAL METHOD RUNOFF COEFFICIENT IS 0.6
63	KM RATIONAL METHOD TIME OF CONCENTRATION IS 6 MIN.
64	KM FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
65	KM IT 2 01JAN90 1200 200
66	BA 0.0008
67	IN 6 01JAN90 1157
68	QI 0 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1
69	QI 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1
70	QI 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1
71	QI 0.1 0.2 0.2 0.2 0.2 0.2 0.2 0.3 0.3 0.5
72	QI 0.8 2.44 0.4 0.3 0.2 0.2 0.2 0.1 0.1 0.1
73	QI 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1 0.1
74	QI 0.1 0 0 0 0 0 0 0 0 0
75	QI 0 0
76	KK COMBINE
77	KO 0 0 0 0 21
78	HC 3
79	ZZ

# SCHEMATIC DIAGRAM OF STREAM NETWORK

## INPUT

LINE	(V) ROUTING	(--->) DIVERSION OR PUMP FLOW
NO.	(.) CONNECTOR	(<---) RETURN OF DIVERTED OR PUMPED FLOW
6	7000A	
	V	
	V	
24	DB7A	
	.	
31	.	7000B
	.	V
	.	V
49	.	DB7B
	.	.
	.	.
56	.	7000B_DS
	.	.
	.	.
76	COMBINE.....	

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION



```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 13AUG09 TIME 16:26:33
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
```

MEADOWOOD J-15956 01/19/09 FILE: MW7A7B.HC1  
 DETENTION FOR 100-YEAR STORM EVENT (BASED ON RATIONAL METHOD)  
 FOR COMINED DRAINAGE BASINS 7000A AND 7000B

5 IO OUTPUT CONTROL VARIABLES

```
IPRNT      3 PRINT CONTROL
IPLOT      1 PLOT CONTROL
QSCAL      0. HYDROGRAPH PLOT SCALE
```

IT HYDROGRAPH TIME DATA

```
NMIN      1 MINUTES IN COMPUTATION INTERVAL
IDATE     1JAN90 STARTING DATE
ITIME     1200 STARTING TIME
NQ        900 NUMBER OF HYDROGRAPH ORDINATES
NDDATE    2JAN90 ENDING DATE
NDTIME    0259 ENDING TIME
ICENT     19 CENTURY MARK
```

```
COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 14.98 HOURS
```

ENGLISH UNITS

```
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT
```

\*\*\*\*\*

6 KK

```
*****
*
* 7000A
*
*****
```

DRAINAGE BASIN 7000A  
 RUN DATE 8/8/2009  
 RATIONAL METHOD HYDROGRAPH PROGRAM  
 COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
 6HR RAINFALL IS 3.6 INCHES  
 RATIONAL METHOD RUNOFF COEFFICIENT IS 0.49

RATIONAL METHOD TIME OF CONCENTRATION IS 10 MIN.  
FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
IT 2 01JAN90 1200 200

16 KO            OUTPUT CONTROL VARIABLES  
                 IPRNT            3   PRINT CONTROL  
                 IPLOT            1   PLOT CONTROL  
                 QSCAL            0.   HYDROGRAPH PLOT SCALE  
                 IPNCH            0   PUNCH COMPUTED HYDROGRAPH  
                 IOUT            21   SAVE HYDROGRAPH ON THIS UNIT  
                 ISAV1            1   FIRST ORDINATE PUNCHED OR SAVED  
                 ISAV2            900   LAST ORDINATE PUNCHED OR SAVED  
                 TIMINT            .017   TIME INTERVAL IN HOURS

18 IN            TIME DATA FOR INPUT TIME SERIES  
                 JXMIN            10   TIME INTERVAL IN MINUTES  
                 JXDATE           1JAN90   STARTING DATE  
                 JXTIME           1155   STARTING TIME

SUBBASIN RUNOFF DATA

17 BA            SUBBASIN CHARACTERISTICS  
                 TAREA            .30   SUBBASIN AREA

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HYDROGRAPH AT STATION    7000A

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	14.98-HR
506.	4.08	(CFS)	57.	23.	23.	23.
		(INCHES)	1.749	1.751	1.751	1.751
		(AC-FT)	28.	28.	28.	28.

CUMULATIVE AREA =    .30 SQ MI

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\*            \*  
24 KK    \*    DB7A    \*  
\*            \*  
\*\*\*\*\*

100-YEAR DETENTION

26 KO            OUTPUT CONTROL VARIABLES  
                 IPRNT            3   PRINT CONTROL  
                 IPLOT            1   PLOT CONTROL  
                 QSCAL            0.   HYDROGRAPH PLOT SCALE  
                 IPNCH            0   PUNCH COMPUTED HYDROGRAPH  
                 IOUT            21   SAVE HYDROGRAPH ON THIS UNIT  
                 ISAV1            1   FIRST ORDINATE PUNCHED OR SAVED  
                 ISAV2            900   LAST ORDINATE PUNCHED OR SAVED

TIMINT .017 TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

27 RS STORAGE ROUTING  
NSTPS 1 NUMBER OF SUBREACHES  
ITYP STOR TYPE OF INITIAL CONDITION  
RSVRIC 6.75 INITIAL CONDITION  
X .00 WORKING R AND D COEFFICIENT

28 SV STORAGE .0 9.3 11.9 14.8 18.8

29 SQ DISCHARGE 0. 13. 32. 96. 255.

30 SE ELEVATION 100.00 103.17 104.00 104.87 106.00

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HYDROGRAPH AT STATION DB7A

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	14.98-HR
254.	4.18	(CFS)	49.	25.	25.	25.
		(INCHES)	1.513	1.926	1.926	1.926
		(AC-FT)	25.	31.	31.	31.

PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	14.98-HR
19.	4.18		12.	9.	9.	9.

PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	14.98-HR
106.00	4.18		103.95	102.89	102.89	102.89

CUMULATIVE AREA = .30 SQ MI

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\* \*  
31 KK \* 7000B \*  
\* \*  
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DRIANAGE BASIN 7000B  
RUN DATE 8/8/2009  
RATIONAL METHOD HYDROGRAPH PROGRAM  
COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
6HR RAINFALL IS 3.6 INCHES  
RATIONAL METHOD RUNOFF COEFFICIENT IS 0.41  
RATIONAL METHOD TIME OF CONCENTRATION IS 12 MIN.  
FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
IT 2 01JAN90 1200 200

41 KO            OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	1	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	900	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.017	TIME INTERVAL IN HOURS

43 IN            TIME DATA FOR INPUT TIME SERIES

JXMIN	12	TIME INTERVAL IN MINUTES
JXDATE	1JAN90	STARTING DATE
JXTIME	1154	STARTING TIME

SUBBASIN RUNOFF DATA

42 BA            SUBBASIN CHARACTERISTICS

TAREA	.07	SUBBASIN AREA
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HYDROGRAPH AT STATION    7000B

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	14.98-HR
97.	4.10	(CFS)	11.	4.	4.	4.
		(INCHES)	1.463	1.466	1.466	1.466
		(AC-FT)	5.	5.	5.	5.

CUMULATIVE AREA =    .07 SQ MI

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\*            \*

49 KK            \*        DB7B   \*

\*            \*

\*\*\*\*\*

DETAIN 7000B

51 KO            OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	1	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	900	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.017	TIME INTERVAL IN HOURS

HYDROGRAPH ROUTING DATA

52 RS	STORAGE ROUTING					
	NSTPS	1	NUMBER OF SUBREACHES			
	ITYP	STOR	TYPE OF INITIAL CONDITION			
	RSVRIC	1.30	INITIAL CONDITION			
	X	.00	WORKING R AND D COEFFICIENT			
53 SV	STORAGE	.0	2.5	3.3	3.7	4.2
54 SQ	DISCHARGE	0.	3.	12.	22.	46.
55 SE	ELEVATION	100.00	103.17	104.00	104.41	106.00

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# HYDROGRAPH AT STATION DB7B

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW				
(CFS)	(HR)	6-HR	24-HR	72-HR	14.98-HR	
46.	4.23	(CFS)	8.	4.	4.	4.
		(INCHES)	1.118	1.467	1.467	1.467
		(AC-FT)	4.	5.	5.	5.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	6-HR	24-HR	72-HR	14.98-HR
4.	4.23	3.	2.	2.	2.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	14.98-HR
106.00	4.23	103.52	102.67	102.67	102.67

CUMULATIVE AREA = .07 SQ MI

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 \* \*  
 56 KK \* 7000B\_DS \*  
 \* \*  
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DRAIANGE BASIN DOWNSTREAM OF DB7B (NOT DETAINED)  
 RUN DATE 8/8/2009  
 RATIONAL METHOD HYDROGRAPH PROGRAM  
 COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
 6HR RAINFALL IS 3.6 INCHES  
 RATIONAL METHOD RUNOFF COEFFICIENT IS 0.6  
 RATIONAL METHOD TIME OF CONCENTRATION IS 6 MIN.  
 FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
 IT 2 01JAN90 1200 200

67 IN	TIME DATA FOR INPUT TIME SERIES		
	JXMIN	6	TIME INTERVAL IN MINUTES
	JXDATE	1JAN90	STARTING DATE
	JXTIME	1157	STARTING TIME

## SUBBASIN RUNOFF DATA

66 BA

## SUBBASIN CHARACTERISTICS

TAREA .00 SUBBASIN AREA

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## HYDROGRAPH AT STATION 7000B\_DS

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	14.98-HR
2.	4.05	(CFS)	0.	0.	0.	0.
		(INCHES)	2.172	2.175	2.175	2.175
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

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\* \*

76 KK

\* COMBINE \*

\* \*

\*\*\*\*\*

77 KO

## OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLT	1	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	900	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.017	TIME INTERVAL IN HOURS

78 HC

## HYDROGRAPH COMBINATION

ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

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## HYDROGRAPH AT STATION COMBINE

PEAK FLOW (CFS)	TIME (HR)		6-HR	24-HR	72-HR	14.98-HR
299.	4.20	(CFS)	58.	30.	30.	30.
		(INCHES)	1.439	1.841	1.841	1.841
		(AC-FT)	29.	37.	37.	37.

CUMULATIVE AREA = .37 SQ MI



RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	7000A	506.	4.08	57.	23.	23.	.30		
ROUTED TO	DB7A	254.	4.18	49.	25.	25.	.30	106.00	4.18
HYDROGRAPH AT	7000B	97.	4.10	11.	4.	4.	.07		
ROUTED TO	DB7B	46.	4.23	8.	4.	4.	.07	106.00	4.23
HYDROGRAPH AT	7000B_DS	2.	4.05	0.	0.	0.	.00		
3 COMBINED AT	COMBINE	299.	4.20	58.	30.	30.	.37		

\*\*\* NORMAL END OF HEC-1 \*\*\*



## **Drainage Basin 8000**

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*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*      JUN 1998                    *
*      VERSION 4.1                  *
*
* RUN DATE 29JUL09 TIME 09:30:52 *
*
*****

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*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
*      609 SECOND STREET
*      DAVIS, CALIFORNIA 95616
*      (916) 756-1104
*
*****

```

```

X      X XXXXXXX XXXXX      X
X      X X      X      X      XX
X      X X      X      X      X
XXXXXXX XXXX      X      XXXXX X
X      X X      X      X      X
X      X X      X      X      X
X      X XXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.  
 THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS.DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

LINE	ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
------	---

\*\*\* FREE \*\*\*

\*DIAGRAM

```

1 ID Meadowood J-15956
2 ID 100-YEAR, 6-HOUR DETENTION ANALYSIS
3 ID 7/28/09 FILENAME: MW8000.HC1
4 IT 1 01JAN90 1200 2000
5 IO 3 1
6
7 KK8149.hcl
8 KM RUN DATE 7/28/2009
9 KM FLOW INFORMATION AT NODE 8149 THAT ENTERS DET BASIN
10 KM RATIONAL METHOD HYDROGRAPH PROGRAM
11 KM COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
12 KM 6HR RAINFALL IS 3.6 INCHES
13 KM RATIONAL METHOD RUNOFF COEFFICIENT IS 0.55
14 KM RATIONAL METHOD TIME OF CONCENTRATION IS 10 MIN.
15 KM FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
16 KM IT 2 01JAN90 1200 200
17 BA 0.0384
18 IN 10 01JAN90 1155
19 QI 0 3 3 3.1 3.2 3.3 3.4 3.6 3.7 3.9
20 QI 4 4.2 4.4 4.7 4.9 5.3 5.5 6.1 6.5 7.5
21 QI 8.1 9.9 11.3 16.5 16.8 90.04 13.3 8.9 6.9 5.8
22 QI 5.1 4.5 4.1 3.8 3.5 3.3 3.1 0 0 0
23 QI 0 0 0 0 0 0 0 0 0 0
24
25 KK DetA
26 KO 0 0 0 0 21
27 RS 1 STOR -1
28 SV 0 .65 .86 1.11 1.78
29 SQ 0 1.54 3.90 13.18 45
30 SE 0 102.37 103 103.72 104
31
32 KK8152.hcl
33 KM RUN DATE 7/28/2009
34 KM FLOW INFORMATION AT NODE 8152 THAT IS NOT DETAINED
35 KM RATIONAL METHOD HYDROGRAPH PROGRAM
36 KM COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
37 KM 6HR RAINFALL IS 3.6 INCHES
38 KM RATIONAL METHOD RUNOFF COEFFICIENT IS 0.701
39 KM RATIONAL METHOD TIME OF CONCENTRATION IS 6 MIN.
40 KM FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
41 KM IT 2 01JAN90 1200 200
42 BA 0.0034
43 IN 6 01JAN90 1157
44 QI 0 0.3 0.3 0.3 0.3 0.4 0.4 0.4 0.4 0.4
45 QI 0.4 0.4 0.4 0.4 0.4 0.4 0.4 0.5 0.5 0.5
46 QI 0.5 0.5 0.5 0.6 0.6 0.6 0.6 0.7 0.7 0.7
47 QI 0.8 0.8 0.9 1 1 1.2 1.3 1.5 1.8 2.6
48 QI 2.9 13.73 2.1 1.4 1.1 0.9 0.8 0.7 0.6 0.6
49 QI 0.5 0.5 0.5 0.5 0.4 0.4 0.4 0.4 0.4 0.4
50 QI 0.3 0 0 0 0 0 0 0 0 0
51 QI 0 0

```

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

49      KK Combine
50      KO      0      0      0      0      21
51      HC      2

52      KK8200.hcl
53      KM      RUN DATE   3/18/2009
54      KM      FLOW INFORMATION FROM BASIN 8200 THAT ENTERS DET BASIN
55      KM      RATIONAL METHOD HYDROGRAPH PROGRAM
56      KM      COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY
57      KM      6HR RAINFALL IS  3.6  INCHES
58      KM      RATIONAL METHOD RUNOFF COEFFICIENT IS  0.551
59      KM      RATIONAL METHOD TIME OF CONCENTRATION IS  11  MIN.
60      KM      FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1
61      KM      IT 2 01JAN90 1200 200
62      BA      0.0408
63      IN      11 01JAN90      1153
64      QI      0      3.1      3.1      3.3      3.4      3.5      3.6      3.8      3.9      4.2
65      QI      4.3      4.6      4.8      5.2      5.4      6      6.4      7.3      7.9      9.7
66      QI      11.1      16.2      24.6      80.3      13      8.7      6.8      5.7      5      4.4
67      QI      4      3.7      3.4      3.2      0      0      0      0      0      0
68      QI      0      0      0      0      0

69      XK      DetB
70      KO      0      0      0      0      21
71      RS      1      STOR      -1
72      SV      0      1.27      1.63      1.97      2.81
73      SQ      0      1.05      3.2      9.40      38.18
74      SE      0      102.34      103      103.54      104

75      KK Combine
76      KO      0      0      0      0      21
77      HC      2
78      ZZ

```

# SCHEMATIC DIAGRAM OF STREAM NETWORK

## INPUT

LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW  
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

```

6      8149.hcl
      V
      V
23      DetA
      .
      .
29      .      8152.hcl
      .      .
      .      .
49      Combine.....
      .
      .
52      .      8200.hcl
      .      V
      .      V
69      .      DetB
      .      .
      .      .
75      Combine.....
  
```

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

```
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* JUN 1998
* VERSION 4.1
*
* RUN DATE 29JUL09 TIME 09:30:52
*
*****
```

```
*****
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*****
```

Meadowood J-15956  
100-YEAR, 6-HOUR DETENTION ANALYSIS  
7/28/09 FILENAME: MW8000.HC1

5 IO OUTPUT CONTROL VARIABLES

```
IPRNT      3 PRINT CONTROL
IPLOT      1 PLOT CONTROL
QSCAL      0. HYDROGRAPH PLOT SCALE
```

IT HYDROGRAPH TIME DATA

```
NMIN      1 MINUTES IN COMPUTATION INTERVAL
IDATE     1JAN90 STARTING DATE
ITIME     1200 STARTING TIME
NQ        2000 NUMBER OF HYDROGRAPH ORDINATES
NDDATE    2JAN90 ENDING DATE
NDTIME    2119 ENDING TIME
ICENT     19 CENTURY MARK
```

```
COMPUTATION INTERVAL .02 HOURS
TOTAL TIME BASE 33.32 HOURS
```

ENGLISH UNITS

```
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT
```

\*\*\* \*\*

6 KK

```
*****
*
* 8149.hcl
*
*****
```

RUN DATE 7/28/2009  
FLOW INFORMATION AT NODE 8149 THAT ENTERS DET BASIN  
RATIONAL METHOD HYDROGRAPH PROGRAM  
COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
6HR RAINFALL IS 3.6 INCHES  
RATIONAL METHOD RUNOFF COEFFICIENT IS 0.55

RATIONAL METHOD TIME OF CONCENTRATION IS 10 MIN.  
 FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
 IT 2 01JAN90 1200 200

17 IN TIME DATA FOR INPUT TIME SERIES  
 JXMIN 10 TIME INTERVAL IN MINUTES  
 JXDATE 1JAN90 STARTING DATE  
 JXTIME 1155 STARTING TIME

# SUBBASIN RUNOFF DATA

16 BA SUBBASIN CHARACTERISTICS  
 TAREA .04 SUBBASIN AREA

\*\*\*

\*\*\* \*\*\* \*\*\* \*\*\* \*\*\*

## HYDROGRAPH AT STATION 8149.hcl

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	33.32-HR
90.	4.08	(CFS) 8.	2.	1.	1.
		(INCHES) 2.001	2.003	2.003	2.003
		(AC-FT) 4.	4.	4.	4.

CUMULATIVE AREA = .04 SQ MI

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\*\*\*\*\*  
 \* \*  
 23 KK \* DetA \*  
 \* \*  
 \*\*\*\*\*

24 KO OUTPUT CONTROL VARIABLES  
 IPRNT 3 PRINT CONTROL  
 IPLOT 1 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 2000 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT .017 TIME INTERVAL IN HOURS

## HYDROGRAPH ROUTING DATA

25 RS STORAGE ROUTING  
 NSTPS 1 NUMBER OF SUBREACHES  
 ITYP STOR TYPE OF INITIAL CONDITION  
 RSVRIC -1.00 INITIAL CONDITION  
 X .00 WORKING R AND D COEFFICIENT

26 SV STORAGE .0 .6 .9 1.1 1.8

\*\*\*

★ ★ ★                      ★ ★ ★                      ★ ★ ★                      ★ ★ ★                      ★ ★ ★

CUMULATIVE AREA = .04 SQ MI

\*\*\*\*\*

39 BA SUBBASIN CHARACTERISTICS

TAREA	SUBBASIN AREA
.00	

☆☆☆



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HYDROGRAPH AT STATION 8152.hc1

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	33.32-HR
14.	4.05	(CFS)	1.	0.	0.	0.
		(INCHES)	2.546	2.547	2.547	2.547
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = .00 SQ MI

\*\*\*

\*\*\*\*\*

49 KK

\* Combine \*

50 KO

OUTPUT CONTROL VARIABLES

IPRNT	3	PRINT CONTROL
IPLOT	1	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	2000	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.017	TIME INTERVAL IN HOURS

51 HC

HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION Combine

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	33.32-HR
46.	4.18	(CFS)	9.	3.	2.	2.
		(INCHES)	1.969	2.321	2.330	2.330
		(AC-FT)	4.	5.	5.	5.

CUMULATIVE AREA = .04 SQ MI

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52 KK \* 8200.hc1 \*  
\* \*  
\*\*\*\*\*

RUN DATE 3/18/2009  
FLOW INFORMATION FROM BASIN 8200 THAT ENTERS DET BASIN  
RATIONAL METHOD HYDROGRAPH PROGRAM  
COPYRIGHT 1992, 2001, RICK ENGINEERING COMPANY  
6HR RAINFALL IS 3.6 INCHES  
RATIONAL METHOD RUNOFF COEFFICIENT IS 0.551  
RATIONAL METHOD TIME OF CONCENTRATION IS 11 MIN.  
FOR THIS DATA TO RUN PROPERLY THIS IT CARD MUST BE ADDED TO YOUR HEC-1  
IT 2 01JAN90 1200 200

63 IN TIME DATA FOR INPUT TIME SERIES  
JXMIN 11 TIME INTERVAL IN MINUTES  
JXDATE 1JAN90 STARTING DATE  
JXTIME 1153 STARTING TIME

SUBBASIN RUNOFF DATA

62 BA SUBBASIN CHARACTERISTICS  
TAREA .04 SUBBASIN AREA

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HYDROGRAPH AT STATION 8200.hc1

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)		6-HR	24-HR	72-HR	33.32-HR
80.	4.10	(CFS)	9.	2.	2.	2.
		(INCHES)	1.966	1.970	1.970	1.970
		(AC-FT)	4.	4.	4.	4.

CUMULATIVE AREA = .04 SQ MI

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69 KK \* DetB \*  
\* \*  
\*\*\*\*\*

70 KO OUTPUT CONTROL VARIABLES  
IPRNT 3 PRINT CONTROL  
IPLOT 1 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
ISAV2 2000 LAST ORDINATE PUNCHED OR SAVED  
TIMINT .017 TIME INTERVAL IN HOURS

## HYDROGRAPH ROUTING DATA

71 RS            STORAGE ROUTING

                NSTPS            1    NUMBER OF SUBREACHES

                ITYP            STOR    TYPE OF INITIAL CONDITION

                RSVRIC        -1.00    INITIAL CONDITION

                X                .00    WORKING R AND D COEFFICIENT

72 SV            STORAGE            .0            1.3            1.6            2.0            2.8

73 SQ            DISCHARGE           0.            1.            3.            9.            38.

74 SE            ELEVATION           .00          102.34          103.00          103.54          104.00

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## HYDROGRAPH AT STATION    DetB

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	33.32-HR
38.	4.22	(CFS) 8.	3.	2.	2.
		(INCHES) 1.862	2.422	2.517	2.517
		(AC-FT) 4.	5.	5.	5.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	6-HR	24-HR	72-HR	33.32-HR
3.	4.22	2.	1.	1.	1.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	33.32-HR
104.00	4.22	103.23	77.45	63.19	63.19

CUMULATIVE AREA = .04 SQ MI

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\*            \*

75 KK       \*    Combine   \*

\*            \*

\*\*\*\*\*

76 KO            OUTPUT CONTROL VARIABLES

                IPRNT            3    PRINT CONTROL

                IPLOT            1    PLOT CONTROL

                QSCAL            0.    HYDROGRAPH PLOT SCALE

                IPNCH            0    PUNCH COMPUTED HYDROGRAPH

                IOUT            21    SAVE HYDROGRAPH ON THIS UNIT

                ISAV1            1    FIRST ORDINATE PUNCHED OR SAVED

                ISAV2            2000    LAST ORDINATE PUNCHED OR SAVED

                TIMINT            .017    TIME INTERVAL IN HOURS

77 HC            HYDROGRAPH COMBINATION

ICOMP

2 NUMBER OF HYDROGRAPHS TO COMBINE

\*\*\*

\*\*\*

\*\*\*

\*\*\*

\*\*\*

\*\*\*

HYDROGRAPH AT STATION Combine

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	33.32-HR
84.	4.20	(CFS) 17.	5.	4.	4.
		(INCHES) 1.915	2.371	2.422	2.422
		(AC-FT) 8.	10.	11.	11.

CUMULATIVE AREA = .08 SQ MI

RUNOFF SUMMARY  
 FLOW IN CUBIC FEET PER SECOND  
 TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD			BASIN AREA	MAXIMUM STAGE	TIME OF MAX STAGE
				6-HOUR	24-HOUR	72-HOUR			
HYDROGRAPH AT	8149.hc1	90.	4.08	8.	2.	1.	.04		
ROUTED TO	DetA	45.	4.18	8.	2.	2.	.04	104.00	4.18
HYDROGRAPH AT	8152.hc1	14.	4.05	1.	0.	0.	.00		
2 COMBINED AT	Combine	46.	4.18	9.	3.	2.	.04		
HYDROGRAPH AT	8200.hc1	80.	4.10	9.	2.	2.	.04		
ROUTED TO	DetB	38.	4.22	8.	3.	2.	.04	104.00	4.22
2 COMBINED AT	Combine	84.	4.20	17.	5.	4.	.08		

\*\*\* NORMAL END OF HEC-1 \*\*\*

**Appendix F**  
**WSPGW Analysis for SR-76 Crossing**

0

T3 05/29/2009

SO		.000	256.430	1				.258.210		
R		471.600	258.820	1		.014			.000	
JX		471.700	258.821	4	3	.014	6.080	258.821	90.0	
		.000								
TS		475.700	258.840	5		.014			.000	
WX		475.700	258.840	6						
R		587.200	259.380	6		.013			.000	.000 0
WE		587.200	259.380	7		.500				
TS		591.200	259.400	8		.014			.000	
JX		591.300	259.401	10	9	.014	5.400	259.400	90.0	
		.000								
R		1125.300	262.158	10		.014			.000	
JX		1129.300	262.159	14	13	.014	5.400	262.160	.0	-
		90.000								
R		1129.400	262.160	14		.014			.000	
WX		1129.400	262.160	15						
R		1250.800	262.740	15		.013			.000	.000 0
JX		1260.600	262.741	16		.013		263.070		
		90.000								
R		1286.800	262.920	16		.013			.000	.000 0
TS		1286.810	262.921	17		.030				
R		1670.670	264.960	17		.030			.000	.000 0
SH		2156.800	268.960	18				268.200		
CD	1	1	0	.000	3.300	2.000	1.500	1.500	.00	
CD	2	1	0	.000	3.300	2.000	1.500	1.500	.00	
CD	3	1	0	.000	3.300	.100	.000	.000	.00	
CD	4	1	0	.000	3.300	2.000	1.500	1.500	.00	
CD	5	1	0	.000	3.300	11.800	.000	.000	.00	
CD	6	4	2	.000	3.000	.000	.000	.000	.00	
CD	7	1	0	.000	3.300	11.800	.000	.000	.00	
CD	8	1	0	.000	2.500	2.000	1.500	1.500	.00	
CD	9	1	0	.000	2.500	.100	.000	.000	.00	
CD	10	1	0	.000	2.500	2.000	1.500	1.500	.00	
CD	11	1	0	.000	1.640	2.000	3.000	3.000	.00	
CD	12	1	0	.000	2.500	9.800	.000	.000	.00	
CD	13	1	0	.000	1.640	2.000	.000	.000	.00	
CD	14	1	0	.000	2.500	9.800	.000	.000	.00	
CD	15	4	2	.000	2.500	.000	.000	.000	.00	
CD	16	1	0	.000	3.300	2.000	1.500	1.500	.00	
CD	17	1	0	.000	3.300	2.000	3.000	3.000	.00	
CD	18	1	0	.000	3.300	2.000	3.000	3.000	.00	
Q			45.310	.0						

JN - 15956-A

Meadowood --- WSPGW Analysis for Existing Condition

05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Width	Top Height	Base Width	No With Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	ISE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
.000	256.430	1.779	258.209	62.19	7.49	.87	259.08	.00	1.98	7.34	3.300	2.000	1.50 0 .0
343.115	.0051	-	-	-	-	.0051	1.74	1.78	1.24	1.78	.014	.00	1.50 TRAP
343.115	258.169	1.779	259.947	62.19	7.49	.87	260.82	.00	1.98	7.34	3.300	2.000	1.50 0 .0
85.133	.0051	-	-	-	-	.0049	.42	1.78	1.24	1.78	.014	.00	1.50 TRAP
428.248	258.600	1.809	260.409	62.19	7.29	.83	261.24	.00	1.98	7.43	3.300	2.000	1.50 0 .0
31.211	.0051	-	-	-	-	.0044	.14	1.81	1.20	1.78	.014	.00	1.50 TRAP
459.460	258.758	1.864	260.623	62.19	6.96	.75	261.37	.00	1.98	7.59	3.300	2.000	1.50 0 .0
9.830	.0051	-	-	-	-	.0039	.04	1.86	1.13	1.78	.014	.00	1.50 TRAP
469.290	258.808	1.921	260.729	62.19	6.63	.68	261.41	.00	1.98	7.76	3.300	2.000	1.50 0 .0
2.310	.0051	-	-	-	-	.0034	.01	1.92	1.06	1.78	.014	.00	1.50 TRAP
471.600	258.820	1.980	260.800	62.19	6.32	.62	261.42	.00	1.98	7.94	3.300	2.000	1.50 0 .0
JUNCT STR	.0101	-	-	-	-	.0022	.00	1.98	1.00	-	.014	.00	1.50 TRAP
471.700	258.821	2.404	261.225	56.11	4.16	.27	261.49	.00	1.88	9.21	3.300	2.000	1.50 0 .0
TRANS STR	.0047	-	-	-	-	.0006	.00	2.40	.61	-	.014	.00	1.50 TRAP
475.700	258.840	2.662	261.502	56.11	1.79	.05	261.55	.00	.89	11.80	3.300	11.800	.00 0 .0
WALL EXIT	-	-	-	-	-	-	-	-	-	-	-	-	-
475.700	258.840	2.662	261.502	56.11	4.23	.28	261.78	.00	1.71	1.90	3.000	.000	.00 2 .0
38.203	.0048	-	-	-	-	.0016	.06	2.66	.28	1.68	.013	.00	.00 PIPE



JN - 15956-A  
Meadowood --- MSPGW Analysis for Existing Condition  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top	Height/	Base Wt	No Wth	
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
513.903	259.025	2.512	261.537	56.11	4.44	.31	261.84	.00	1.71	2.21	3.000	.000	.00	2 .0
8.593	.0048	-	-	-	-	.0017	.01	2.51	.33	1.68	.013	.00	.00	PIPE
522.496	259.067	2.480	261.547	56.11	4.49	.31	261.86	.00	1.71	2.27	3.000	.000	.00	2 .0
HYDRAULIC JUMP														
522.496	259.067	1.683	260.749	56.11	6.88	.73	261.48	.00	1.71	2.98	3.000	.000	.00	2 .0
56.532	.0048	-	-	-	-	.0048	.27	1.68	.73	1.68	.013	.00	.00	PIPE
579.028	259.340	1.683	261.023	56.11	6.88	.73	261.76	.00	1.71	2.98	3.000	.000	.00	2 .0
8.172	.0048	-	-	-	-	.0047	.04	1.68	.73	1.68	.013	.00	.00	PIPE
587.200	259.380	1.713	261.093	56.11	6.72	.70	261.80	.00	1.71	2.97	3.000	.000	.00	2 .0
587.200	259.380	2.214	261.594	56.11	5.02	.39	261.98	.00	1.71	2.64	3.000	.000	.00	2 .0
WALL ENTRANCE														
587.200	259.380	3.397	262.777	56.11	1.40	.03	262.81	.00	.89	11.80	3.300	11.800	.00	0 .0
TRANS STR														
591.200	259.400	3.349	262.749	56.11	2.39	.09	262.84	.00	1.88	12.05	2.500	2.000	1.50	0 .0
JUNCT STR														
591.300	259.401	3.383	262.784	50.71	2.12	.07	262.85	.00	1.79	12.15	2.500	2.000	1.50	0 .0
17.322	.0052	-	-	-	-	.0002	.00	3.38	.27	1.61	.014	.00	1.50	TRAP
608.622	259.490	3.290	262.780	50.71	2.22	.08	262.86	.00	1.79	11.87	2.500	2.000	1.50	0 .0
16.826	.0052	-	-	-	-	.0002	.00	3.29	.28	1.61	.014	.00	1.50	TRAP

Program Package Serial Number: 1462

WATER SURFACE PROFILE LISTING

Date: 6-8-2009 Time: 3:44:12

JN - 15956-A

Meadowood --- WSPGW Analysis for Existing Condition  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Flow Depth	Top Width	Height/Dia.	Base Wt	No With Pks/Plp
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Flow Norm Dp	"N"	X-Fall	2R	Type Ch
625.448	259.577	3.199	262.777	50.71	2.33	.08	262.86	.00	1.79	11.60	2.500	2.000	1.50 0 .0
16.332	.0052	-	-	-	-	.0003	.00	3.20	.30	1.61	.014	.00	1.50 TRAP
641.780	259.662	3.111	262.773	50.71	2.44	.09	262.87	.00	1.79	11.33	2.500	2.000	1.50 0 .0
15.842	.0052	-	-	-	-	.0003	.00	3.11	.32	1.61	.014	.00	1.50 TRAP
657.622	259.743	3.025	262.768	50.71	2.56	.10	262.87	.00	1.79	11.07	2.500	2.000	1.50 0 .0
15.352	.0052	-	-	-	-	.0004	.01	3.02	.34	1.61	.014	.00	1.50 TRAP
672.974	259.823	2.941	262.764	50.71	2.69	.11	262.88	.00	1.79	10.82	2.500	2.000	1.50 0 .0
14.863	.0052	-	-	-	-	.0004	.01	2.94	.36	1.61	.014	.00	1.50 TRAP
687.836	259.899	2.859	262.758	50.71	2.82	.12	262.88	.00	1.79	10.58	2.500	2.000	1.50 0 .0
14.371	.0052	-	-	-	-	.0005	.01	2.86	.38	1.61	.014	.00	1.50 TRAP
702.207	259.974	2.779	262.753	50.71	2.96	.14	262.89	.00	1.79	10.34	2.500	2.000	1.50 0 .0
13.875	.0052	-	-	-	-	.0005	.01	2.78	.40	1.61	.014	.00	1.50 TRAP
716.083	260.045	2.701	262.746	50.71	3.10	.15	262.90	.00	1.79	10.10	2.500	2.000	1.50 0 .0
13.374	.0052	-	-	-	-	.0006	.01	2.70	.43	1.61	.014	.00	1.50 TRAP
729.457	260.114	2.625	262.739	50.71	3.25	.16	262.90	.00	1.79	9.87	2.500	2.000	1.50 0 .0
12.864	.0052	-	-	-	-	.0007	.01	2.62	.46	1.61	.014	.00	1.50 TRAP
742.320	260.181	2.550	262.731	50.71	3.41	.18	262.91	.00	1.79	9.65	2.500	2.000	1.50 0 .0
12.341	.0052	-	-	-	-	.0008	.01	2.55	.48	1.61	.014	.00	1.50 TRAP

JN - 15956-A  
 Meadowood --- WSPGW Analysis for Existing Condition  
 05/29/2009

*****															*****														
Station	Invert Elev	Depth (ft)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top	Height/ Base Wt	No Wth																	
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	2R	Type Ch															
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****															
754.661	260.244	2.478	262.722	50.71	3.58	.20	262.92	.00	1.79	9.43	2.500	2.000	1.50	0 .0															
11.801	.0052	-	-	-	-	.0009	.01	2.48	.51	1.61	.014	.00	1.50	TRAP															
766.463	260.305	2.407	262.713	50.71	3.75	.22	262.93	.00	1.79	9.22	2.500	2.000	1.50	0 .0															
11.240	.0052	-	-	-	-	.0010	.01	2.41	.55	1.61	.014	.00	1.50	TRAP															
777.702	260.363	2.338	262.702	50.71	3.94	.24	262.94	.00	1.79	9.02	2.500	2.000	1.50	0 .0															
10.648	.0052	-	-	-	-	.0011	.01	2.34	.58	1.61	.014	.00	1.50	TRAP															
788.350	260.418	2.271	262.689	50.71	4.13	.26	262.95	.00	1.79	8.81	2.500	2.000	1.50	0 .0															
10.017	.0052	-	-	-	-	.0013	.01	2.27	.62	1.61	.014	.00	1.50	TRAP															
798.367	260.470	2.206	262.676	50.71	4.33	.29	262.97	.00	1.79	8.62	2.500	2.000	1.50	0 .0															
9.331	.0052	-	-	-	-	.0014	.01	2.21	.65	1.61	.014	.00	1.50	TRAP															
807.698	260.518	2.142	262.660	50.71	4.54	.32	262.98	.00	1.79	8.42	2.500	2.000	1.50	0 .0															
8.572	.0052	-	-	-	-	.0016	.01	2.14	.70	1.61	.014	.00	1.50	TRAP															
816.271	260.563	2.079	262.642	50.71	4.76	.35	262.99	.00	1.79	8.24	2.500	2.000	1.50	0 .0															
7.710	.0052	-	-	-	-	.0018	.01	2.08	.74	1.61	.014	.00	1.50	TRAP															
823.981	260.602	2.018	262.621	50.71	5.00	.39	263.01	.00	1.79	8.06	2.500	2.000	1.50	0 .0															
4.235	.0052	-	-	-	-	.0020	.01	2.02	.78	1.61	.014	.00	1.50	TRAP															
828.215	260.624	1.983	262.608	50.71	5.14	.41	263.02	.00	1.79	7.95	2.500	2.000	1.50	0 .0															
HYDRAULIC JUMP																													
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HYDRAULIC JUMP

Program Package Serial Number: 1462

## WATER SURFACE PROFILE LISTING

Date: 6- 8-2009 Time: 3:44:12

JN - 15956-A

Meadowood --- WSPGW Analysis for Existing Condition

05/29/2009

Station	Invert Elev	Depth {FT}	Water Elev	Q (CFS)	Vel {FPS}	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT or I.D.	Base Wt ZL	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR Type Ch
828.215	260.624	1.607	262.231	50.71	7.16	.80	263.03	.00	1.79	6.82	2.500	2.000	1.50 0 .0
180.776	.0052					.0052	.93	1.61	1.24	1.61	.014	.00	1.50 TRAP
1008.992	261.557	1.607	263.164	50.71	7.16	.80	263.96	.00	1.79	6.82	2.500	2.000	1.50 0 .0
75.732	.0052					.0050	.38	1.61	1.24	1.61	.014	.00	1.50 TRAP
1084.724	261.948	1.632	263.580	50.71	6.99	.76	264.34	.00	1.79	6.90	2.500	2.000	1.50 0 .0
29.422	.0052					.0045	.13	1.63	1.20	1.61	.014	.00	1.50 TRAP
1114.146	262.100	1.683	263.783	50.71	6.66	.69	264.47	.00	1.79	7.05	2.500	2.000	1.50 0 .0
9.046	.0052					.0040	.04	1.68	1.13	1.61	.014	.00	1.50 TRAP
1123.192	262.147	1.735	263.882	50.71	6.35	.63	264.51	.00	1.79	7.20	2.500	2.000	1.50 0 .0
2.108	.0052					.0035	.01	1.73	1.06	1.61	.014	.00	1.50 TRAP
1125.300	262.158	1.789	263.947	50.71	6.05	.57	264.52	4.28	1.79	7.37	2.500	2.000	1.50 0 .0
JUNCT STR	.0003					.0017	.01	6.07	1.00		.014	.00	1.50 TRAP
1129.300	262.159	2.379	264.538	45.31	1.94	.06	264.60	.00	.87	9.80	2.500	9.800	.00 0 .0
.100	.0101					.0002	.00	2.38	.22	.64	.014	.00	.00 TRAP
1129.400	262.160	2.378	264.538	45.31	1.94	.06	264.60	.00	.87	9.80	2.500	9.800	.00 0 .0
WALL EXIT													
1129.400	262.160	2.379	264.539	45.31	4.70	.34	264.88	.00	1.62	1.08	2.500	.000	.00 2 .0
62.672	.0048					.0027	.17	2.38	.28	1.69	.013	.00	.00 PIPE

## WATER SURFACE PROFILE LISTING

Date: 6-8-2009 Time: 3:44:12

JN - 15956-A  
Meadowood --- WSPGW Analysis for Existing Condition  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top	Height/Base Wt	No Wch
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude	NI Norm Dp	"N" X-Fall	ZL Prs/Pip
1192.072	262.459	2.213	264.673	45.31	4.93	.38	265.05	.00	1.62	1.59	2.500	.000 .00 2 .0
44.484	.0048	-	-	-	-	.0028	.13	2.21	.36	1.69	.013	.00 .00 PIPE
1236.556	262.672	2.089	264.761	45.31	5.17	.41	265.18	.00	1.62	1.85	2.500	.000 .00 2 .0
14.244	.0048	-	-	-	-	.0030	.04	2.09	.42	1.69	.013	.00 .00 PIPE
1250.800	262.740	2.049	264.789	45.31	5.26	.43	265.22	.26	1.62	1.92	2.500	.000 .00 2 .0
JUNCT STR .0001	-	-	-	-	-	.0017	.02	2.31	.44		.013	.00 .00 PIPE
----- WARNING - Junction Analysis - Change in Channel Type -----												
1260.600	262.741	2.667	265.408	45.31	2.83	.12	265.53	.00	1.69	10.00	3.300	2.000 1.50 0 .0
9.813	.0068	-	-	-	-	.0004	.00	2.67	.39	1.37	.013	.00 1.50 TRAP
1270.413	262.808	2.591	265.399	45.31	2.97	.14	265.54	.00	1.69	9.77	3.300	2.000 1.50 0 .0
9.416	.0068	-	-	-	-	.0005	.00	2.59	.42	1.37	.013	.00 1.50 TRAP
1279.829	262.872	2.518	265.390	45.31	3.12	.15	265.54	.00	1.69	9.55	3.300	2.000 1.50 0 .0
6.971	.0068	-	-	-	-	.0005	.00	2.52	.44	1.37	.013	.00 1.50 TRAP
1286.800	262.920	2.463	265.383	45.31	3.23	.16	265.55	.00	1.69	9.39	3.300	2.000 1.50 0 .0
TRANS STR .0976	-	-	-	-	-	.0019	.00	2.46	.47		.030	.00 1.50 TRAP
1286.810	262.921	2.586	265.507	45.31	1.80	.05	265.56	.00	1.40	17.51	3.300	2.000 3.00 0 .0
14.298	.0053	-	-	-	-	.0009	.01	2.59	.26	1.76	.030	.00 3.00 TRAP

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JN - 15956-A  
Meadowood --- WSPGW Analysis for Existing Condition  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top/Height	Base Wt	No With
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N" X-Fall	ZR Type Ch
1301.108	262.997	2.518	265.515	45.31	1.88	.06	265.57	.00	1.40	17.11	3.300	2.000 3.00 0 .0
14.219	.0053	-	-	-	-	.0010	.01	2.52	.28	1.76	.030	.00 3.00 TRAP
1315.327	263.072	2.452	265.524	45.31	1.98	.06	265.58	.00	1.40	16.71	3.300	2.000 3.00 0 .0
14.191	.0053	-	-	-	-	.0012	.02	2.45	.30	1.76	.030	.00 3.00 TRAP
1329.518	263.148	2.387	265.535	45.31	2.07	.07	265.60	.00	1.40	16.32	3.300	2.000 3.00 0 .0
14.225	.0053	-	-	-	-	.0013	.02	2.39	.32	1.76	.030	.00 3.00 TRAP
1343.742	263.223	2.324	265.547	45.31	2.17	.07	265.62	.00	1.40	15.94	3.300	2.000 3.00 0 .0
14.337	.0053	-	-	-	-	.0015	.02	2.32	.33	1.76	.030	.00 3.00 TRAP
1358.080	263.300	2.262	265.562	45.31	2.28	.08	265.64	.00	1.40	15.57	3.300	2.000 3.00 0 .0
14.553	.0053	-	-	-	-	.0017	.03	2.26	.36	1.76	.030	.00 3.00 TRAP
1372.633	263.377	2.202	265.579	45.31	2.39	.09	265.67	.00	1.40	15.21	3.300	2.000 3.00 0 .0
14.909	.0053	-	-	-	-	.0020	.03	2.20	.38	1.76	.030	.00 3.00 TRAP
1387.542	263.456	2.144	265.600	45.31	2.51	.10	265.70	.00	1.40	14.86	3.300	2.000 3.00 0 .0
15.464	.0053	-	-	-	-	.0022	.03	2.14	.40	1.76	.030	.00 3.00 TRAP
1403.005	263.538	2.086	265.625	45.31	2.63	.11	265.73	.00	1.40	14.52	3.300	2.000 3.00 0 .0
16.317	.0053	-	-	-	-	.0025	.04	2.09	.43	1.76	.030	.00 3.00 TRAP
1419.323	263.625	2.030	265.655	45.31	2.76	.12	265.77	.00	1.40	14.18	3.300	2.000 3.00 0 .0
17.652	.0053	-	-	-	-	.0029	.05	2.03	.45	1.76	.030	.00 3.00 TRAP

## WATER SURFACE PROFILE LISTING

Date: 6-8-2009 Time: 3:44:12

JN - 15956-A

Meadowood --- WSPGW Analysis for Existing Condition  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Width	Top Height/Dia.-FT	Base Width	No Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	ISE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR Type Ch
1436.975	263.719	1.976	265.695	45.31	2.89	.13	265.82	.00	1.40	13.86	3.300	2.000	3.00 0
19.848	.0053	-	-	-	-	.0033	.07	1.98	.48	1.76	.030	.00	3.00 TRAP
1456.823	263.824	1.923	265.747	45.31	3.03	.14	265.89	.00	1.40	13.54	3.300	2.000	3.00 0
23.827	.0053	-	-	-	-	.0037	.09	1.92	.51	1.76	.030	.00	3.00 TRAP
1480.650	263.951	1.871	265.821	45.31	3.18	.16	265.98	.00	1.40	13.22	3.300	2.000	3.00 0
32.606	.0053	-	-	-	-	.0042	.14	1.87	.54	1.76	.030	.00	3.00 TRAP
1513.257	264.124	1.820	265.944	45.31	3.34	.17	266.12	.00	1.40	12.92	3.300	2.000	3.00 0
64.918	.0053	-	-	-	-	.0048	.31	1.82	.57	1.76	.030	.00	3.00 TRAP
1578.175	264.469	1.771	266.239	45.31	3.50	.19	266.43	.00	1.40	12.62	3.300	2.000	3.00 0
77.199	.0053	-	-	-	-	.0052	.40	1.77	.61	1.76	.030	.00	3.00 TRAP
1655.374	264.879	1.757	266.636	45.31	3.55	.20	266.83	.00	1.40	12.54	3.300	2.000	3.00 0
15.296	.0053	-	-	-	-	.0053	.08	1.76	.62	1.76	.030	.00	3.00 TRAP
1670.670	264.960	1.757	266.717	45.31	3.55	.20	266.91	.00	1.40	12.54	3.300	2.000	3.00 0
486.130	.0053	-	-	-	-	.0026	4.41	1.76	.62	1.76	.030	.00	3.00 TRAP
2156.800	268.960	1.757	270.717	45.31	3.55	.20	270.91	.00	1.40	12.54	3.300	2.000	3.00 0

T1 JN - 15956-A

0

T2 Meadowood --- WSPGW Analysis for Alt.1 Grading

T3 05/29/2009

SO	.000	256.430	1					258.220		
R	471.600	258.820	1		.014				.000	
JX	471.700	258.821	4	3	.014	6.080		258.821	90.0	
	.000									
TS	475.700	258.840	5		.014				.000	
WX	475.700	258.840	6							
R	587.200	259.380	6		.013				.000	.000 0
WE	587.200	259.380	7		.500					
TS	591.200	259.400	8		.014				.000	
JX	591.300	259.401	10	9	.014	5.400		259.400	90.0	
	.000									
R	1125.300	262.158	10		.014				.000	
JX	1129.300	262.159	14	13	.014	5.400		262.160	.0	-
	90.000									
R	1129.400	262.160	14		.014				.000	
WX	1129.400	262.160	15							
R	1250.800	262.740	15		.013				.000	.000 0
JX	1254.800	263.070	17	16	.013	6.420		263.070	-90.0	
	90.000									
R	1968.800	266.640	17		.013				.000	.000 0
JX	1972.800	266.970	18		.013					-
	90.000									
R	2028.800	267.250	18		.013				.000	.000 0
JX	2032.800	267.580	19		.013					
	90.000									
R	2156.800	268.200	19		.013				.000	.000 0
SH	2156.800	268.200	19					268.200		
CD	1	1	0		.000	3.300	2.000	1.500	1.500	.00
CD	2	1	0		.000	3.300	2.000	1.500	1.500	.00
CD	3	1	0		.000	3.300	.100	.000	.000	.00
CD	4	1	0		.000	3.300	2.000	1.500	1.500	.00
CD	5	1	0		.000	3.300	11.800	.000	.000	.00
CD	6	4	2		.000	3.000	.000	.000	.000	.00
CD	7	1	0		.000	3.300	11.800	.000	.000	.00
CD	8	1	0		.000	2.500	2.000	1.500	1.500	.00
CD	9	1	0		.000	2.500	.100	.000	.000	.00
CD	10	1	0		.000	2.500	2.000	1.500	1.500	.00
CD	11	1	0		.000	1.640	2.000	3.000	3.000	.00
CD	12	1	0		.000	2.500	9.800	.000	.000	.00
CD	13	1	0		.000	1.640	2.000	.000	.000	.00
CD	14	1	0		.000	2.500	9.800	.000	.000	.00
CD	15	4	2		.000	2.500	.000	.000	.000	.00
CD	16	4	1		.000	1.500	.000	.000	.000	.00
CD	17	4	1		.000	3.500	.000	.000	.000	.00
CD	18	4	1		.000	3.500	.000	.000	.000	.00
CD	19	4	1		.000	3.500	.000	.000	.000	.00
Q		39.530	.0							



Date: 6- 8-2009 Time: 3:44:27

JN - 15956-A

Meadowood --- WSPGW Analysis for Alt.1 Grading

05/29/2009

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*****
Station | Invert | Depth | Water | Q | Vel | Vel | Energy | Super | Critical | Flow Top | Height | Base Wt | No Wth
| Elev | (FT) | Elev | (CFS) | (FPS) | Head | Grd.El. | Elev | Depth | Width | Dia.-FT | or I.D. | ZL | Prs/Pip
|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
L/Elem | Ch Slope | | | | | SF Ave | HF | SE Dpth | Froude N | Norm Dp | "N" | X-Fall | ZR | Type Ch
*****
.000 256.430 1.787 258.217 62.83 7.51 .88 259.09 .00 1.99 7.36 3.300 2.000 1.50 0 .0
343.353 .0051 .0051 1.74 1.79 1.24 1.79 .014 .00 1.50 TRAP
343.353 258.170 1.787 259.957 62.83 7.51 .88 260.83 .00 1.99 7.36 3.300 2.000 1.50 0 .0
85.315 .0051 .0049 .42 1.79 1.24 1.79 .014 .00 1.50 TRAP
428.668 258.602 1.818 260.421 62.83 7.31 .83 261.25 .00 1.99 7.46 3.300 2.000 1.50 0 .0
30.868 .0051 .0044 .14 1.82 1.20 1.79 .014 .00 1.50 TRAP
459.535 258.759 1.874 260.633 62.83 6.97 .75 261.39 .00 1.99 7.62 3.300 2.000 1.50 0 .0
9.776 .0051 .0039 .04 1.87 1.13 1.79 .014 .00 1.50 TRAP
469.312 258.808 1.931 260.740 62.83 6.64 .69 261.43 .00 1.99 7.79 3.300 2.000 1.50 0 .0
2.288 .0051 .0034 .01 1.93 1.06 1.79 .014 .00 1.50 TRAP
471.600 258.820 1.991 260.811 62.83 6.33 .62 261.43 .00 1.99 7.97 3.300 2.000 1.50 0 .0
JUNCT STR .0101 .0022 .00 1.99 1.00 .014 .00 1.50 TRAP
471.700 258.821 2.414 261.235 56.75 4.18 .27 261.51 .00 1.89 9.24 3.300 2.000 1.50 0 .0
TRANS STR .0047 .0006 .00 2.41 .61 .014 .00 1.50 TRAP
475.700 258.840 2.675 261.515 56.75 1.80 .05 261.56 .00 .90 11.80 3.300 11.800 .00 0 .0
WALL EXIT
475.700 258.840 2.675 261.515 56.75 4.26 .28 261.80 .00 1.72 1.86 3.000 .000 .00 2 .0
39.003 .0048 .0017 .07 2.68 .28 1.69 .013 .00 .00 PIPE

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JN - 15956-A  
 Meadowood --- WSPGW Analysis for Alt.1 Grading  
 05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top/Height	Base Wt	No Wth	2L	Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	ISE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****	*****
514.703	259.029	2.523	261.552	56.75	4.47	.31	261.86	.00	1.72	2.19	3.000	.000	.00	2 .0
8.578	.0048	-	-	-	-	.0018	.02	2.52	.33	1.69	.013	.00	.00	PIPE
523.281	259.070	2.491	261.561	56.75	4.52	.32	261.88	.00	1.72	2.25	3.000	.000	.00	2 .0
HYDRAULIC JUMP	-	-	-	-	-	-	-	-	-	-	-	-	-	-
523.281	259.070	1.694	260.765	56.75	6.89	.74	261.50	.00	1.72	2.97	3.000	.000	.00	2 .0
56.066	.0048	-	-	-	-	.0048	.27	1.69	.73	1.69	.013	.00	.00	PIPE
579.347	259.342	1.694	261.036	56.75	6.89	.74	261.77	.00	1.72	2.97	3.000	.000	.00	2 .0
7.853	.0048	-	-	-	-	.0047	.04	1.69	.73	1.69	.013	.00	.00	PIPE
587.200	259.380	1.723	261.103	56.75	6.75	.71	261.81	.00	1.72	2.97	3.000	.000	.00	2 .0
587.200	259.380	2.230	261.610	56.75	5.04	.39	262.00	.00	1.72	2.62	3.000	.000	.00	2 .0
WALL ENTRANCE	-	-	-	-	-	-	-	-	-	-	-	-	-	-
587.200	259.380	3.428	262.808	56.75	1.40	.03	262.84	.00	.90	11.80	3.300	11.800	.00	0 .0
TRANS STR	.0050	-	-	-	-	.0002	.00	3.43	.13		.014	.00	.00	TRAP
591.200	259.400	3.381	262.781	56.75	2.37	.09	262.87	.00	1.89	12.14	2.500	2.000	1.50	0 .0
JUNCT STR	.0101	-	-	-	-	.0002	.00	3.38	.30		.014	.00	1.50	TRAP
591.300	259.401	3.414	262.815	51.35	2.11	.07	262.88	.00	1.80	12.24	2.500	2.000	1.50	0 .0
17.469	.0052	-	-	-	-	.0002	.00	3.41	.26	1.62	.014	.00	1.50	TRAP
608.769	259.491	3.320	262.811	51.35	2.22	.08	262.89	.00	1.80	11.96	2.500	2.000	1.50	0 .0
16.970	.0052	-	-	-	-	.0002	.00	3.32	.28	1.62	.014	.00	1.50	TRAP

JN - 15956-A  
Meadowood --- WSPGW Analysis for Alt.1 Grading  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top	Height/Base Wt	No Wch		
L/Elem	Ch Slope					SF Ave	HF	ISE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
625.739	259.579	3.229	262.808	51.35	2.32	.08	262.89	.00	1.80	11.69	2.500	2.000	1.50	0
16.474	.0052	-	-	-	-	.0003	.00	3.23	.30	1.62	.014	.00	1.50	TRAP
642.213	259.664	3.140	262.804	51.35	2.44	.09	262.90	.00	1.80	11.42	2.500	2.000	1.50	0
15.980	.0052	-	-	-	-	.0003	.00	3.14	.32	1.62	.014	.00	1.50	TRAP
658.193	259.746	3.053	262.799	51.35	2.56	.10	262.90	.00	1.80	11.16	2.500	2.000	1.50	0
15.488	.0052	-	-	-	-	.0003	.01	3.05	.34	1.62	.014	.00	1.50	TRAP
673.681	259.826	2.968	262.795	51.35	2.68	.11	262.91	.00	1.80	10.90	2.500	2.000	1.50	0
14.996	.0052	-	-	-	-	.0004	.01	2.97	.36	1.62	.014	.00	1.50	TRAP
688.677	259.904	2.886	262.789	51.35	2.81	.12	262.91	.00	1.80	10.66	2.500	2.000	1.50	0
14.502	.0052	-	-	-	-	.0004	.01	2.89	.38	1.62	.014	.00	1.50	TRAP
703.179	259.979	2.805	262.784	51.35	2.95	.14	262.92	.00	1.80	10.41	2.500	2.000	1.50	0
14.004	.0052	-	-	-	-	.0005	.01	2.80	.40	1.62	.014	.00	1.50	TRAP
717.184	260.051	2.726	262.777	51.35	3.09	.15	262.93	.00	1.80	10.18	2.500	2.000	1.50	0
13.501	.0052	-	-	-	-	.0006	.01	2.73	.43	1.62	.014	.00	1.50	TRAP
730.685	260.121	2.649	262.770	51.35	3.24	.16	262.93	.00	1.80	9.95	2.500	2.000	1.50	0
12.989	.0052	-	-	-	-	.0007	.01	2.65	.45	1.62	.014	.00	1.50	TRAP
743.674	260.188	2.575	262.762	51.35	3.40	.18	262.94	.00	1.80	9.72	2.500	2.000	1.50	0
12.465	.0052	-	-	-	-	.0007	.01	2.57	.48	1.62	.014	.00	1.50	TRAP

JN - 15956-A

Meadowood --- WSPGW Analysis for Alt.1 Grading

05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Width	Height/Dia.-FT	Base Wt/or I.D.	No ZL	Wth Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	2R	Type Ch
756.139	260.252	2.502	262.754	51.35	3.57	.20	262.95	.00	1.80	9.50	2.500	2.000	1.50	0 .0
11.925	.0052					.0008	.01	2.50	.51	1.62	.014	.00	1.50	TRAP
768.064	260.314	2.430	262.744	51.35	3.74	.22	262.96	.00	1.80	9.29	2.500	2.000	1.50	0 .0
11.363	.0052					.0010	.01	2.43	.54	1.62	.014	.00	1.50	TRAP
779.427	260.372	2.361	262.733	51.35	3.93	.24	262.97	.00	1.80	9.08	2.500	2.000	1.50	0 .0
10.772	.0052					.0011	.01	2.36	.58	1.62	.014	.00	1.50	TRAP
790.200	260.428	2.293	262.721	51.35	4.12	.26	262.98	.00	1.80	8.88	2.500	2.000	1.50	0 .0
10.143	.0052					.0012	.01	2.29	.61	1.62	.014	.00	1.50	TRAP
800.342	260.480	2.227	262.707	51.35	4.32	.29	263.00	.00	1.80	8.68	2.500	2.000	1.50	0 .0
9.461	.0052					.0014	.01	2.23	.65	1.62	.014	.00	1.50	TRAP
809.803	260.529	2.162	262.691	51.35	4.53	.32	263.01	.00	1.80	8.49	2.500	2.000	1.50	0 .0
8.708	.0052					.0016	.01	2.16	.69	1.62	.014	.00	1.50	TRAP
818.511	260.574	2.100	262.674	51.35	4.75	.35	263.02	.00	1.80	8.30	2.500	2.000	1.50	0 .0
7.855	.0052					.0018	.01	2.10	.73	1.62	.014	.00	1.50	TRAP
826.365	260.615	2.038	262.653	51.35	4.98	.39	263.04	.00	1.80	8.11	2.500	2.000	1.50	0 .0
5.043	.0052					.0020	.01	2.04	.78	1.62	.014	.00	1.50	TRAP
831.408	260.641	1.991	262.632	51.35	5.17	.42	263.05	.00	1.80	7.97	2.500	2.000	1.50	0 .0

HYDRAULIC JUMP

JN - 15956-A  
Meadowood --- WSPGW Analysis for Alt.1 Grading  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top Height	Base Wt	No Wth	ZL	Pipe/Pip
L/Elem	Ch Slope					SE Ave	HF	ISE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
831.408	260.641	1.616	262.257	51.35	7.18	.80	263.06	.00	1.80	6.85	2.500	2.000	1.50	0
176.682	.0052	-	-	-	-	.0052	.91	1.62	1.24	1.62	.014	.00	1.50	TRAP
1008.090	261.553	1.616	263.169	51.35	7.18	.80	263.97	.00	1.80	6.85	2.500	2.000	1.50	0
76.427	.0052	-	-	-	-	.0050	.38	1.62	1.24	1.62	.014	.00	1.50	TRAP
1084.516	261.947	1.642	263.589	51.35	7.01	.76	264.35	.00	1.80	6.93	2.500	2.000	1.50	0
29.523	.0052	-	-	-	-	.0045	.13	1.64	1.20	1.62	.014	.00	1.50	TRAP
1114.039	262.100	1.693	263.793	51.35	6.68	.69	264.49	.00	1.80	7.08	2.500	2.000	1.50	0
9.116	.0052	-	-	-	-	.0040	.04	1.69	1.13	1.62	.014	.00	1.50	TRAP
1123.156	262.147	1.745	263.892	51.35	6.37	.63	264.52	.00	1.80	7.24	2.500	2.000	1.50	0
2.145	.0052	-	-	-	-	.0035	.01	1.75	1.06	1.62	.014	.00	1.50	TRAP
1125.300	262.158	1.800	263.958	51.35	6.07	.57	264.53	4.32	1.80	7.40	2.500	2.000	1.50	0
JUNCT STR	.0003	-	-	-	-	.0017	.01	6.12	1.00	-	.014	.00	1.50	TRAP
1129.300	262.159	2.395	264.554	45.95	1.96	.06	264.61	.00	.88	9.80	2.500	9.800	.00	0
.100	.0101	-	-	-	-	.0002	.00	2.39	.22	.64	.014	.00	.00	TRAP
1129.400	262.160	2.394	264.554	45.95	1.96	.06	264.61	.00	.88	9.80	2.500	9.800	.00	0
WALL EXIT	-	-	-	-	-	-	-	-	-	-	-	-	-	-
1129.400	262.160	2.394	264.554	45.95	4.75	.35	264.90	.00	1.63	1.01	2.500	.000	.00	2
67.367	.0048	-	-	-	-	.0028	.19	2.39	.27	1.71	.013	.00	.00	PIPE

## JN - 15956-A

Meadowood --- WSPGW Analysis for Alt.1 Grading  
 05/29/2009

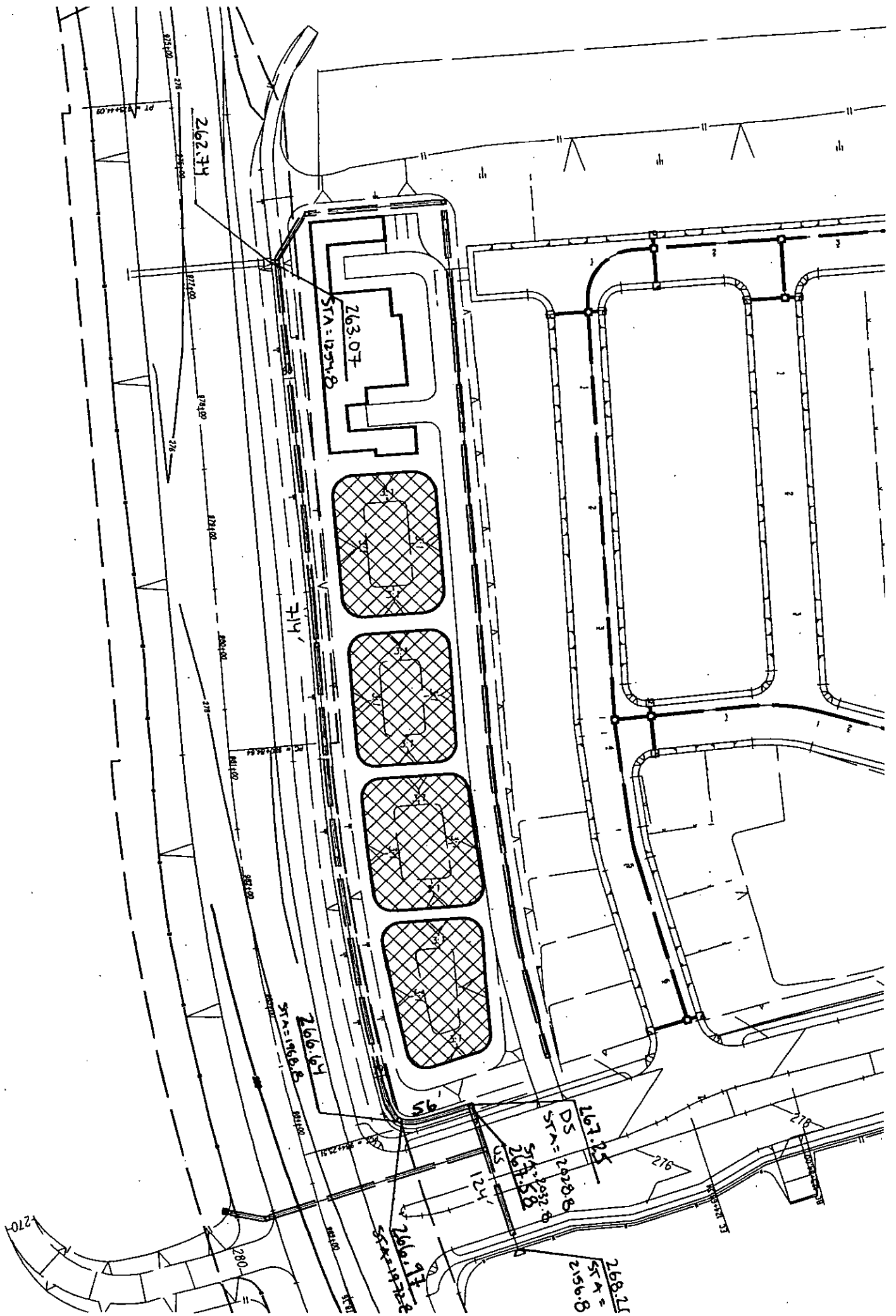
Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Depth	Flow Top	Height/ Base Wt	No Wth Pts/Pip		
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR	Type Ch
1196.767	262.482	2.223	264.705	45.95	4.98	.39	265.09	.00	1.63	1.57	2.500	.000	.00	2 .0
46.671	.0048	-	-	-	-	.0029	.14	2.22	.36	1.71	.013	.00	.00	PIPE
1243.438	262.705	2.097	264.802	45.95	5.22	.42	265.23	.00	1.63	1.84	2.500	.000	.00	2 .0
7.363	.0048	-	-	-	-	.0030	.02	2.10	.42	1.71	.013	.00	.00	PIPE
1250.800	262.740	2.077	264.817	45.95	5.27	.43	265.25	2.50	1.63	1.87	2.500	.000	.00	2 .0
JUNCT STR	.0825	-	-	-	-	-	-	2.50	.43	-	.013	.00	.00	PIPE
1254.800	263.070	1.864	264.934	39.53	7.59	.89	265.83	.00	1.95	3.49	3.500	.000	.00	1 .0
653.108	.0050	-	-	-	-	.0050	3.27	1.86	1.10	1.86	.013	.00	.00	PIPE
1907.908	266.336	1.864	268.199	39.53	7.59	.89	269.09	.00	1.95	3.49	3.500	.000	.00	1 .0
48.078	.0050	-	-	-	-	.0049	.24	1.86	1.10	1.86	.013	.00	.00	PIPE
1955.986	266.576	1.879	268.455	39.53	7.51	.88	269.33	.00	1.95	3.49	3.500	.000	.00	1 .0
12.814	.0050	-	-	-	-	.0046	.06	1.88	1.08	1.86	.013	.00	.00	PIPE
1968.800	266.640	1.954	268.594	39.53	7.16	.80	269.39	3.50	1.95	3.48	3.500	.000	.00	1 .0
JUNCT STR	.0825	-	-	-	-	-	-	3.50	1.00	-	.013	.00	.00	PIPE
1972.800	266.970	1.864	268.834	39.53	7.59	.89	269.73	.00	1.95	3.49	3.500	.000	.00	1 .0
43.185	.0050	-	-	-	-	.0049	.21	1.86	1.10	1.86	.013	.00	.00	PIPE
2015.985	267.186	1.879	269.065	39.53	7.51	.88	269.94	.00	1.95	3.49	3.500	.000	.00	1 .0
12.815	.0050	-	-	-	-	.0046	.06	1.88	1.08	1.86	.013	.00	.00	PIPE

JN - 15956-A

Meadowood --- MSPGW Analysis for Alt.1 Grading  
05/29/2009

Station	Invert Elev	Depth (FT)	Water Elev	Q (CFS)	Vel (FPS)	Vel Head	Energy Grd.El.	Super Elev	Critical Flow Depth	Flow Top Height	Base Wt	No Wch	Prs/Pip
L/Elem	Ch Slope					SF Ave	HF	SE Dpth	Froude N	Norm Dp	"N"	X-Fall	ZR
2028.800	267.250	1.954	269.204	39.53	7.16	.80	270.00	3.50	1.95	3.48	3.500	.000	.00
JUNCT STR	.0825												
2032.800	267.580	1.864	269.444	39.53	7.59	.89	270.34	.00	1.95	3.49	3.500	.000	.00
62.706	.0050					.0050	.31	1.86	1.10	1.86	.013	.00	.00
2095.506	267.894	1.864	269.757	39.53	7.59	.89	270.65	.00	1.95	3.49	3.500	.000	.00
48.486	.0050					.0049	.24	1.86	1.10	1.86	.013	.00	.00
2143.992	268.136	1.879	270.015	39.53	7.51	.88	270.89	.00	1.95	3.49	3.500	.000	.00
12.808	.0050					.0046	.06	1.88	1.08	1.86	.013	.00	.00
2156.800	268.200	1.954	270.154	39.53	7.16	.80	270.95	.00	1.95	3.48	3.500	.000	.00

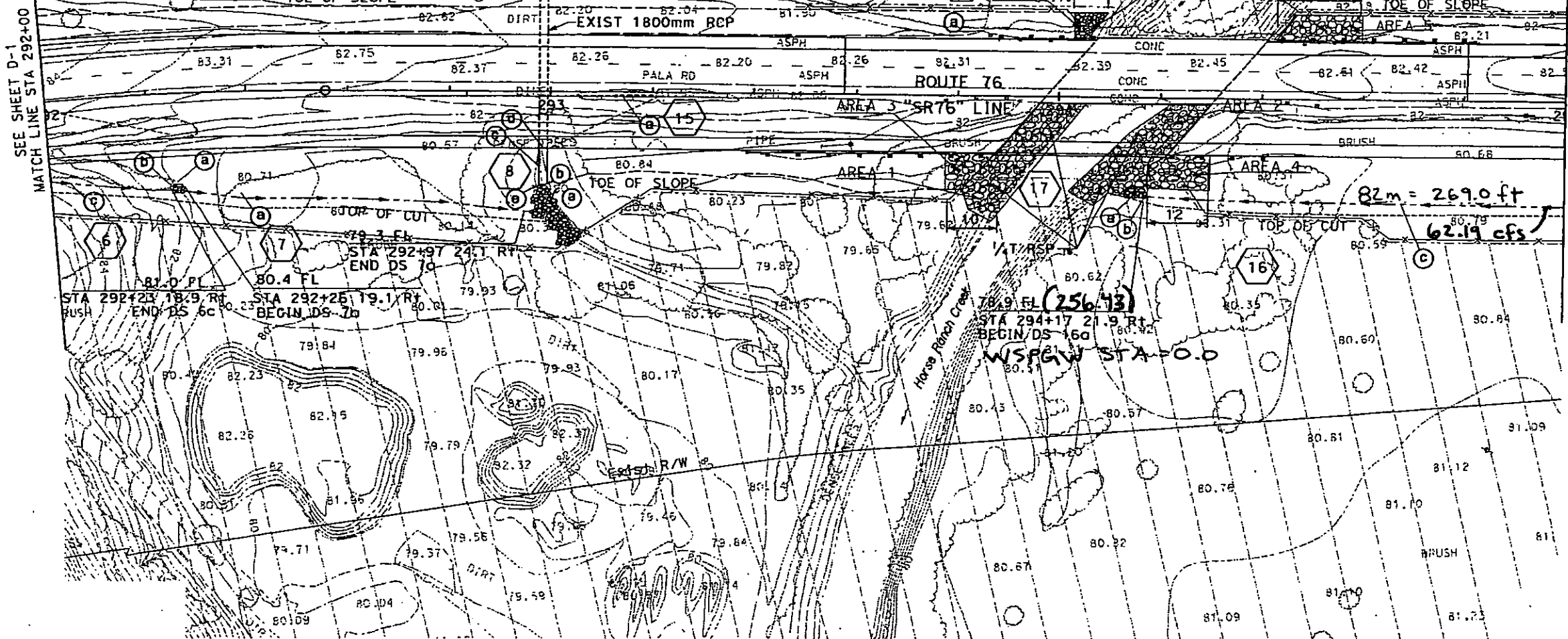
ALT 1





- 6 (a) RIPRAP ENERGY DISSIPATOR (SEE DRAINAGE DETAIL ON SHEET DD-1)  
 (b) CUTOFF WALL (SEE DRAINAGE DETAIL SHEET DD-4)  
 (c) CONCRETE TRAPEZOIDAL DITCH (SEE DRAINAGE DETAIL SHEET DD-3)
- 7 (a) BIOSWALE (SEE DRAINAGE DETAIL SHEET DD-3)
- 8 SEE DRAINAGE PROFILE SHEET DP-1
- 15 (a) ABANDON EXISTING PIPES AND INLETS
- 16 (a) RIPRAP ENERGY DISSIPATOR (SEE DRAINAGE DETAIL ON SHEET DD-1)  
 (b) CUTOFF WALL (SEE DRAINAGE DETAIL SHEET DD-4)  
 (c) CONCRETE TRAPEZOIDAL DITCH (SEE DRAINAGE DETAIL SHEET DD-3)
- 17 RSP for BRIDGE (SEE DRAINAGE DETAIL SHEET DD-3)

SEE SHEET D-1  
 MATCH LINE STA 292+00



MATCH LINE STA 295+00  
 SEE SHEET D-3

DIST	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No
11	SD	76	R28.0-30.1	58

*Hadi Sami*  
 REGISTERED CIVIL ENGINEER 2/1/08

PLANS APPROVAL DATE

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GRANITE CONSTRUCTION COMPANY  
 38000 MONROE STREET  
 INDIO, CALIFORNIA 92203

URS CORPORATION  
 1515 MURRAY CANYON RD, SUITE 1000  
 SAN DIEGO, CALIFORNIA 92108

SCALE 1:1000

\* Metric \*

# DRAINAGE PLAN

SCALE 1:500

D-2

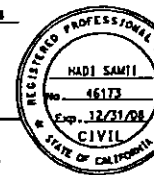
THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY.

ALL DIMENSIONS ARE IN METERS  
 UNLESS OTHERWISE SHOWN



DIST	COUNTY	ROUTE	KILOMETER POST TOTAL PROJECT	SHEET No	T SH
11	SD	76	R28.0-30.1	60	

*Hadi Jamir*  
REGISTERED CIVIL ENGINEER

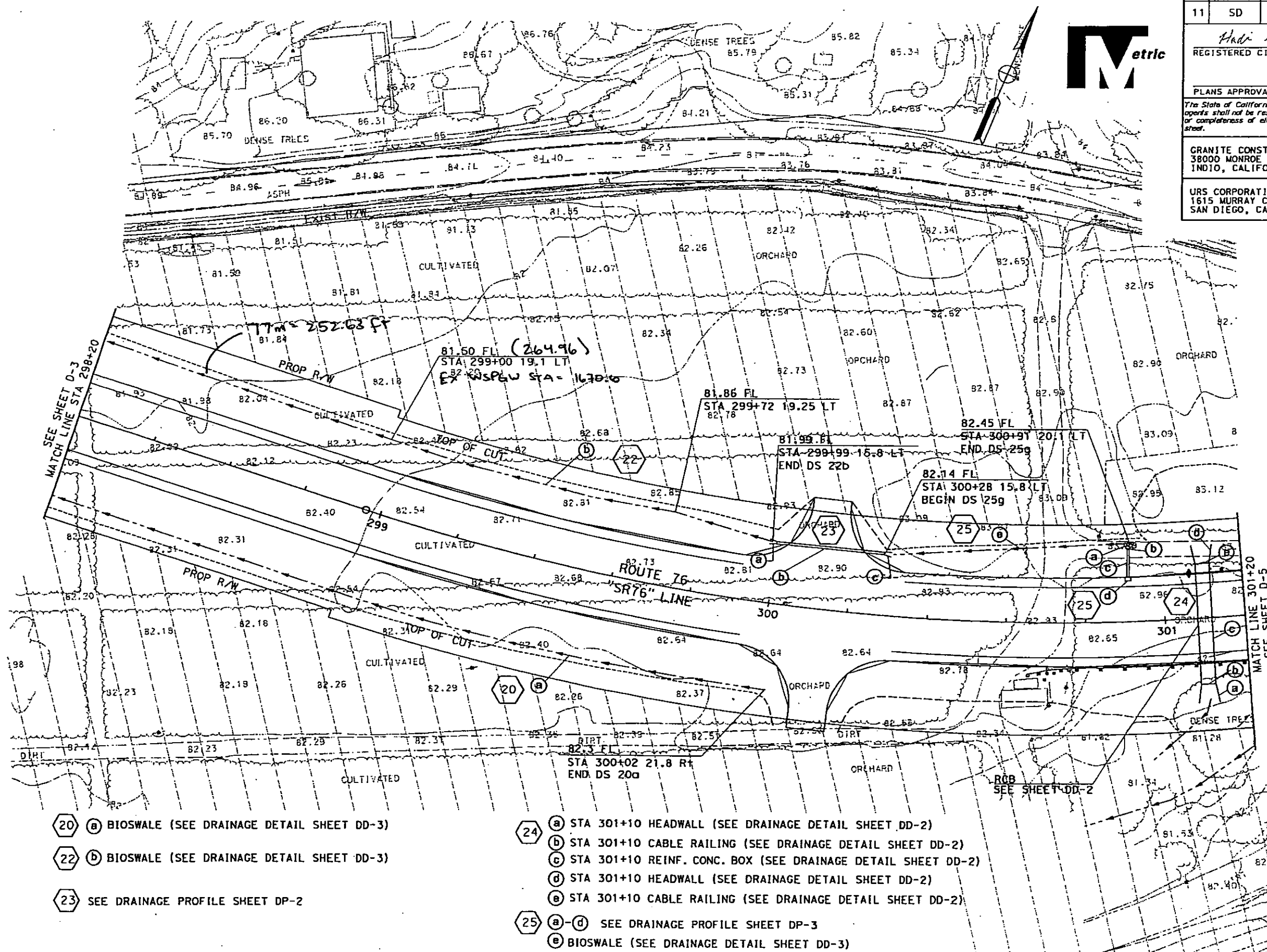


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GRANITE CONSTRUCTION COMPANY  
38000 MONROE STREET  
INDIO, CALIFORNIA 92203

URS CORPORATION  
1615 MURRAY CANYON RD, SUITE 1000  
SAN DIEGO, CALIFORNIA 92108



# DRAINAGE PLAN

SCALE : 1:500

**D - 4**

THIS PLAN ACCURATE FOR DRAINAGE WORK ONLY.

ALL DIMENSIONS ARE IN METERS  
UNLESS OTHERWISE SHOWN

```

| USERNAME => jeremy_kahn
| DCN FILE => ...\\OB Drainage\\io004.dgn

```

חתחת וזל

FD 231 501

[illegible]